



United States  
Environmental Protection Agency  
Wood Heater Certification Test Report

**Jotul North America**  
**F400**

Volume 1 of 1

**LoKEE**  
**TESTING LABORATORY**

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## TEST SERIES INFORMATION

Unit name and model number: F400

Type of unit: Wood Heater

Manufacturer: Jotul North America  
Address: 400 Riverside Street  
Portland, ME 04104

Contact: Shawn Malloy  
Phone Number: 1-207-797-5912  
Fax Number: 1-207-772-0523

Observers: Shawn Malloy

Date Received: 3/31/2000 Aged: 4/4-5/2000 Dates Tested: 4/7-12/2000

**Tested by:** LoKee Testing Lab using EPA Methods 28, 28A and 5H where applicable.

Test Location: 13235 Prairie Circle East  
Sumner, WA 98390-7250

Test Site Elevation: 500 feet above sea level

LoKee's Field Team

Team Members: Chip Wadington  
Cindy Kingman  
Deborah Wadington

The following pages contain (1) test unit storage information, (2) a diagram showing the height and location of the stack components and sampling ports, and (3) copies of the certification test notices and cancellations sent to the EPA.



## STOVE STORAGE INFORMATION

1. **Temporary Storage at LoKee**

A single, steel, banding strap is placed around the unit, preventing opening of the loading door.

2. **Permanent Storage**

After certification is granted, additional banding is placed both horizontally and vertically around the unit to prevent access to the interior of the unit. An address label is then taped over the intersecting bands to act as a seal. Warning labels are affixed on the unit. The unit is then shipped via common carrier to the manufacturer's designated storage facility unless otherwise noted. A sample of the warning label follows.

## WARNING

### SEALED EPA TEST UNIT

**DO NOT TAMPER WITH SEALS  
TO DO SO WILL VOID CERTIFICATION**

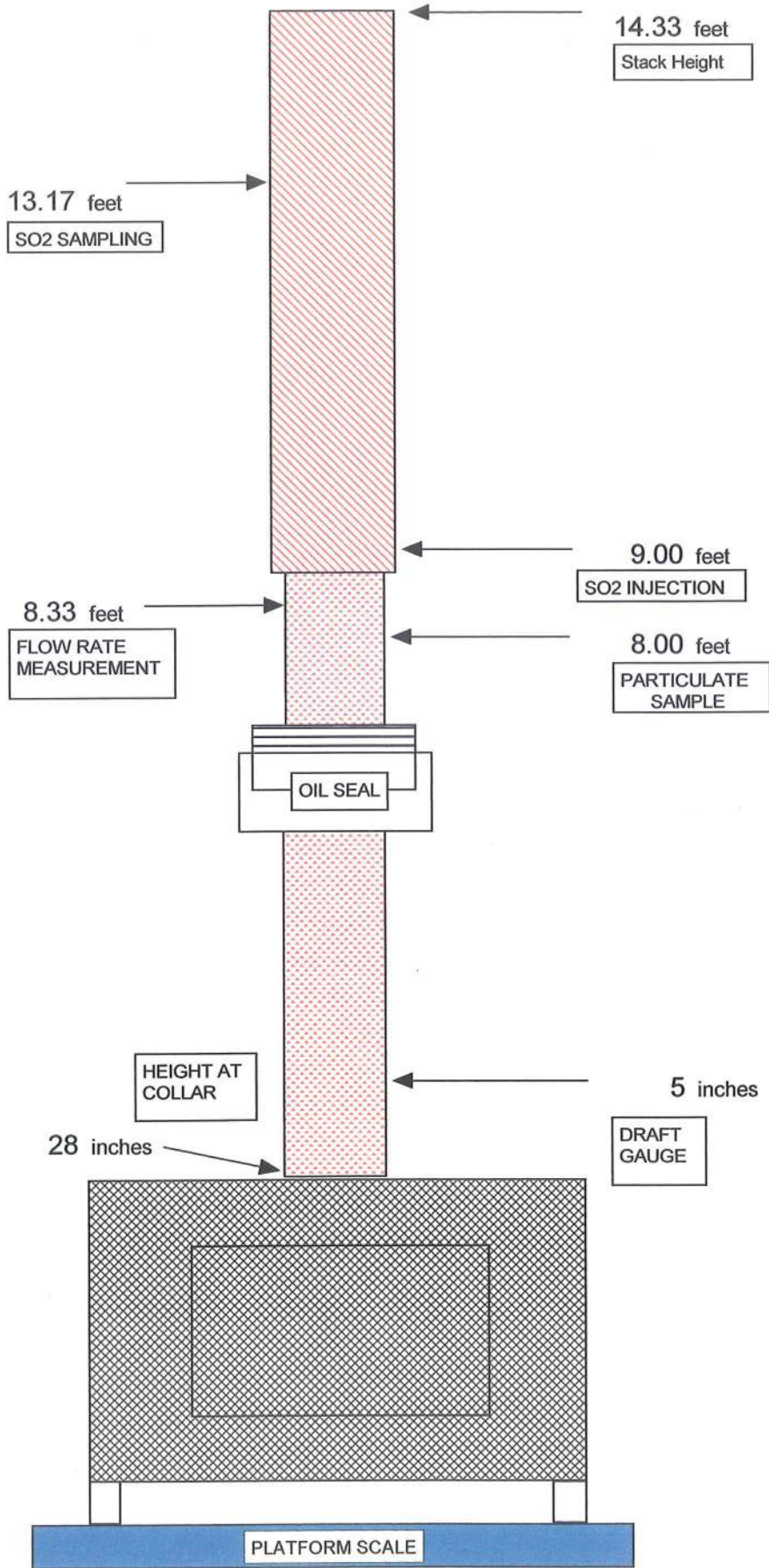
**JOTUL NORTH AMERICA**

**F400**



Model: F400

Date: 04/12/00





# AGING DATA SHEET

UNIT: F400

DATE: 4-4-00

| Hr # | DATE | TIME | TEMP<br>TOP <sub>1</sub> | TEMP<br>Firebox <sub>2</sub> |
|------|------|------|--------------------------|------------------------------|
| 1    | 4-4  | 1350 | 318                      | 641                          |
| 2    | "    | 1450 | 501                      | 370                          |
| 3    | "    | 1550 | 551                      | 601                          |
| 4    | "    | 1650 | 338                      | 622                          |
| 5    | "    | 1750 | 278                      | 498                          |
| 6    | 4-5  | 1515 | 577                      | 887                          |
| 7    | "    | 1615 | 317                      | 598                          |
| 8    | "    | 1715 | 428                      | 348                          |
| 9    | "    | 1815 | 592                      | 591                          |
| 10   | "    | 1915 | 358                      | 631                          |
| 11   |      |      |                          |                              |
| 12   |      |      |                          |                              |
| 13   |      |      |                          |                              |
| 14   |      |      |                          |                              |
| 15   |      |      |                          |                              |
| 16   |      |      |                          |                              |
| 17   |      |      |                          |                              |
| 18   |      |      |                          |                              |
| 19   |      |      |                          |                              |
| 20   |      |      |                          |                              |
| 21   |      |      |                          |                              |
| 22   |      |      |                          |                              |
| 23   |      |      |                          |                              |
| 24   |      |      |                          |                              |
| 25   |      |      |                          |                              |

| Hr # | DATE | TIME | TEMP<br>1 | TEMP<br>2 |
|------|------|------|-----------|-----------|
| 26   |      |      |           |           |
| 27   |      |      |           |           |
| 28   |      |      |           |           |
| 29   |      |      |           |           |
| 30   |      |      |           |           |
| 31   |      |      |           |           |
| 32   |      |      |           |           |
| 33   |      |      |           |           |
| 34   |      |      |           |           |
| 35   |      |      |           |           |
| 36   |      |      |           |           |
| 37   |      |      |           |           |
| 38   |      |      |           |           |
| 39   |      |      |           |           |
| 40   |      |      |           |           |
| 41   |      |      |           |           |
| 42   |      |      |           |           |
| 43   |      |      |           |           |
| 44   |      |      |           |           |
| 45   |      |      |           |           |
| 46   |      |      |           |           |
| 47   |      |      |           |           |
| 48   |      |      |           |           |
| 49   |      |      |           |           |
| 50   |      |      |           |           |

**COMMENTS:**

4-4-00 Stove lit 1015  
 4-5-00 " " 1110





**LOKEE TESTING LABORATORY.**  
13235 PRAIRIE CIRCLE EAST, SUMNER, WA 98390-7250  
Phone (360)-897-9685

**To:** Robert C. Marshall, Jr., US EPA  
**From:** Chip Wadington, LoKee Testing Laboratory  
**Subject:** Wood Stove Certification Test Notification

This is to notify EPA that:

**Manufacturer's Name:** JOTUL USA INC.  
**Address:** 400 Riverside Street  
Portland, ME 04104

**Contact:** Shawn Malloy  
**Phone:** 1-207-797-5912

has scheduled the Model #F400 for certification testing at LoKee according to the following:

| <b>Dates Scheduled</b> | <b>Date Notification Sent</b> | <b>Date Notification Canceled</b> | <b>Testing Activity (if any)</b> |
|------------------------|-------------------------------|-----------------------------------|----------------------------------|
|                        |                               |                                   |                                  |
|                        |                               |                                   |                                  |
|                        |                               |                                   |                                  |
|                        |                               |                                   |                                  |
| 2/7-11/2000            | 1/5/2000                      |                                   | None                             |
| 2/14-18/2000           | 1/5/2000                      |                                   | None                             |
| 2/21-25/2000           | 1/5/2000                      |                                   | None                             |
| 2/28-2/3/2000          | 1/5/2000                      |                                   | None                             |
| 3/27-31/2000           | 2/25/2000                     |                                   | None                             |
| 4/3-7/2000             | 2/25/2000                     |                                   | Cert started                     |
| 4/10-14/2000           | 2/25/2000                     |                                   | Cert complete                    |
| 4/17-21/2000           | 2/25/2000                     |                                   | None                             |
| 4/24-28/2000           | 2/25/2000                     |                                   | none                             |
|                        |                               |                                   |                                  |







# Wood Heater Emission Test Summary

## Laboratory/Wood Heater Information

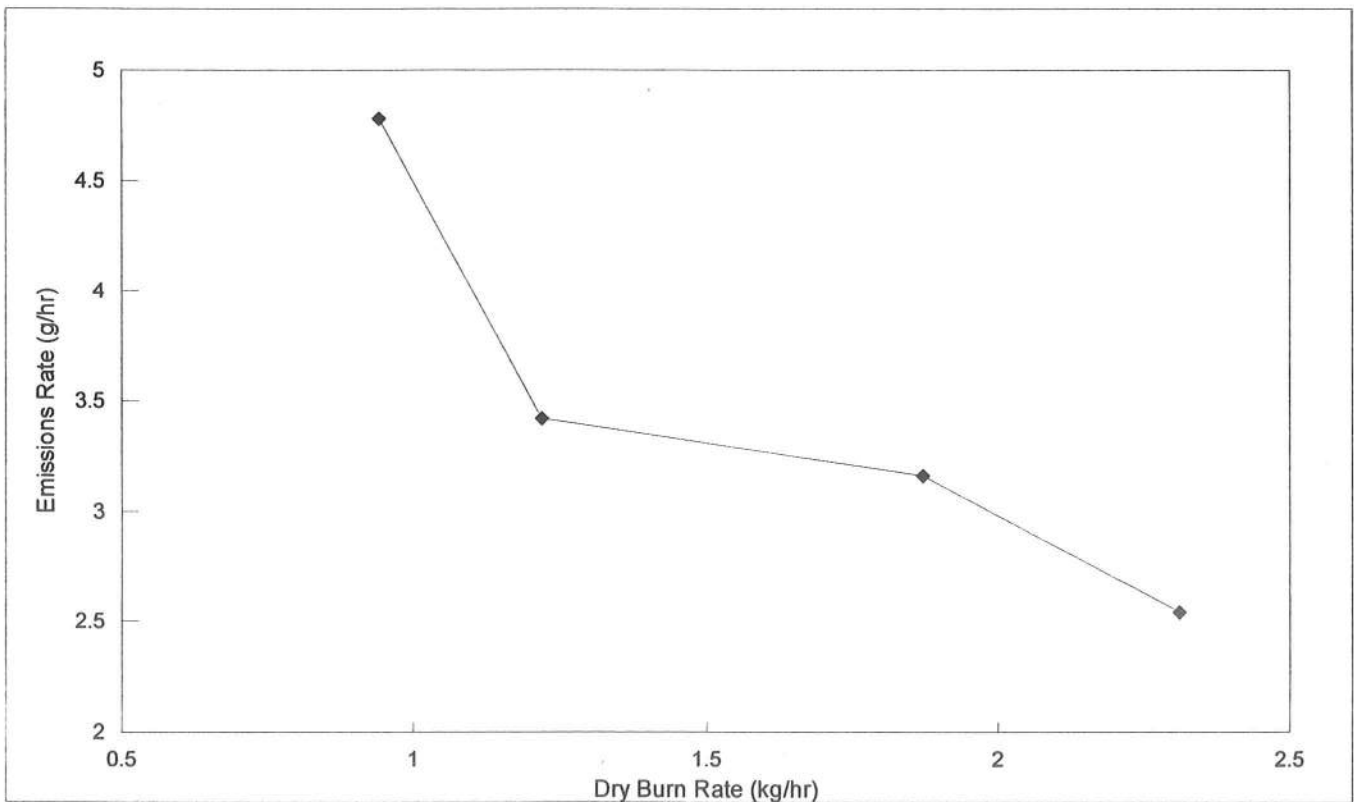
Stove Manufacturer: **Jotul**  
Model Identification: **F400**  
Stove Type> 1=cat,  
2=noncat, 3=pellet: **2**

Laboratory Name: **LoKee Testing Lab**  
Laboratory Contact: **CHIP WADINGTON**  
Telephone no.: **360-897-9685**

Test Dates: **4/7-12/2000**

Test Methods Used  
Method 28/Other: **28**  
Sampling Method: **5H**

| Run no. | Burn Rate (kg/hr) | Emission Rate (g/hr) | Heat Output (Btu/hr) | Wtd Avg (g/hr)<br>3.77 |
|---------|-------------------|----------------------|----------------------|------------------------|
| 1       | 0.94              | 4.78                 | 11335                |                        |
| 2       | 1.22              | 3.42                 | 14711                |                        |
| 3       | 1.87              | 3.16                 | 22549                |                        |
| 4       | 2.31              | 2.54                 | 27854                |                        |





Unit : Jotul F400

DATA SUMMARY

|                                   | RUN #        | 1       | 3       | 4       | 2       |
|-----------------------------------|--------------|---------|---------|---------|---------|
| <b>Particulate Emissions:</b>     |              |         |         |         |         |
| Concentration:                    | grains/dscf: | .1922   | .1072   | .0750   | .0526   |
| Emissions Rate                    | grams/hr:    | 4.78    | 3.42    | 3.16    | 2.54    |
| Emissions Factor                  | grams/kg:    | 5.11    | 2.79    | 1.69    | 1.10    |
| Front Half Catch                  | % of total   | 32.90   | 25.09   | 39.34   | 38.55   |
| Total Mass Captured               | total catch: | 1.1356  | .5022   | .1993   | .1751   |
|                                   |              |         |         |         |         |
| <b>Heat Output (EPA Default):</b> | BTU/hr       | 11286.5 | 14759.2 | 22500.6 | 27806.2 |
|                                   |              |         |         |         |         |
| <b>Fuel Burn Rates:</b>           |              |         |         |         |         |
| Average kg/hr (dry)               | Kg/hr        | 0.94    | 1.22    | 1.87    | 2.31    |
|                                   |              |         |         |         |         |
| <b>Fuel Moisture Content:</b>     |              |         |         |         |         |
| Kindling (wet basis)              | %            | 13.917  | 14.040  | 14.821  | 12.562  |
| Pretest Fuel (wet basis)          | %            | 16.162  | 17.643  | 17.241  | 16.452  |
| Test Fuel (wet basis)             | %            | 17.961  | 16.994  | 16.304  | 17.164  |
|                                   |              |         |         |         |         |
| <b>Air to Fuel Ratio</b>          |              | -       | -       | -       | -       |
|                                   |              |         |         |         |         |
| <b>Average Stack Gas</b>          |              |         |         |         |         |
| Avg CO <sub>2</sub>               | %            | 6.27    | 6.68    | 8.37    | 9.22    |
| Avg O <sub>2</sub>                | %            | -       | -       | -       | -       |
| Avg CO                            | %            | 1.19    | 0.96    | 0.66    | 0.58    |
| Avg Moisture                      | %            | 6.65    | 7.31    | 8.12    | 8.69    |
| <b>Avg Stack Gas Emissions:</b>   |              |         |         |         |         |
| CO                                | g/Kg         | 163.51  | 129.18  | 76.44   | 62.77   |
|                                   | g/hr         | 153.04  | 158.12  | 142.64  | 144.76  |





Unit : Jotul F400

|                                  | RUN #               | 1      | 3      | 4      | 2      |
|----------------------------------|---------------------|--------|--------|--------|--------|
| <b>Avg Stack Gas Flow Rate</b>   |                     |        |        |        |        |
| EPA CMB                          | dscfm               | 6.40   | 8.20   | 10.83  | 12.45  |
| Tracer Gas                       | dscfm               | 7.372  | 8.570  | 9.336  | 10.469 |
| Draft (static)                   | in H <sub>2</sub> O | -0.036 | -0.041 | -0.055 | -0.056 |
| Proportionality Average          | %                   | 100    | 100    | 100    | 100    |
| <b>Average Temperatures</b>      |                     |        |        |        |        |
| Stack Gas                        | °F                  | 298    | 352    | 494    | 552    |
| Firebox                          | °F                  | 645    | 651    | 781    | 772    |
| Secondary                        | °F                  | 789    | 893    | 1096   | 1089   |
| Catalytic Combustor              | °F                  | -      | -      | -      | -      |
| Top                              | °F                  | 369    | 406    | 520    | 571    |
| Left Side                        | °F                  | 278    | 322    | 383    | 412    |
| Back                             | °F                  | 284    | 293    | 353    | 366    |
| Right Side                       | °F                  | 275    | 298    | 361    | 377    |
| Bottom                           | °F                  | 215    | 229    | 244    | 242    |
| Temperature Change               | °F                  | -74.8  | -41.2  | -37.2  | -31.2  |
| <b>Test Chamber Environment</b>  |                     |        |        |        |        |
| Average Barometer                | in. Hg              | 30.20  | 30.09  | 30.09  | 30.21  |
| Average Temperature              | °F                  | 75     | 80     | 81     | 81     |
| Ambient Moisture                 | % H <sub>2</sub> O  | 1.3    | 1.25   | 1.3    | 1.2    |
| Relative Humidity                | %RH                 | 38.0   | 39.5   | 38.5   | 36.0   |
| Air Velocity                     | m/sec               | 0      | 0      | 0      | 0      |
| <b>Fuel Weight and Burn Time</b> |                     |        |        |        |        |
| Density (dry basis)              | gm/cm <sup>3</sup>  | -      | -      | -      | -      |
| Coal Bed Weight                  | lbs                 | 3.1    | 2.8    | 2.6    | 2.7    |
| Pre Test Fuel (inc kindling)     | lbs                 | 44.1   | 41.6   | 39.1   | 41.2   |
| Test Fuel                        | lbs                 | 13.2   | 13.0   | 12.7   | 13.3   |
| Burn Time                        | min                 | 315    | 240    | 155    | 130    |







TABLE 1 ----- RAW DATA

CLIENT : Jotul

TEST No. : 1

MODEL: F400

DATE: 07-Apr-00

\*\*\*\*\*

| TIME<br>(MIN.) | METER<br>READING<br>(C F) | DELTA<br>H<br>(IN. H2O) | METER<br>TEMP.<br>(DEG. F) | PERCENT<br>CO<br>( % ) | PERCENT<br>CO2<br>( % ) | SO2<br>COCENTR.<br>PPM |
|----------------|---------------------------|-------------------------|----------------------------|------------------------|-------------------------|------------------------|
| 0              | 158.000                   | 0.150                   | 80                         | 1.24                   | 5.60                    | 450                    |
| 5              | 159.500                   | 0.160                   | 82                         | 1.09                   | 3.80                    | 425                    |
| 10             | 161.121                   | 0.160                   | 82                         | 0.49                   | 1.90                    | 425                    |
| 15             | 162.743                   | 0.140                   | 82                         | 0.51                   | 2.00                    | 450                    |
| 20             | 164.274                   | 0.130                   | 82                         | 0.57                   | 2.20                    | 475                    |
| 25             | 165.725                   | 0.120                   | 82                         | 0.64                   | 2.40                    | 500                    |
| 30             | 167.104                   | 0.110                   | 82                         | 0.72                   | 2.70                    | 525                    |
| 35             | 168.417                   | 0.120                   | 82                         | 0.73                   | 3.00                    | 500                    |
| 40             | 169.795                   | 0.120                   | 82                         | 0.87                   | 3.50                    | 500                    |
| 45             | 171.174                   | 0.280                   | 82                         | 0.19                   | 12.50                   | 325                    |
| 50             | 173.293                   | 0.280                   | 82                         | 0.11                   | 12.00                   | 325                    |
| 55             | 175.412                   | 0.280                   | 82                         | 0.11                   | 12.10                   | 325                    |
| 60             | 177.531                   | 0.280                   | 82                         | 0.17                   | 9.70                    | 325                    |
| 65             | 179.651                   | 0.280                   | 82                         | 0.07                   | 11.00                   | 325                    |
| 70             | 181.770                   | 0.280                   | 82                         | 0.04                   | 12.40                   | 325                    |
| 75             | 183.889                   | 0.280                   | 83                         | 0.03                   | 13.00                   | 325                    |
| 80             | 186.016                   | 0.270                   | 85                         | 0.06                   | 11.20                   | 325                    |
| 85             | 188.159                   | 0.270                   | 85                         | 0.06                   | 10.00                   | 325                    |
| 90             | 190.302                   | 0.270                   | 85                         | 0.06                   | 9.40                    | 325                    |
| 95             | 192.444                   | 0.270                   | 85                         | 0.13                   | 8.70                    | 325                    |
| 100            | 194.587                   | 0.240                   | 85                         | 0.23                   | 8.50                    | 350                    |
| 105            | 196.577                   | 0.180                   | 86                         | 0.53                   | 8.70                    | 400                    |
| 110            | 198.325                   | 0.180                   | 86                         | 0.71                   | 8.40                    | 400                    |
| 115            | 200.074                   | 0.160                   | 86                         | 0.84                   | 7.90                    | 425                    |
| 120            | 201.719                   | 0.130                   | 86                         | 1.06                   | 7.50                    | 475                    |
| 125            | 203.192                   | 0.130                   | 86                         | 1.04                   | 7.40                    | 475                    |
| 130            | 204.664                   | 0.130                   | 86                         | 1.02                   | 7.60                    | 475                    |
| 135            | 206.137                   | 0.130                   | 86                         | 0.99                   | 7.80                    | 475                    |
| 140            | 207.609                   | 0.130                   | 86                         | 0.74                   | 7.50                    | 475                    |
| 145            | 209.082                   | 0.140                   | 86                         | 0.89                   | 7.00                    | 450                    |
| 150            | 210.636                   | 0.100                   | 86                         | 1.34                   | 5.90                    | 525                    |
| 155            | 211.968                   | 0.110                   | 86                         | 1.39                   | 5.80                    | 500                    |
| 160            | 213.367                   | 0.110                   | 86                         | 1.54                   | 5.80                    | 500                    |
| 165            | 214.767                   | 0.110                   | 86                         | 1.48                   | 5.90                    | 500                    |
| 170            | 216.166                   | 0.110                   | 86                         | 1.56                   | 5.90                    | 500                    |
| 175            | 217.565                   | 0.110                   | 87                         | 1.61                   | 5.60                    | 500                    |
| 180            | 218.969                   | 0.100                   | 88                         | 2.16                   | 5.10                    | 525                    |
| 185            | 220.311                   | 0.100                   | 88                         | 2.21                   | 5.00                    | 525                    |
| 190            | 221.653                   | 0.100                   | 89                         | 2.21                   | 5.00                    | 525                    |
| 195            | 223.000                   | 0.100                   | 89                         | 1.97                   | 5.40                    | 525                    |
| 200            | 224.348                   | 0.090                   | 89                         | 2.04                   | 5.20                    | 550                    |
| 205            | 225.634                   | 0.090                   | 89                         | 2.11                   | 5.20                    | 550                    |
| 210            | 226.920                   | 0.090                   | 89                         | 2.26                   | 5.00                    | 550                    |
| 215            | 228.206                   | 0.090                   | 90                         | 2.24                   | 4.90                    | 550                    |



|     |         |       |    |      |      |     |
|-----|---------|-------|----|------|------|-----|
| 220 | 229.496 | 0.090 | 90 | 2.24 | 4.90 | 575 |
| 225 | 230.731 | 0.090 | 90 | 1.28 | 5.40 | 550 |
| 230 | 232.021 | 0.090 | 90 | 1.29 | 5.30 | 575 |
| 235 | 233.256 | 0.090 | 90 | 1.31 | 5.30 | 575 |
| 240 | 234.491 | 0.090 | 90 | 1.35 | 5.30 | 575 |
| 245 | 235.725 | 0.090 | 90 | 1.52 | 5.20 | 575 |
| 250 | 236.960 | 0.090 | 90 | 1.53 | 5.10 | 575 |
| 255 | 238.194 | 0.090 | 90 | 1.33 | 5.50 | 575 |
| 260 | 239.429 | 0.080 | 91 | 1.53 | 5.60 | 575 |
| 265 | 240.668 | 0.080 | 91 | 1.67 | 5.50 | 575 |
| 270 | 241.907 | 0.080 | 91 | 1.68 | 5.30 | 575 |
| 275 | 243.146 | 0.080 | 91 | 1.80 | 5.20 | 575 |
| 280 | 244.385 | 0.080 | 91 | 1.86 | 5.20 | 600 |
| 285 | 245.573 | 0.080 | 91 | 1.95 | 4.90 | 600 |
| 290 | 246.760 | 0.080 | 91 | 2.05 | 4.50 | 600 |
| 295 | 247.948 | 0.080 | 91 | 2.06 | 4.40 | 600 |
| 300 | 249.135 | 0.080 | 91 | 1.81 | 3.80 | 600 |
| 305 | 250.323 | 0.007 | 91 | 1.90 | 3.80 | 625 |
| 310 | 251.463 | 0.070 | 91 | 1.93 | 3.90 | 625 |
| 315 | 252.603 | 0.070 | 91 | 2.02 | 4.10 | 625 |
| 320 |         |       |    |      |      |     |





TABLE 2---RAW DATA

|             |                  |             |                  |
|-------------|------------------|-------------|------------------|
| CLIENT :    | Jotul            | TEST No.    | 1                |
| MODEL:      | F400             | DATE:       | 07-Apr-00        |
| *****       |                  |             |                  |
| METER CAL.  |                  | Wt. WOOD    |                  |
| FACTOR (Y)  | ----- 0.989      | BURNED (LB) | ----- 13.2 Lbs   |
| BAROMETRIC  |                  | WET, FUEL   |                  |
| PRESS. (Pb) | ----- 30.2 in Hg | MOISTURE %  | ----- 17.961 %   |
| LEAK RATE   |                  | Wt. PART.   |                  |
| POST (Lp)   | ----- 0.011 cfm  | COLLECTED   | ----- 1.1356 g   |
| WATER       |                  | METER       |                  |
| VOL. (V1c)  | ----- 138.1 ML   | VOLUME Vm   | ----- 94.603 mcf |
| TEST        |                  | HC MOLE     |                  |
| TIME (MIN)  | ----- 315 min    | FRACTION    | ----- 0.0132     |



TABLE 3 -----FIELD DATA AVERAGES

CLIENT :Jotul

TEST No. 1

MODEL: F400

DATE: 07-Apr-00

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|           |       |             |           |       |        |
|-----------|-------|-------------|-----------|-------|--------|
| AVG DELTA |       |             | AVG PRCNT |       |        |
| H         | ----- | 0.14 in H2O | CO        | ----- | 1.19 % |
| AVG METER |       |             | AVG PRCNT |       |        |
| TEMP. Tm  | ----- | 87 deg F    | CO2       | ----- | 6.27 % |
| AVG PPM   |       |             | AVG BAL   |       |        |
| SO2       | ----- | 489 PPM     | CO2/CO    | ----- | 5.27 % |



TABLE 4 ----- CALCULATIONS

CLIENT : Jotul

TEST No. 1

MODEL: F400

DATE: 07-Apr-00

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|                    |                             |                   |         |                          |
|--------------------|-----------------------------|-------------------|---------|--------------------------|
| STD SAMPLE         |                             | STACK GAS         |         |                          |
| VOL. Vm(std) ----- | 91.25 dscf                  | FLOW Qsd -----    | 383.985 | dscf/Hr<br>&<br>dscf/min |
|                    |                             |                   | 6.40    |                          |
| VOL. WATER         |                             | PARTICULATE       |         |                          |
| VAPOR Vw(std) ---- | 6.500 scf                   | CONCTR. Cs -----  | 0.0124  | g/dscf                   |
| PRCNT              |                             | PARTC. EMISS.     |         |                          |
| MSTR Bws -----     | 6.65 %                      | RATE E -----      | 4.78    | g/Hr                     |
| BURN               |                             | MOLES OF GAS      |         |                          |
| RATE BR -----      | 0.94 Kg/Hr                  | PER Lb WOOD Nt -- | 0.48    | Lb-mole/Lb               |
| CO EMISSION        |                             | PART. EMISS.      |         |                          |
| RATE -----         | 153.04 g/Hr                 | RATE -----        | 5.11    | g/Kgdry<br>fuel          |
|                    | &<br>163.51 g/Kgdry<br>fuel |                   |         |                          |



TABLE 5 ----- PROPORTIONAL RATE VARIATION

CLIENT : Jotul

TEST No. : 1

MODEL: F400

DATE: 07-Apr-00

\*\*\*\*\*

| TIME<br>INTEVAL<br>Ti | PPM<br>*<br>Vm | PROPRTN.<br>RATE VAR.<br>PR | PROPRTN<br>RATE VAR.<br>AVERAGE |
|-----------------------|----------------|-----------------------------|---------------------------------|
| 5                     | 658.0          | 97                          | 100                             |
| 10                    | 670.3          | 99                          |                                 |
| 15                    | 670.7          | 99                          |                                 |
| 20                    | 670.3          | 99                          |                                 |
| 25                    | 670.6          | 99                          |                                 |
| 30                    | 670.8          | 99                          |                                 |
| 35                    | 670.6          | 99                          |                                 |
| 40                    | 670.3          | 99                          |                                 |
| 45                    | 670.8          | 99                          |                                 |
| 50                    | 670.3          | 99                          |                                 |
| 55                    | 670.3          | 99                          |                                 |
| 60                    | 670.3          | 99                          |                                 |
| 65                    | 670.6          | 99                          |                                 |
| 70                    | 670.3          | 99                          |                                 |
| 75                    | 669.7          | 99                          |                                 |
| 80                    | 670.3          | 99                          |                                 |
| 85                    | 674.1          | 100                         |                                 |
| 90                    | 674.1          | 100                         |                                 |
| 95                    | 673.8          | 100                         |                                 |
| 100                   | 674.1          | 100                         |                                 |
| 105                   | 673.5          | 100                         |                                 |
| 110                   | 675.4          | 100                         |                                 |
| 115                   | 675.8          | 100                         |                                 |
| 120                   | 675.3          | 100                         |                                 |
| 125                   | 675.8          | 100                         |                                 |
| 130                   | 675.3          | 100                         |                                 |
| 135                   | 675.8          | 100                         |                                 |
| 140                   | 675.3          | 100                         |                                 |
| 145                   | 675.8          | 100                         |                                 |
| 150                   | 675.4          | 100                         |                                 |
| 155                   | 675.3          | 100                         |                                 |
| 160                   | 675.6          | 100                         |                                 |
| 165                   | 676.0          | 100                         |                                 |
| 170                   | 675.6          | 100                         |                                 |
| 175                   | 674.9          | 100                         |                                 |
| 180                   | 676.1          | 100                         |                                 |
| 185                   | 677.9          | 100                         |                                 |
| 190                   | 677.3          | 100                         |                                 |
| 195                   | 679.2          | 100                         |                                 |
| 200                   | 679.7          | 101                         |                                 |
| 205                   | 679.3          | 100                         |                                 |
| 210                   | 679.3          | 100                         |                                 |
| 215                   | 678.7          | 100                         |                                 |
| 220                   | 680.2          | 101                         |                                 |





|     |       |     |
|-----|-------|-----|
| 225 | 680.8 | 101 |
| 230 | 680.2 | 101 |
| 235 | 680.8 | 101 |
| 240 | 680.8 | 101 |
| 245 | 680.2 | 101 |
| 250 | 680.8 | 101 |
| 255 | 680.2 | 101 |
| 260 | 680.2 | 101 |
| 265 | 681.7 | 101 |
| 270 | 681.7 | 101 |
| 275 | 681.7 | 101 |
| 280 | 681.7 | 101 |
| 285 | 682.1 | 101 |
| 290 | 681.5 | 101 |
| 295 | 682.1 | 101 |
| 300 | 681.5 | 101 |
| 305 | 682.1 | 101 |
| 310 | 681.7 | 101 |
| 315 | 681.8 | 101 |
| 320 |       |     |
| 325 |       |     |



COMPUTER INPUT DATA SHEET #1

5,5106

Client: JOTUL U.S.A., INC.

Address: 400 RIVERSIDE STREET  
PORTLAND, ME 04104

4.78  
at .94 kg/h

Phone: 207-797-5912 Fax: 207-772-0523

Run No.: 1 Date of Test: 4-7-2000 Burn Rate: .936

Model No.: \_\_\_\_\_  min  min-1.25  fan

Stove Type:  Cat  Non Cat  Pellet  1.25-1.9  max  insert

Dry Gas Meter: Y Factor: .989 Post Leak Rate: .011 cfm Time: 315 min.  
(0.000) (Data Sheet #2) (.000) (Data Sheet #2) (000) (Data Sheet #2)

Dry Gas Meter Volume: \_\_\_\_\_ 94.603 cf ✓  
(00.000) (Data Sheet #2) 6.40 calc

Stack Flow: 7.372 dscfm Δ H: .138 in. H<sub>2</sub>O  
(00.000) (Data Sheet #2) (.000) (Data Sheet #2)

Barometric Pressure: \_\_\_\_\_ 30.20 in. Hg  
(00.00) (Data Sheet #2)

H<sub>2</sub>O Captured: \_\_\_\_\_ 138.1 g  
(00.0) (Data Sheet #3)

Total Particulate Catch: \_\_\_\_\_ 1.1356 g  
(0.0000) (Data Sheet #6)

Flue Gas Moisture: \_\_\_\_\_ 6.6567 %  
(00.000) (Data Sheet #7)

Particulate Emission: \_\_\_\_\_ .1922 gr/dscf  
(0.0000) (Data Sheet #7)

Ambient Moisture: \_\_\_\_\_ 1.3 %  
(0.00) (Data Sheet #8)

Stove Weight: \_\_\_\_\_ — lbs  
(000) (Data Sheet #8)

Total Fuel Consumed During Burn: \_\_\_\_\_ 13.2 lbs  
(00.0) (Data sheet #8)

Fuel Higher Heating Value (dry): \_\_\_\_\_ — BTU/lb  
(0000) (Data Sheet #8)

Fuel % Moisture (dry): 21.893 % (wet): 17.961 %  
(00.00) (Data Sheet #10)

Stack Static Pressure: \_\_\_\_\_ -.036 in. H<sub>2</sub>O  
(0.000) (Data Sheet #12)

Temperature (Average Room) Combustion Air: \_\_\_\_\_ 75 °F  
(00) Data Sheet #14)

Stove Temperature Change: \_\_\_\_\_ -74.8 °F  
(00.0) (Data Sheet #14)



METER BOX DATA SHEET PAGE # 2

Page: 1 of 3

UNIT: F400 RUN: 1 DATE: 47.00

Meter Box: 5H Y Factor: .989

Leak checks: 15 " Hg @ .020 cfm      " Hg @      cfm

15 " Hg @ .011 cfm      " Hg @      cfm

Inject SO<sub>2</sub> @ 100 cc/min. Nozzle: Probe @ 3/8" od Initial Volume: 1.500

95

| ROTO PRESS: <u>.15</u> |      |               | SAMPLING RATIO: <u>26</u> : 1 |             |                |             | BP: <u>30.20</u> |                  |           |  |
|------------------------|------|---------------|-------------------------------|-------------|----------------|-------------|------------------|------------------|-----------|--|
| MIN                    | TIME | METER READING | SAMPLE MDCF                   | STACK DSCFM | DELTA H        | METER TEMP  | SO2 PPM          | ROTO TEMP        | PUMP VACC |  |
| 0                      | 1235 | 158.000       | —                             | 7.749       | .15            | 80          | 450              | 80               | 1.0       |  |
| 5                      | 40   | 159.500       | —                             | 8.175       | .16            | 82          | 425              | 82               | 3.0       |  |
| 10                     | 45   | 167.121       | 167.121                       | 8.175       | .16            | 82          | 425              | 82               | 1.0       |  |
| 15                     | 50   | 162.743       | 162.743                       | 7.721       | .14            | 82          | 450              | 82               | 1.0       |  |
| 20                     | 55   | 164.274       | 164.274                       | 7.314       | .13            | 82          | 475              | 82               | 1.0       |  |
| 25                     | 1300 | 165.725       | 165.725                       | 6.949       | .12            | 82          | 500              | 82               | 1.0       |  |
| 30                     | 05   | 167.104       | 167.104                       | 6.618       | .11            | 82          | 525              | 82               | 1.0       |  |
| 35                     | 10   | 168.417       | 168.417                       | 6.949       | .12            | 82          | 500              | 82               | 1.0       |  |
| 40                     | 15   | 169.795       | 169.795                       | 6.949       | .12            | 82          | 500              | 82               | 1.0       |  |
| 45                     | 20   | 171.174       | 171.174                       | 10.690      | .28            | 82          | 325              | 82               | 3.0       |  |
| 50                     | 25   | 173.293       | 173.293                       | 10.690      | .28            | 82          | 325              | 82               | 3.0       |  |
| 55                     | 30   | 175.412       | 175.412                       | 10.690      | .28            | 82          | 325              | 82               | 3.0       |  |
| ROTO PRESS: <u>.15</u> |      |               | TOTALS:                       |             | <u>98.689</u>  | <u>2.05</u> | <u>982</u>       | BP: <u>30.20</u> |           |  |
| 60                     | 1335 | 177.531       | 177.531                       | 10.690      | .28            | 82          | 325              | 82               | 3.0       |  |
| 65                     | 40   | 179.651       | 179.651                       | 10.690      | .28            | 82          | 325              | 82               | 3.0       |  |
| 70                     | 45   | 181.770       | 181.770                       | 10.690      | .28            | 82          | 325              | 82               | 3.0       |  |
| 75                     | 50   | 183.889       | 183.889                       | 10.670      | .28            | 83          | 325              | 83               | 3.0       |  |
| 80                     | 55   | 186.016       | 186.016                       | 10.631      | .27            | 85          | 325              | 85               | 3.0       |  |
| 85                     | 1400 | 188.159       | 188.159                       | 10.631      | .27            | 85          | 325              | 85               | 3.0       |  |
| 90                     | 05   | 190.302       | 190.302                       | 10.631      | .27            | 85          | 325              | 85               | 3.0       |  |
| 95                     | 10   | 192.444       | 192.444                       | 10.631      | .27            | 85          | 325              | 85               | 3.0       |  |
| 100                    | 15   | 194.587       | 194.587                       | 9.872       | .24            | 85          | 350              | 85               | 3.0       |  |
| 105                    | 20   | 196.577       | 196.577                       | 8.622       | .18            | 86          | 400              | 86               | 2.0       |  |
| 110                    | 25   | 198.325       | 198.325                       | 8.622       | .18            | 86          | 400              | 86               | 2.0       |  |
| 115                    | 30   | 200.074       | 200.074                       | 8.115       | .16            | 86          | 425              | 86               | 2.0       |  |
|                        |      |               | TOTALS:                       |             | <u>120.495</u> | <u>2.96</u> | <u>1012</u>      | MAX VACC =       |           |  |
| TOTAL Cu Ft.           |      |               | TOTALS:                       |             | <u>219.164</u> | <u>5.01</u> | <u>1994</u>      | AVG. BP:         |           |  |





METER BOX DATA SHEET PAGE # 2

Page: 2 of 3

UNIT: F400 RUN: 1 DATE: 4-7-00

Meter Box: SH Y Factor: .989

Leak checks: 15 " Hg @ .020 cfm      " Hg @      cfm

15 " Hg @ .011 cfm      " Hg @      cfm

Inject SO<sub>2</sub> @ 100 cc/min. Nozzle : Probe @ 3/8" od Initial Volume: 1,500

| ROTO: PRESS: <u>.14</u> |      | SAMPLING RATIO: <u>26</u> : 1 |             |             |               |                | BP: <u>30,20</u> |                  |           |  |
|-------------------------|------|-------------------------------|-------------|-------------|---------------|----------------|------------------|------------------|-----------|--|
| MIN                     | TIME | METER READING                 | SAMPLE MDCF | STACK DSCFM | DELTA H       | METER TEMP     | SO2 PPM          | ROTO TEMP        | PUMP VACC |  |
| 120                     | 1435 | 201.719                       | 201.719     | 7.261       | .13           | 86             | 475              | 86               | 2.0       |  |
| 125                     | 40   | 203.192                       | 203.192     | 7.261       | .13           | 86             | 475              | 86               | 2.0       |  |
| 130                     | 45   | 204.664                       | 204.664     | 7.261       | .13           | 86             | 475              | 86               | 2.0       |  |
| 135                     | 50   | 206.137                       | 206.137     | 7.261       | .13           | 86             | 475              | 86               | 2.0       |  |
| 140                     | 55   | 207.609                       | 207.609     | 7.261       | .13           | 86             | 475              | 86               | 2.0       |  |
| 145                     | 1500 | 209.082                       | 209.082     | 7.664       | .14           | 86             | 450              | 86               | 2.0       |  |
| 150                     | 05   | 210.636                       | 210.636     | 6.569       | .10           | 86             | 525              | 86               | 2.0       |  |
| 155                     | 10   | 211.968                       | 211.968     | 6.898       | .11           | 86             | 500              | 86               | 2.0       |  |
| 160                     | 15   | 213.367                       | 213.367     | 6.898       | .11           | 86             | 500              | 86               | 2.0       |  |
| 165                     | 20   | 214.767                       | 214.767     | 6.898       | .11           | 86             | 500              | 86               | 2.0       |  |
| 170                     | 25   | 216.166                       | 216.166     | 6.898       | .11           | 86             | 500              | 86               | 2.0       |  |
| 175                     | 30   | 217.565                       | 217.565     | 6.885       | .11           | 87             | 500              | 87               | 2.0       |  |
| ROTO PRESS: <u>.14</u>  |      | TOTALS:                       |             |             | <u>85.015</u> | <u>1.44</u>    | <u>1033</u>      | BP: <u>30,20</u> |           |  |
| 180                     | 1535 | 218.969                       | 218.969     | 6.545       | .10           | 88             | 525              | 88               | 2.0       |  |
| 185                     | 40   | 220.311                       | 220.311     | 6.545       | .10           | 88             | 525              | 88               | 2.0       |  |
| 190                     | 45   | 221.653                       | 221.653     | 6.533       | .10           | 89             | 525              | 89               | 2.0       |  |
| 195                     | 50   | 223.000                       | 223.000     | 6.533       | .10           | 89             | 525              | 89               | 2.0       |  |
| 200                     | 55   | 224.348                       | 224.348     | 6.236       | .09           | 89             | 550              | 89               | 1.0       |  |
| 205                     | 1600 | 225.634                       | 225.634     | 6.236       | .09           | 89             | 550              | 89               | 1.0       |  |
| 210                     | 05   | 226.920                       | 226.920     | 6.236       | .09           | 89             | 550              | 89               | 1.0       |  |
| 215                     | 10   | 228.206                       | 228.206     | 6.225       | .09           | 90             | 550              | 90               | 1.0       |  |
| 220                     | 15   | 229.496                       | 229.496     | 5.954       | .09           | 90             | 575              | 90               | 1.0       |  |
| 225                     | 20   | 230.731                       | 230.731     | 6.225       | .09           | 90             | 550              | 90               | 1.0       |  |
| 230                     | 25   | 232.021                       | 232.021     | 5.954       | .09           | 90             | 575              | 90               | 1.0       |  |
| 235                     | 30   | 233.256                       | 233.256     | 5.954       | .09           | 90             | 575              | 90               | 1.0       |  |
|                         |      |                               |             | TOTALS:     | <u>75.176</u> | <u>1.12</u>    | <u>1071</u>      | MAX VACC =       |           |  |
| TOTAL Cu Fl.            |      |                               |             |             | TOTALS:       | <u>160.191</u> | <u>2.56</u>      | <u>2104</u>      | AVG. BP:  |  |





METER BOX DATA SHEET PAGE # 2

Page: 3 of 3

UNIT: F400 RUN: 1 DATE: 4-7-00

Meter Box: 5H Y Factor: .989

Leak checks: 15 " Hg @ .020 cfm / " Hg @ / cfm

15 " Hg @ .011 cfm / " Hg @ / cfm

Inject SO<sub>2</sub> @ 100 cc/min. Nozzle: Probe @ 3/8" od Initial Volume: 1.500

| ROTO: PRESS: <u>.14</u> |      |               | SAMPLING RATIO: <u>24</u> : 1 |             |         |            | BP: <u>30.20</u> |                |           |  |
|-------------------------|------|---------------|-------------------------------|-------------|---------|------------|------------------|----------------|-----------|--|
| MIN                     | TIME | METER READING | SAMPLE MDCF                   | STACK DSCFM | DELTA H | METER TEMP | SO2 PPM          | ROTO TEMP      | PUMP VACC |  |
| 240                     | 1635 | 234.491       | 234.491                       | 5.954       | .09     | 90         | 575              | 90             | 1.0       |  |
| 245                     | 40   | 235.725       | 235.725                       | 5.954       | .09     | 90         | 575              | 90             | 1.0       |  |
| 250                     | 45   | 236.960       | 236.960                       | 5.954       | .09     | 90         | 575              | 90             | 1.0       |  |
| 255                     | 50   | 238.194       | 238.194                       | 5.954       | .09     | 90         | 575              | 90             | 1.0       |  |
| 260                     | 55   | 239.429       | 239.429                       | 5.943       | .08     | 91         | 575              | 91             | 1.0       |  |
| 265                     | 1700 | 240.668       | 240.668                       | 5.943       | .08     | 91         | 575              | 91             | 1.0       |  |
| 270                     | 05   | 241.907       | 241.907                       | 5.943       | .08     | 91         | 575              | 91             | 1.0       |  |
| 275                     | 10   | 243.146       | 243.146                       | 5.943       | .08     | 91         | 575              | 91             | 1.0       |  |
| 280                     | 15   | 244.385       | 244.385                       | 5.696       | .08     | 91         | 600              | 91             | 1.0       |  |
| 285                     | 20   | 245.573       | 245.573                       | 5.696       | .08     | 91         | 600              | 91             | 1.0       |  |
| 290                     | 25   | 246.760       | 246.760                       | 5.696       | .08     | 91         | 600              | 91             | 1.0       |  |
| 295                     | 30   | 247.948       | 247.948                       | 5.696       | .08     | 91         | 600              | 91             | 1.0       |  |
| ROTO PRESS: <u>.14</u>  |      |               | TOTALS: 70.372                |             | 1.00    | 1088       | BP.: 30.20       |                |           |  |
| 300                     | 1735 | 249.135       | 249.135                       | 5.696       | .08     | 91         | 600              | 91             | 1.0       |  |
| 305                     | 40   | 250.323       | 250.323                       | 5.468       | .07     | 91         | 625              | 91             | 1.0       |  |
| 310                     | 45   | 251.463       | 251.463                       | 5.468       | .07     | 91         | 625              | 91             | 1.0       |  |
| 315                     | 50   | 252.603       | 252.603                       | 5.468       | .07     | 91         | 625              | 91             | 1.0       |  |
| 320                     |      |               |                               |             |         |            |                  |                |           |  |
| 325                     |      |               |                               |             |         |            |                  |                |           |  |
| 330                     |      |               |                               |             |         |            |                  |                |           |  |
| 335                     |      |               |                               |             |         |            |                  |                |           |  |
| 340                     |      |               |                               |             |         |            |                  |                |           |  |
| 345                     |      |               |                               |             |         |            |                  |                |           |  |
| 350                     |      |               |                               |             |         |            |                  |                |           |  |
| 355                     |      |               |                               |             |         |            | <u>÷64</u>       |                |           |  |
| TOTALS:                 |      |               |                               | 471.827     | 8.860   | 5550       | MAX VACC =       |                | 3.0       |  |
| TOTAL Cu Ft.            |      | 94.603        | TOTALS:                       |             | 7.372   | .138       | 87               | AVG. BP: 30.20 |           |  |

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**PARTICULATE CATCH / MOISTURE DATA SHEET # 3**

UNIT: F400 RUN: 1 DATE: 4-7-00

| SCALE CHECK | LEVEL | ZEROED |
|-------------|-------|--------|
| INITIAL :   | ✓     | ✓      |
| FINAL :     | ✓     | ✓      |

| SCALE   | WEIGHT |
|---------|--------|
| 295.0 g | 295.0  |
| 590.0 g | 590.0  |
| 885.0 g | 885.0  |

| IMPINGER     | #1      | #2    | #3    | #4     |
|--------------|---------|-------|-------|--------|
| FINAL WT     | 703.7   | 600.1 | 516.1 | 888.7  |
| INITIAL WT   | 593.7   | 593.7 | 513.9 | 869.2  |
| NET WT GRAMS | 110.0 ✓ | 6.4 ✓ | 2.2 ✓ | 19.5 ✓ |

TOTAL CATCH: 138.1 GRAMS H<sub>2</sub>O

**FRONT HALF**

|              |         |  |
|--------------|---------|--|
| FILTER #     | 18F     |  |
| FINAL WT g   | .8680 ✓ |  |
| INITIAL WT g | .6690 ✓ |  |
| NET WT g     | .1990 ✓ |  |

|               |            |
|---------------|------------|
| BEAKER #      | 51         |
| DESC.         | ACETONE    |
| FINAL WT g    | 105.0507 ✓ |
| INITIAL WT g  | 104.8756 ✓ |
| NET WT g      | .1751 ✓    |
| VOL. DESC. ml | 125        |

**BACK HALF**

|              |         |  |
|--------------|---------|--|
| FILTER #     | 18B     |  |
| FINAL WT g   | .5570 ✓ |  |
| INITIAL WT g | .4300 ✓ |  |
| NET WT g     | .1270 ✓ |  |

| BEAKER #     | 52         | 53         | 54               | 55               |         |
|--------------|------------|------------|------------------|------------------|---------|
| DESC.        | ACETONE    | METHCHLOR  | H <sub>2</sub> O | H <sub>2</sub> O |         |
| FINAL WT g   | 107.8619 ✓ | 105.8394 ✓ | 107.3907 ✓       | 93.5941 ✓        |         |
| INITIAL WT g | 107.5006 ✓ | 105.7378 ✓ | 107.3124 ✓       | 93.4958 ✓        |         |
| NET WT g     | .3613 ✓    | .1016 ✓    | .0785 ✓          | .0983 ✓          | .1768 ✓ |
| VOL. DESC ml | 200        | 75         | 125              | 125              | (350)   |





**WOODSTOVE DATA SHEET #4-1  
INITIAL FILTER WEIGHTS (TARE WEIGHTS)**

Into Dessicator: Date 10-28-99 Time: 1725 By: ME  
 Manufacturer: S+S Grade: #25 GLASS Front Size: 11CM Lot No.: ZB921  
 Back Size: 8.2CM Lot No.: ZB911

| FILTER # | DATE: <u>11-1</u> |      | DATE: <u>11-4</u> |      | DATE: _____      |      |
|----------|-------------------|------|-------------------|------|------------------|------|
|          | FIRST WEIGHT      | TIME | SECOND WEIGHT     | TIME | THIRD WEIGHT     | TIME |
| 11B      | .4291             | 1911 | .4291             | 1818 | JOTUL #30B R#4   |      |
| 12B      | .4316             | 1912 | .4313             | 1819 | JOTUL #30BIT R#1 |      |
| 13B      | .4299             | 1913 | .4298             | 1820 | JOTUL #30BIT R#2 |      |
| 14B      | .4306             | 1914 | .4306             | 1821 | JOTUL #30BIT R#3 |      |
| 15B      | .4313             | 1915 | .4313             | 1822 | JOTUL #30BIT R#4 |      |
| 16B      | .4319             | 1916 | .4315             | 1822 |                  |      |
| 17B      | .4278             | 1916 | .4277             | 1823 |                  |      |
| 18B      | .4302             | 1917 | .4300             | 1824 | JOTUL F400 R#1   |      |
| 19B      | .4288             | 1918 | .4285             | 1825 | JOTUL F400 R#2   |      |
| 20B      | .4340             | 1919 | .4340             | 1826 | JOTUL F400 R#3   |      |

|     |        |      |       |      |                  |  |
|-----|--------|------|-------|------|------------------|--|
| 11F | .66610 | 1928 | .6659 | 1835 | JOTUL #30B R#4   |  |
| 12F | .6837  | 1929 | .6833 | 1836 | JOTUL #30BIT R#1 |  |
| 13F | .6707  | 1930 | .6704 | 1837 | JOTUL #30BIT R#2 |  |
| 14F | .6719  | 1931 | .6722 | 1838 | JOTUL #30BIT R#3 |  |
| 15F | .6673  | 1932 | .6674 | 1839 | JOTUL #30BIT R#4 |  |
| 16F | .6809  | 1933 | .6806 | 1840 |                  |  |
| 17F | .6657  | 1934 | .6654 | 1840 |                  |  |
| 18F | .6693  | 1935 | .6690 | 1841 | JOTUL F400 R#1   |  |
| 19F | .6744  | 1935 | .6745 | 1842 | JOTUL F400 R#2   |  |
| 20F | .6654  | 1936 | .6655 | 1843 | JOTUL F400 R#3   |  |

Checked by: [Signature] Date: 11-4-99 Time: 1905

**BALANCE ROOM ENVIRONMENTAL CONDITIONS**

| DATE | TIME | BY | WB | DB | % RH |
|------|------|----|----|----|------|
| 11-1 | 1815 | ME | 5  | 73 | 46   |
| 11-4 | 1805 | ME | 5  | 76 | 46   |



## BEAKER TARE WEIGHTS DATA SHEET #4-2

Into Dessicator:    Date: 1-18-2000    Time: 0700    By: DKW

| BEAKER # | FIRST WEIGHT         | TIME | SECOND WEIGHT  | TIME | THIRD WEIGHT         | TIME                |
|----------|----------------------|------|----------------|------|----------------------|---------------------|
|          | DATE: <u>1-21-00</u> |      | BY: <u>DKW</u> |      | DATE: <u>1-23-00</u> |                     |
| 41       | 105.4903             | 2120 | 105.4906       | 1215 |                      |                     |
| 42       | 104.6708             | 2121 | 104.6712       | 1217 | } TOTAL #3CBI<br>R#3 |                     |
| 43       | 107.3607             | 2122 | 107.3609       | 1218 |                      |                     |
| 44       | 107.7970             | 2123 | 107.7966       | 1219 |                      |                     |
| 45       | 94.9398              | 2124 | 94.9403        | 1220 |                      |                     |
| 46       | 106.0518             | 2125 | 106.0513       | 1221 |                      |                     |
| 47       | 107.0394             | 2126 | 107.0390       | 1222 | } TOTAL #3CBI<br>R#4 |                     |
| 48       | 97.7533              | 2127 | 97.7534        | 1224 |                      |                     |
| 49       | 108.3605             | 2128 | 108.3602       | 1225 |                      |                     |
| 50       | 96.5368              | 2129 | 96.5364        | 1226 |                      |                     |
| 51       | 104.8760             | 2129 | 104.8756       | 1227 |                      | } TOTAL F400<br>R#1 |
| 52       | 107.5011             | 2130 | 107.5006       | 1228 |                      |                     |
| 53       | 105.7382             | 2131 | 105.7378       | 1229 |                      |                     |
| 54       | 107.3129             | 2132 | 107.3124       | 1229 |                      |                     |
| 55       | 93.4956              | 2133 | 93.4958        | 1230 |                      |                     |

**BALANCE ROOM ENVIRONMENTAL CONDITIONS**

| DATE | TIME | BY  | WB | DB | % RH | Checked by:                                |
|------|------|-----|----|----|------|--|
| 1-21 | 2115 | DKW | }  | 77 | 41   | DKW  |
| 1-23 | 1210 | DKW |    | 73 | 44   | Date: <u>1-23-00</u><br>Time: <u>17:40</u> |





WOODSTOVE DATA SHEET # 4-3 : CONSTANT WEIGHTS

F400

RUN: 1

DATE: 4-7-00

UNIT:

| Beaker # | Date | Time | By  | First Weight | Date | Time | By  | Second Weight | Date | Time | By  | Third Weight | Date | Time | By  |
|----------|------|------|-----|--------------|------|------|-----|---------------|------|------|-----|--------------|------|------|-----|
| 51       | 4-8  | 0900 | JKW | 105.0511     | 4-9  | 1757 | JKW | 105.0507      | 4-10 | 1336 | JKW |              |      |      |     |
| 52       | 4-8  | 0900 | JKW | 107.8624     | 4-9  | 1758 | JKW | 107.8619      | 4-10 | 1337 | JKW |              |      |      |     |
| 53       | 4-8  | 2030 | JKW | 105.8397     | 4-10 | 1338 | JKW | 105.8389      | 4-10 | 1758 | JKW | 105.8394     | 4-11 | 1154 | JKW |
| 54       | 4-8  | 0900 | JKW | 107.3912     | 4-9  | 1759 | JKW | 107.3909      | 4-10 | 1339 | JKW |              |      |      |     |
| 55       | 4-8  | 0900 | JKW | 93.5941      | 4-9  | 1800 | JKW | 93.5941       | 4-10 | 1340 | JKW |              |      |      |     |

| Filter # | Date | Time | By  | First Weight | Date | Time | By  | Second Weight | Date | Time | By  | Third Weight | Date | Time | By |
|----------|------|------|-----|--------------|------|------|-----|---------------|------|------|-----|--------------|------|------|----|
| 18F      | 4-7  | 1825 | JKW | 8679         | 4-8  | 2053 | JKW | 8680          | 4-9  | 1801 | JKW |              |      |      |    |
| 18B      | 4-7  | 1825 | JKW | 5573         | 4-8  | 2054 | JKW | 5570          | 4-9  | 1801 | JKW |              |      |      |    |

SCALE ROOM ENVIRONMENTAL CONDITIONS

| Weighing Session | Date | Time | By  | WB | DB | %RH |
|------------------|------|------|-----|----|----|-----|
| 1                | 4-8  | 2050 | JKW |    | 78 | 48  |
| 2                | 4-9  | 1755 | JKW |    | 70 | 47  |
| 3                | 4-10 | 1335 | JKW |    | 78 | 49  |
| 4                | 4-10 | 1755 | JKW |    | 78 | 49  |

| Weighing Session | Date | Time | By  | WB | DB | %RH |
|------------------|------|------|-----|----|----|-----|
| 5                | 4-11 | 1150 | JKW |    | 78 | 48  |
| 6                |      |      |     |    |    |     |
| 7                |      |      |     |    |    |     |
| 8                |      |      |     |    |    |     |



### BLANK PROCESSING DATA SHEET # 5

UNIT: F400 RUN: 1 DATE: 4-7-2000

BLANKS DONE: 12-27-99

| BEAKER       | A              | B             | C            |
|--------------|----------------|---------------|--------------|
|              | 200 ml ACETONE | 75 ml DICHLOR | 200 ml WATER |
|              | FISHER OPTIMA  | FISHER OPTIMA |              |
|              | LOT #          | LOT #         |              |
| FINAL WEIGHT | 108.9011       | 106.3073      | 106.9666     |
| TARE WEIGHT  | 108.9003       | 106.3062      | 106.9651     |
| NET WEIGHT   | .0008          | .0011         | .0015        |

TARE BEAKERS INTO DESC: TIME: 11:30 DATE: 12-20-99

DATE: 1222 BY: NW DATE: 1223 BY: NW DATE: \_\_\_\_\_ BY: \_\_\_\_\_

| BEAKER | 1 ST WT  | TIME | 2 ND WT  | TIME | 3 RD WT | TIME |
|--------|----------|------|----------|------|---------|------|
| A      | 108.8999 | 1940 | 108.9003 | 1948 | ✓       |      |
| B      | 106.3058 | 1941 | 106.3062 | 1949 | ✓       |      |
| C      | 106.9647 | 1942 | 106.9651 | 1950 | ✓       |      |

FINAL BEAKERS INTO DESC: TIME: 1330 DATE: 12-24-99

DATE: 1224 BY: NW DATE: 1225 BY: NW DATE: 1227 BY: NW

| BEAKER | 1 ST WT  | TIME | 2 ND WT  | TIME | 3 RD WT  | TIME   |
|--------|----------|------|----------|------|----------|--------|
| A      | 108.8999 | 2021 | 108.9016 | 1816 | 108.9011 | 1224 ✓ |
| B      | 106.3061 | 2022 | 106.3077 | 1817 | 106.3073 | 1225 ✓ |
| C      | 106.9643 | 2023 | 106.9670 | 1818 | 106.9666 | 1226 ✓ |

#### TARE QC

| DATE  | TIME | BY | WB | DB | %  |
|-------|------|----|----|----|----|
| 12-22 | 1935 | NW | }  | 77 | 47 |
| 12-23 | 1945 | NW |    | 75 | 48 |
|       |      |    | }  |    |    |
|       |      |    |    |    |    |

#### FINAL QC

| DATE | TIME | BY | WB | DB | %  |
|------|------|----|----|----|----|
| 1224 | 1945 | NW | }  | 76 | 45 |
| 1225 | 1740 | NW |    | 75 | 38 |
| 1227 | 1210 | NW | }  | 76 | 46 |
|      |      |    |    |    |    |





# NET PARTICULATE CATCH CALCULATION DATA SHEET #6

UNIT : F400 RUN : 1 DATE : 4-7-2000

## BLANK CALCULATIONS

Acetone :  $\frac{.0008 \text{ g}}{200 \text{ ml}} = .000004 \text{ g/ml}$   
 Dichloromethane :  $\frac{.0011 \text{ g}}{75 \text{ ml}} = .000015 \text{ g/ml}$   
 Distilled Water :  $\frac{.0015 \text{ g}}{200 \text{ ml}} = .000008 \text{ g/ml}$

## FRONT HALF CATCH

FILTERS :  $\frac{.1990 \text{ g}}{\text{Total Catch}} - \frac{1}{\text{\# of Filters}} (.0000 \text{ g}) = .1990 \text{ g}$

BEAKERS :  $\frac{.1751 \text{ g}}{\text{Total Catch}} - \frac{125 \text{ ml Acetone}}{\text{ml Acetone}} (.000004 \text{ g}) = .1746 \text{ g}$

TOTAL FRONT HALF CATCH : .3736 g

## BACK HALF CATCH

FILTERS :  $\frac{.1270 \text{ g}}{\text{Total Catch}} - \frac{1}{\text{\# of Filters}} (.0000 \text{ g}) = .1270 \text{ g}$

BEAKERS :  
 Acetone :  $\frac{.3613 \text{ g}}{\text{Total Catch}} - \frac{200 \text{ ml Acetone}}{\text{ml Acetone}} (.000004 \text{ g}) = .3605 \text{ g}$

Extract :  $\frac{.1016 \text{ g}}{\text{Total Catch}} - \frac{75 \text{ ml Dichloromethane}}{\text{ml Dichloromethane}} (.000015 \text{ g}) = .1005 \text{ g}$

Water :  $\frac{.1768 \text{ g}}{\text{Total Catch}} - \frac{350 \text{ ml Water}}{\text{ml Water}} (.000008 \text{ g}) = .1740 \text{ g}$

TOTAL BACK HALF CATCH : .7620 g

TOTAL CATCH : 1.1356 g

% FRONT HALF : 32.90 %



# CALCULATIONS DATA SHEET # 7

UNIT: F400 RUN: 1 DATE: 4-7-2000

$$1) Vm (std) = \frac{(94.603 \text{ Vm})(17.64) (0.989 \text{ mcf}) (30.20 \text{ " Hg} + \frac{138 \text{ " H}_2\text{O}}{13.6})}{(547 \text{ TmA})} = \frac{91.1517}{000.0000} \text{ dscf}$$

$$2) Vw (std) = (0.04707) (138.1 \text{ ml H}_2\text{O}) = \frac{6.5004}{00.0000} \text{ scf}$$

$$3) Asw = \frac{(6.5004 \text{ scf})}{(6.5004 \text{ scf} + 91.1517 \text{ dscf})} = \frac{0.0666}{.0000} \text{ Bws} \times 100 = \frac{6.6567}{00.0000} \% \text{ H}_2\text{O}$$

$$4) Cs = \frac{(1.1356 \text{ g.})}{(91.1517 \text{ dscf})} (15.43) = \frac{.1922}{0.0000} \text{ gr / dscf}$$

$$5) \text{ Estimated g / hr} = \frac{(1.1356 \text{ g.})}{(91.1517 \text{ dscf})} (7.372 \text{ dscfm}) (60) = \frac{5.5166}{00.0000} \text{ g / hr}$$

|   |                             |
|---|-----------------------------|
| Vm = total cubic feet pulled on meter box during test                 | (000.000 Vm)                |
| mcf = meter correction factor ( Y factor ) of meter box used for test | (0.000 mcf)                 |
| " Hg = average barometric pressure during test                        | (00.00 " Hg)                |
| " H <sub>2</sub> O = average delta H for test                         | ( .000 " H <sub>2</sub> O)  |
| TmA = average meter temperature for test in degrees Absolute          | (000 TmA)                   |
| ml H <sub>2</sub> O = total water caught during test                  | (000.0 ml H <sub>2</sub> O) |
| g. = total particulate catch for test                                 | (00.0000 g.)                |
| dscfm = average stack flow during test                                | (00.000 dscf)               |





### TEST DATA SHEET # 8

UNIT: F400 RUN: 1 DATE: 4-7-00

Test Chamber Air Velocity Start: 0 Stop: 0 Avg.: 0

Wet Bulb / Dry Bulb Pre: WB: 60 DB: 76 = 38 % RH 1.2 % H<sub>2</sub>O

Post: WB: 64 DB: 81 = 38 % RH 1.4 % H<sub>2</sub>O

Average: 38 %RH 1.3 % H<sub>2</sub>O

Empty Stove Weight (lbs): ✓ w/ stack & oil seal: Wet: ✓ Dry: 390.0

Kindling Weight (lbs): Paper: 2 Wood: 3.0

Preburn Fuel Weight: 11.0 + 13.5 + 13.8 + 2.8 Total: 41.1

Kindling & Preburn Fuel Weight (wood only) (lbs): Total: 44.1

Coal Bed Wt Range (lbs): 3.3 - 2.7 Scale: 393.3 - 392.7

Upper: .25 x fuel weight: Always round DOWN to nearest tenth

Lower: .20 x fuel weight: Always round UP to nearest tenth Actual Coal Bed Weight: 3.1

Maximum Coal Bed Removal (lbs):  $((\frac{3.3}{\text{Upper}} + \frac{2.7}{\text{Lower}}) \div 2) \cdot 25 = \underline{2.7}$

Test Fuel (.75" x 1.5" x 5" spacers) = 20 pcs

| Dimensions | Length in inches | No. Pcs | Weight in lbs | % of Load |
|------------|------------------|---------|---------------|-----------|
| 2" x 4"    | 13               | 3       | 5.2           | 39.4      |
| 4" x 4"    | 13               | 2       | 8.0           | 60.6      |

Test Fuel Weight: 13.2 lbs

Estimated Dry Burn Rate: 2.371

$$\frac{13.2 - (13.2 \times .17961)}{2.2046} \times \frac{60}{315} = \underline{.936} \text{ kg/hr}$$

Estimated BTU's/hr:  $19,140 \times \frac{63}{100} \times \frac{.936}{\text{DBR}} = \underline{11286.48} \text{ BTU's/hr}$

EPA Default Efficiencies: Non-cat: 63 Cat: 72 Pellet: 78

295 = .99



# WOOD STOVE OPERATING DATA PAGE #9

Unit : F 400 Run : 1 Date : 4-7-00

FIRE STARTED: 0815

## WARM UP AND PREBURN:

PRIMARY AIR : Set wide open for all warm-up / preburn fuel charges. Then set to 1/16" at start of preburn.

SECONDARY AIR : N/A CAT BYPASS : N/A

## CHARCOAL BED PREPARATION :

Raked and leveled prior to each warm-up / preburn charge. At 1 1/2 min. prior to loading last fuel, raked and leveled. In stove 40 sec.

## TEST:

DOOR wide open during loading 1 min. 0 sec.

PRIMARY AIR : Opened full for first 5 min., then set to run setting of 1/16".

SECONDARY AIR : N/A CAT BYPASS : N/A

## FAN:

ON / ~~OFF~~ during warm-up

ON / ~~OFF~~ during preburn

ON / ~~OFF~~ first        minutes of test

ON / ~~OFF~~ balance of test run

Fan speed set at N/A

WOOD DATA: KINDLING: A mix of the grades listed below:

|          | SIZE | MILL         | GRADE          | SPECIES      |
|----------|------|--------------|----------------|--------------|
| PREBURN: | 2x4  | Manke/Tacoma | Std. or better | s. grn D fir |
| TEST:    | 2x4  | Packwood     | # 2 or better  | s. grn D fir |
|          | 4x4  | Packwood     | # 2 or better  | s. grn D fir |

PELLET FUEL MANUFACTURER : N/A BRAND : N/A

## All Grades WCLB rules:

## WARM UP INFORMATION:

All pre-burn / warm up fuel pieces were either 16 or 12 inches.

1st warm up / pre-burn fuel charge (11.0 lbs.) added at 0825

2nd warm up / pre-burn fuel charge (13.5 lbs.) added at 0925

3rd warm up / pre-burn fuel charge (13.8 lbs.) added at 1020

4th warm up / pre-burn fuel charge (2.8 lbs.) added at 1130

5th warm up / pre-burn fuel charge (       lbs.) added at





### TEST DATA SHEET #10

Unit : F400 Run : 1 Date : 4-7-00

Room Temperature : 70 °F Correction Factor : 0

Uncorrected Values are corrected for room temperature : Yes          No ✓

Time Test Fuel moisture reading taken : 1110

Calibration Checks : X ✓ Y ✓ 12.0 12.1 22.0 22.1

| pc # | Dimen.   | Use | TOP   |      | BOTTOM |      | SIDE   |      | Avg Corrected |
|------|----------|-----|-------|------|--------|------|--------|------|---------------|
|      |          |     | Uncor | Cor. | Uncor. | Cor. | Uncor. | Cor. |               |
| 1    | 2"x4"x8' | K   | 16.0  | 17.0 | 14.5   | 15.5 | 15.0   | 16.0 | 16.167        |
| 2    |          |     |       |      |        |      |        |      |               |
| 3    |          |     |       |      |        |      |        |      |               |
| 4    | 2"x4"x8' | P   | 17.5  | 18.7 | 18.0   | 19.2 | 18.0   | 19.2 | 19.033        |
| 5    | 2"x4"x8' | P   | 17.5  | 18.7 | 18.0   | 19.2 | 18.0   | 19.2 | 19.033        |
| 6    | 2"x4"x8' | P   | 18.0  | 19.2 | 18.5   | 19.8 | 19.0   | 20.3 | 19.767        |
| 7    | 2"x4"x8' | P   |       |      |        |      |        |      | 57.833        |
| 8    | 2"x4"x8' | P   |       |      |        |      |        |      |               |
| 9    |          |     |       |      |        |      |        |      |               |
| 10   |          |     |       |      |        |      |        |      |               |
| 11   |          |     |       |      |        |      |        |      |               |
| 12   | 2x4x13   | T   | 17.5  | 18.7 | 18.0   | 19.2 | 18.0   | 19.2 | 19.033        |
| 13   | "        | T   | 21.0  | 22.5 | 21.5   | 23.1 | 21.0   | 22.5 | 22.700        |
| 14   | "        | T   | 23.5  | 25.2 | 23.0   | 24.7 | 23.5   | 25.2 | 25.033        |
| 15   | 4x4x13   | T   | 17.5  | 18.7 | 17.5   | 18.7 | 18.0   | 19.2 | 18.867        |
| 16   | "        | T   | 22.0  | 23.7 | 22.5   | 24.1 | 22.0   | 23.7 | 23.833        |
| 17   |          |     |       |      |        |      |        |      | 109.466       |
| 18   |          |     |       |      |        |      |        |      |               |
| 19   |          |     |       |      |        |      |        |      |               |
| 20   | Spacers  | T   | 22.0  | 23.7 | 23.0   | 24.7 | 23.0   | 24.7 |               |

Key for Use : K = Kindling P = Pretest Fuel T = Test Fuel

|                  | KINDLING | PRETEST FUEL | TEST FUEL |
|------------------|----------|--------------|-----------|
| Dry Moisture % : | 16.167 % | 19.278 %     | 21.893 %  |
| Wet Moisture % : | 13.917 % | 16.162 %     | 17.961 %  |

To obtain Wet from Dry :  $\frac{100 \times \% \text{ Dry Reading}}{100 + \% \text{ Dry Reading}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges : 16 - 20 % wet: 19 - 25 % dry (17.5 - 22.5 on Meter Uncor. reading) at 70°





WEIGHT: 39.2

AS DATA SHEET # 12

of 3

F400

RUN: 1 DATE: 4-7-00 PAGE: 1

| TIME               | SCALE            | FUEL            | DROP          | V.               | CO <sub>2</sub> | V.           | O <sub>2</sub> | V.               | CO              | BAL              | WB           | DB           | % H <sub>2</sub> O | CAL WB       | STACK          | STATIC          | SO <sub>2</sub> PPM |
|--------------------|------------------|-----------------|---------------|------------------|-----------------|--------------|----------------|------------------|-----------------|------------------|--------------|--------------|--------------------|--------------|----------------|-----------------|---------------------|
| <del>0 135</del>   | <del>406.3</del> | <del>13.2</del> | <del>—</del>  | <del>.223</del>  | <del>5.6</del>  | <del>—</del> | <del>—</del>   | <del>.124</del>  | <del>1.24</del> | <del>4.5</del>   | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>313</del> | <del>-040</del> | <del>450</del>      |
| <del>5 40</del>    | <del>406.0</del> | <del>12.9</del> | <del>.3</del> | <del>.155</del>  | <del>3.8</del>  | <del>—</del> | <del>—</del>   | <del>.109</del>  | <del>1.09</del> | <del>3.5</del>   | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>379</del> | <del>-040</del> | <del>425</del>      |
| <del>10 45</del>   | <del>405.7</del> | <del>12.6</del> | <del>.3</del> | <del>.1079</del> | <del>1.9</del>  | <del>—</del> | <del>—</del>   | <del>.1049</del> | <del>.49</del>  | <del>3.9</del>   | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>368</del> | <del>036</del>  | <del>425</del>      |
| <del>15 50</del>   | <del>405.5</del> | <del>12.4</del> | <del>.2</del> | <del>.082</del>  | <del>2.0</del>  | <del>—</del> | <del>—</del>   | <del>.051</del>  | <del>.51</del>  | <del>3.9</del>   | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>234</del> | <del>034</del>  | <del>450</del>      |
| <del>20 55</del>   | <del>405.4</del> | <del>12.3</del> | <del>.1</del> | <del>.087</del>  | <del>2.2</del>  | <del>—</del> | <del>—</del>   | <del>.057</del>  | <del>.57</del>  | <del>3.8</del>   | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>226</del> | <del>031</del>  | <del>475</del>      |
| <del>25 1300</del> | <del>405.2</del> | <del>12.1</del> | <del>.2</del> | <del>.094</del>  | <del>2.4</del>  | <del>—</del> | <del>—</del>   | <del>.064</del>  | <del>.64</del>  | <del>3.7</del>   | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>216</del> | <del>030</del>  | <del>500</del>      |
| <del>30 05</del>   | <del>405.0</del> | <del>11.9</del> | <del>.2</del> | <del>.108</del>  | <del>2.7</del>  | <del>—</del> | <del>—</del>   | <del>.072</del>  | <del>.72</del>  | <del>3.7</del>   | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>207</del> | <del>029</del>  | <del>525</del>      |
| <del>35 10</del>   | <del>404.7</del> | <del>11.6</del> | <del>.3</del> | <del>.122</del>  | <del>3.0</del>  | <del>—</del> | <del>—</del>   | <del>.073</del>  | <del>.73</del>  | <del>4.1</del>   | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>204</del> | <del>030</del>  | <del>500</del>      |
| <del>40 15</del>   | <del>404.5</del> | <del>11.4</del> | <del>.2</del> | <del>.140</del>  | <del>3.5</del>  | <del>—</del> | <del>—</del>   | <del>.087</del>  | <del>.87</del>  | <del>4.0</del>   | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>203</del> | <del>030</del>  | <del>500</del>      |
| <del>45 20</del>   | <del>403.7</del> | <del>10.6</del> | <del>.8</del> | <del>.498</del>  | <del>12.5</del> | <del>—</del> | <del>—</del>   | <del>.079</del>  | <del>.19</del>  | <del>6.4.2</del> | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>452</del> | <del>-054</del> | <del>325</del>      |
| <del>50 25</del>   | <del>403.0</del> | <del>9.9</del>  | <del>.7</del> | <del>.478</del>  | <del>12.0</del> | <del>—</del> | <del>—</del>   | <del>.071</del>  | <del>.11</del>  | <del>10.19</del> | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>468</del> | <del>-056</del> | <del>325</del>      |
| <del>55 30</del>   | <del>402.3</del> | <del>9.2</del>  | <del>.7</del> | <del>.482</del>  | <del>12.1</del> | <del>—</del> | <del>—</del>   | <del>.071</del>  | <del>.11</del>  | <del>10.58</del> | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>482</del> | <del>-058</del> | <del>325</del>      |
| TOTAL              | *****            | ****            | ****          | *****            | *****           | *****        | *****          | *****            | *****           | *****            | *****        | *****        | *****              | *****        | 3652           | -468            | *****               |
| <del>60 1335</del> | <del>401.8</del> | <del>8.7</del>  | <del>.5</del> | <del>.389</del>  | <del>9.7</del>  | <del>—</del> | <del>—</del>   | <del>.07</del>   | <del>.17</del>  | <del>55.9</del>  | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>457</del> | <del>055</del>  | <del>325</del>      |
| <del>65 40</del>   | <del>401.2</del> | <del>8.1</del>  | <del>.6</del> | <del>.441</del>  | <del>11.0</del> | <del>—</del> | <del>—</del>   | <del>.07</del>   | <del>.07</del>  | <del>149.0</del> | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>464</del> | <del>056</del>  | <del>325</del>      |
| <del>70 45</del>   | <del>400.7</del> | <del>7.6</del>  | <del>.5</del> | <del>.497</del>  | <del>12.4</del> | <del>—</del> | <del>—</del>   | <del>.07</del>   | <del>.04</del>  | <del>282.6</del> | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>487</del> | <del>057</del>  | <del>325</del>      |
| <del>75 50</del>   | <del>400.0</del> | <del>6.9</del>  | <del>.7</del> | <del>.518</del>  | <del>13.0</del> | <del>—</del> | <del>—</del>   | <del>.07</del>   | <del>.03</del>  | <del>381.2</del> | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>503</del> | <del>057</del>  | <del>325</del>      |
| <del>80 55</del>   | <del>399.5</del> | <del>6.4</del>  | <del>.5</del> | <del>.448</del>  | <del>11.2</del> | <del>—</del> | <del>—</del>   | <del>.06</del>   | <del>.06</del>  | <del>175.1</del> | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>476</del> | <del>055</del>  | <del>325</del>      |
| <del>85 1400</del> | <del>399.1</del> | <del>6.0</del>  | <del>.4</del> | <del>.400</del>  | <del>10.0</del> | <del>—</del> | <del>—</del>   | <del>.06</del>   | <del>.06</del>  | <del>156.2</del> | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>463</del> | <del>054</del>  | <del>325</del>      |
| <del>90 05</del>   | <del>398.7</del> | <del>5.6</del>  | <del>.4</del> | <del>.378</del>  | <del>9.4</del>  | <del>—</del> | <del>—</del>   | <del>.06</del>   | <del>.06</del>  | <del>147.6</del> | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>449</del> | <del>053</del>  | <del>325</del>      |
| <del>95 10</del>   | <del>398.3</del> | <del>5.2</del>  | <del>.4</del> | <del>.347</del>  | <del>8.7</del>  | <del>—</del> | <del>—</del>   | <del>.06</del>   | <del>.13</del>  | <del>64.7</del>  | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>430</del> | <del>051</del>  | <del>325</del>      |
| <del>100 15</del>  | <del>398.0</del> | <del>4.9</del>  | <del>.3</del> | <del>.339</del>  | <del>8.5</del>  | <del>—</del> | <del>—</del>   | <del>.06</del>   | <del>.23</del>  | <del>36.2</del>  | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>419</del> | <del>050</del>  | <del>350</del>      |
| <del>105 20</del>  | <del>397.6</del> | <del>4.5</del>  | <del>.4</del> | <del>.347</del>  | <del>8.7</del>  | <del>—</del> | <del>—</del>   | <del>.05</del>   | <del>.53</del>  | <del>16.2</del>  | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>412</del> | <del>050</del>  | <del>400</del>      |
| <del>110 25</del>  | <del>397.3</del> | <del>4.2</del>  | <del>.3</del> | <del>.335</del>  | <del>8.4</del>  | <del>—</del> | <del>—</del>   | <del>.07</del>   | <del>.71</del>  | <del>11.7</del>  | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>406</del> | <del>049</del>  | <del>400</del>      |
| <del>115 30</del>  | <del>396.9</del> | <del>3.8</del>  | <del>.4</del> | <del>.316</del>  | <del>7.9</del>  | <del>—</del> | <del>—</del>   | <del>.08</del>   | <del>.84</del>  | <del>9.3</del>   | <del>—</del> | <del>—</del> | <del>—</del>       | <del>—</del> | <del>384</del> | <del>048</del>  | <del>425</del>      |
| TOTAL              | *****            | ****            | ****          | *****            | *****           | *****        | *****          | *****            | *****           | *****            | *****        | *****        | *****              | *****        | 5352           | -635            | *****               |
| TOTAL              | *****            | *****           | *****         | *****            | *****           | *****        | *****          | *****            | *****           | *****            | *****        | *****        | *****              | *****        | 9004           | -1103           | *****               |





WEIGHT: 392.1

UNIT: F400

GAS DATA SHEET # 12

RUN: ( DATE: 4-7-2000 PAGE: 2 of 3

| TIME  | SCALE | FUEL | DROP | V.   | CO <sub>2</sub> | V.   | O <sub>2</sub> | V.   | CO | BAL | WB | DB | % H <sub>2</sub> O | CAL WB | STACK | STATIC | SO <sub>2</sub> PPM |
|-------|-------|------|------|------|-----------------|------|----------------|------|----|-----|----|----|--------------------|--------|-------|--------|---------------------|
| 120   | 396.6 | 3.5  | .3   | .306 | 7.5             | .106 | 1.06           | 7.0  |    |     |    |    |                    |        | 358   | -046   | 475                 |
| 125   | 396.3 | 3.2  | .3   | .297 | 7.4             | .104 | 1.04           | 7.1  |    |     |    |    |                    |        | 347   | -044   | 475                 |
| 130   | 396.1 | 3.0  | .2   | .306 | 7.6             | .102 | 1.02           | 7.5  |    |     |    |    |                    |        | 337   | -043   | 475                 |
| 135   | 395.8 | 2.7  | .3   | .314 | 7.8             | .099 | .99            | 7.9  |    |     |    |    |                    |        | 335   | -043   | 475                 |
| 140   | 395.6 | 2.5  | .2   | .302 | 7.5             | .074 | .74            | 10.1 |    |     |    |    |                    |        | 336   | -042   | 475                 |
| 145   | 395.4 | 2.3  | .2   | .280 | 7.0             | .089 | .89            | 7.8  |    |     |    |    |                    |        | 328   | -041   | 450                 |
| 150   | 395.2 | 2.1  | .2   | .238 | 5.9             | .134 | 1.34           | 4.4  |    |     |    |    |                    |        | 303   | -039   | 525                 |
| 155   | 395.2 | 2.1  | .1   | .232 | 5.8             | .139 | 1.39           | 4.1  |    |     |    |    |                    |        | 287   | -036   | 500                 |
| 160   | 395.1 | 2.0  | .1   | .233 | 5.8             | .154 | 1.54           | 3.8  |    |     |    |    |                    |        | 278   | -034   | 500                 |
| 165   | 395.0 | 1.9  | .1   | .235 | 5.9             | .148 | 1.48           | 3.9  |    |     |    |    |                    |        | 270   | -033   | 500                 |
| 170   | 394.9 | 1.8  | .1   | .236 | 5.9             | .156 | 1.56           | 3.8  |    |     |    |    |                    |        | 264   | -032   | 500                 |
| 175   | 394.8 | 1.7  | .1   | .226 | 5.6             | .161 | 1.61           | 3.5  |    |     |    |    |                    |        | 260   | -031   | 500                 |
| TOTAL |       |      |      |      |                 |      |                |      |    |     |    |    |                    |        | 3707  | -464   | *****               |
| 180   | 394.7 | 1.6  | .1   | .206 | 5.1             | .216 | 2.16           | 2.4  |    |     |    |    |                    |        | 252   | -030   | 525                 |
| 185   | 394.6 | 1.5  | .1   | .202 | 5.0             | .221 | 2.21           | 2.3  |    |     |    |    |                    |        | 247   | -029   | 525                 |
| 190   | 394.5 | 1.4  | .1   | .201 | 5.0             | .221 | 2.21           | 2.3  |    |     |    |    |                    |        | 244   | -029   | 525                 |
| 195   | 394.5 | 1.4  | .1   | .215 | 5.4             | .197 | 1.97           | 2.7  |    |     |    |    |                    |        | 243   | -028   | 525                 |
| 200   | 394.4 | 1.3  | .1   | .209 | 5.2             | .204 | 2.04           | 2.5  |    |     |    |    |                    |        | 241   | -028   | 550                 |
| 205   | 394.4 | 1.3  | .1   | .267 | 5.2             | .211 | 2.11           | 2.4  |    |     |    |    |                    |        | 238   | -027   | 550                 |
| 210   | 394.3 | 1.2  | .1   | .201 | 5.0             | .226 | 2.26           | 2.2  |    |     |    |    |                    |        | 237   | -027   | 550                 |
| 215   | 394.3 | 1.2  | .1   | .196 | 4.9             | .224 | 2.24           | 2.2  |    |     |    |    |                    |        | 235   | -027   | 550                 |
| 220   | 394.2 | 1.1  | .1   | .197 | 4.9             | .224 | 2.24           | 2.2  |    |     |    |    |                    |        | 233   | -027   | 575                 |
| 225   | 394.1 | 1.0  | .1   | .215 | 5.4             | .128 | 1.28           | 4.2  |    |     |    |    |                    |        | 229   | -026   | 550                 |
| 230   | 394.0 | .9   | .1   | .214 | 5.3             | .129 | 1.29           | 4.1  |    |     |    |    |                    |        | 228   | -026   | 575                 |
| 235   | 394.0 | .9   | .1   | .213 | 5.3             | .131 | 1.31           | 4.0  |    |     |    |    |                    |        | 227   | -026   | 575                 |
| TOTAL |       |      |      |      |                 |      |                |      |    |     |    |    |                    |        | 2854  | -330   | *****               |
| TOTAL |       |      |      |      |                 |      |                |      |    |     |    |    |                    |        | 6561  | -794   | *****               |





WEIGHT: 39.1

UNIT: F400

GAS ΛΥΓΑ ΣΠΕΕΙ # 12

RUN: 1

DATE: 4-7-00

PAGE: 3

of 3

| TIME           | SCALE            | FUEL          | DROP          | V.              | CO <sub>2</sub> | V.           | O <sub>2</sub> | V.              | CO             | BAL   | WB    | DB    | % H <sub>2</sub> O | CAL WB | STACK          | STATIC          | SO <sub>2</sub> PPM |
|----------------|------------------|---------------|---------------|-----------------|-----------------|--------------|----------------|-----------------|----------------|-------|-------|-------|--------------------|--------|----------------|-----------------|---------------------|
| <del>240</del> | <del>393.9</del> | <del>.8</del> | <del>.1</del> | <del>.212</del> | <del>5.3</del>  | <del>-</del> | <del>-</del>   | <del>.135</del> | <del>3.9</del> |       |       |       |                    |        | <del>226</del> | <del>7027</del> | <del>575</del>      |
| <del>245</del> | <del>393.9</del> | <del>.8</del> | <del>0</del>  | <del>.209</del> | <del>5.2</del>  |              |                | <del>.152</del> | <del>3.4</del> |       |       |       |                    |        | <del>227</del> | <del>7026</del> | <del>575</del>      |
| <del>250</del> | <del>393.8</del> | <del>.7</del> | <del>.1</del> | <del>.206</del> | <del>5.1</del>  |              |                | <del>.153</del> | <del>3.3</del> |       |       |       |                    |        | <del>225</del> | <del>7026</del> | <del>575</del>      |
| <del>255</del> | <del>393.8</del> | <del>.7</del> | <del>0</del>  | <del>.221</del> | <del>5.5</del>  |              |                | <del>.133</del> | <del>4.1</del> |       |       |       |                    |        | <del>224</del> | <del>7026</del> | <del>575</del>      |
| <del>260</del> | <del>393.7</del> | <del>.6</del> | <del>.1</del> | <del>.225</del> | <del>5.6</del>  |              |                | <del>.153</del> | <del>3.7</del> |       |       |       |                    |        | <del>224</del> | <del>7026</del> | <del>575</del>      |
| <del>265</del> | <del>393.6</del> | <del>.5</del> | <del>.1</del> | <del>.219</del> | <del>5.5</del>  |              |                | <del>.167</del> | <del>3.3</del> |       |       |       |                    |        | <del>224</del> | <del>7026</del> | <del>575</del>      |
| <del>270</del> | <del>393.6</del> | <del>.5</del> | <del>0</del>  | <del>.214</del> | <del>5.3</del>  |              |                | <del>.168</del> | <del>3.2</del> |       |       |       |                    |        | <del>223</del> | <del>7026</del> | <del>575</del>      |
| <del>275</del> | <del>393.6</del> | <del>.5</del> | <del>0</del>  | <del>.208</del> | <del>5.2</del>  |              |                | <del>.180</del> | <del>2.9</del> |       |       |       |                    |        | <del>223</del> | <del>7026</del> | <del>575</del>      |
| <del>280</del> | <del>393.5</del> | <del>.4</del> | <del>.1</del> | <del>.207</del> | <del>5.2</del>  |              |                | <del>.186</del> | <del>2.8</del> |       |       |       |                    |        | <del>223</del> | <del>7025</del> | <del>600</del>      |
| <del>285</del> | <del>393.4</del> | <del>.3</del> | <del>.1</del> | <del>.196</del> | <del>4.9</del>  |              |                | <del>.195</del> | <del>2.5</del> |       |       |       |                    |        | <del>224</del> | <del>7025</del> | <del>600</del>      |
| <del>290</del> | <del>393.3</del> | <del>.2</del> | <del>.1</del> | <del>.181</del> | <del>4.5</del>  |              |                | <del>.205</del> | <del>2.2</del> |       |       |       |                    |        | <del>219</del> | <del>7026</del> | <del>600</del>      |
| <del>295</del> | <del>393.3</del> | <del>.2</del> | <del>0</del>  | <del>.177</del> | <del>4.4</del>  |              |                | <del>.206</del> | <del>2.1</del> |       |       |       |                    |        | <del>217</del> | <del>7026</del> | <del>600</del>      |
| TOTAL          | *****            | ****          | ****          | *****           | *****           | *****        | *****          | *****           | *****          | ***** | ***** | ***** | *****              | *****  | 2676           | -311            | *****               |
| 300            | 393.2            | .1            | .1            | .153            | 3.8             |              |                | .181            | 1.81           | 2.1   |       |       |                    |        | 213            | 7025            | 600                 |
| 305            | 393.2            | .1            | 0             | .154            | 3.8             |              |                | .190            | 1.90           | 2.0   |       |       |                    |        | 208            | 7025            | 625                 |
| 310            | 393.2            | .1            | 0             | .154            | 3.9             |              |                | .193            | 1.93           | 2.0   |       |       |                    |        | 206            | 7024            | 625                 |
| 315            | 393.1            | 0             | .1            | .164            | 4.1             |              |                | .202            | 2.02           | 2.0   |       |       |                    |        | 204            | 7024            | 625                 |
| TOTAL          | *****            | ****          | ****          | *****           | *****           | *****        | *****          | *****           | *****          | ***** | ***** | ***** | *****              | *****  | 19072          | -2306           | *****               |
| TOTAL          | *****            | ****          | ****          | *****           | *****           | *****        | *****          | *****           | *****          | ***** | ***** | ***** | *****              | *****  | 298            | -036            | *****               |

64



























## ZERO / SPAN CHECK DATA SHEET #15-1

Date: 4-7-00 Analyte: CO<sub>2</sub> (15-1)

Source: F400 Run #: 1

Zero Cyl. #: TX 79373 Conc.: 0.00 % CO<sub>2</sub> Cyl. Press.: 960 PSI

Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 12.79 % CO<sub>2</sub> Cyl. Press.: 1750 PSI

Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: HORIBA Model: PIR-2000 SN: 407069

Range: 0 - 25.0 % CO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 25.0 % CO<sub>2</sub>

EPA Control Limits =  $\pm 2.5\%$  of 25.0 % CO<sub>2</sub> =  $\pm 0.625 % CO_2$

Method 28 A =  $\pm .2 %$  of 25.0 % CO<sub>2</sub> =  $\pm .05 % CO_2$

PRE RUN Audit: by: A. Whidston Time: 1115 Temp: 85 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |       |        | ± Conc. Difference | Δ %     |
|---------|-------------------|------|-------|-----------------|-------|--------|--------------------|---------|
|         | Meter             | DVM  | %     | Meter           | DVM   | %      |                    |         |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | -.002 | -.098  | -.098 ✓            | -.393 ✓ |
| SPAN    | 51.2              | .512 | 12.79 | 51.0            | .510  | 12.761 | -.029 ✓            | -.115 ✓ |

POST RUN Audit: by: D. Whidston Time: 1805 Temp: 78 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |        | ± Conc. Difference | Δ %     |
|---------|-------------------|------|-------|-----------------|------|--------|--------------------|---------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %      |                    |         |
| ZERO    | 00.0              | .000 | 00.0  | 00.3            | .003 | .027   | .027 ✓             | .109 ✓  |
| SPAN    | 51.2              | .512 | 12.79 | 51.0            | .510 | 12.761 | -.029 ✓            | -.115 ✓ |

± Conc. Difference = Act % - Exp (Std) %

Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





## ZERO / SPAN CHECK DATA SHEET #15-2

Date: 4-7-00 Analyte: O<sub>2</sub> (15-2)

Source: F400 Run #: 1

Zero Cyl. #: TX79373 Conc.: 0.00 % O<sub>2</sub> Cyl. Press.: 960 PSI  
 Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 12.69 % O<sub>2</sub> Cyl. Press.: 1750 PSI  
 Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: TELEDYNE Model: 320 A SN: 37400  
 Range: 0 - 25.0 % O<sub>2</sub> Analyzer Output: 0 - 1.0 v.  
 Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 25.0 % O<sub>2</sub>  
 EPA Control Limits =  $\pm 2.5\%$  of 25.0 % O<sub>2</sub> =  $\pm 0.625 % O_2$   
 Method 28 A =  $\pm .2 %$  of 25.0 % O<sub>2</sub> =  $\pm .05 % O_2$

PRE RUN Audit : by: D. W. [Signature] Time: 1115 Temp: 85 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |          | ± Conc. Difference | Δ %    |
|---------|-------------------|------|-------|-----------------|------|----------|--------------------|--------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %        |                    |        |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | .001 | .050     | .050 ✓             | .200 ✓ |
| SPAN    | 12.7              | .508 | 12.69 | 12.7            | .510 | 12.737 ✓ | .047 ✓             | .187 ✓ |

POST RUN Audit : by: D. W. [Signature] Time: 1805 Temp: 79 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |          | ± Conc. Difference | Δ %    |
|---------|-------------------|------|-------|-----------------|------|----------|--------------------|--------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %        |                    |        |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | .062 | .075     | .075 ✓             | .299 ✓ |
| SPAN    | 12.7              | .508 | 12.69 | 12.7            | .509 | 12.712 ✓ | .022 ✓             | .088 ✓ |

± Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





## ZERO / SPAN CHECK DATA SHEET #15-3

Date: 4-7-00 Analyte: CO (15-3)

Source: F400 Run #: 1

Zero Cyl. #: TX79373 Conc.: 0.00 % CO Cyl. Press.: 960 PSI  
 Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 4.75 % CO Cyl. Press.: 1750 PSI  
 Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: HORIBA Model: PIR-2000 SN: 408005  
 Range: 0 - 10.0 % CO Analyzer Output: 0 - 1.0 v.  
 Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 10.0 % CO  
 EPA Control Limits =  $\pm 2.5\%$  of 10.0 % CO =  $\pm 0.25 % CO$   
 Method 28 A =  $\pm .2 %$  of 10.0 % CO =  $\pm .02 % CO$

PRE RUN Audit: by: [Signature] Time: 1115 Temp: 85 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |       | ± Conc. Difference | Δ %    |
|---------|-------------------|------|------|-----------------|------|-------|--------------------|--------|
|         | Meter             | DVM  | %    | Meter           | DVM  | %     |                    |        |
| ZERO    | 00.0              | .000 | 00.0 | 00.0            | .000 | .004  | .004 ✓             | .042 ✓ |
| SPAN    | 47.5              | .475 | 4.75 | 47.5            | .475 | 4.752 | .002 ✓             | .021 ✓ |

POST RUN Audit: by: [Signature] Time: 1805 Temp: 78 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |         | ± Conc. Difference | Δ %    |
|---------|-------------------|------|------|-----------------|------|---------|--------------------|--------|
|         | Meter             | DVM  | %    | Meter           | DVM  | %       |                    |        |
| ZERO    | 00.0              | .000 | 00.0 | 00.0            | .000 | .004    | .004 ✓             | .042 ✓ |
| SPAN    | 47.5              | .475 | 4.75 | 47.5            | .475 | 4.752 ✓ | .002 ✓             | .021 ✓ |

± Conc. Difference =  $\text{Act \%} - \text{Exp (Std) \%}$   
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$



## ZERO / SPAN CHECK DATA SHEET #15-4

Date: 4-7-00 Analyte: SO<sub>2</sub> (15-4)

Source: F400 Run #: 1

Zero Cyl. #: TX79373 Conc.: 0.00 ppm SO<sub>2</sub> Cyl. Press.: 960 PSI

Certified by: AIR LIQUINE Date: 9-22-1998

Span Cyl. #: CC67475 Conc.: 1260 ppm SO<sub>2</sub> Cyl. Press.: 650 PSI

Certified by: AIR LIQUINE Date: 9-22-1998

Analyzer: Make: HORIBA Model: PIR-2000 SN: 403019

Range: 0 - 2500 ppm SO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 2500 ppm SO<sub>2</sub>

EPA Control Limits =  $\pm 2.5\%$  of 2500 ppm SO<sub>2</sub> =  $\pm 62.5$  ppm SO<sub>2</sub>

PRE RUN Audit: by: A. Wadlington Time: 1110 Temp: 85 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |          | ± Conc. Difference | Δ %      |
|---------|-------------------|------|------|-----------------|------|----------|--------------------|----------|
|         | Meter             | DVM  | PPM  | Meter           | DVM  | %        |                    |          |
| ZERO    | 00.0              | .000 | 00.0 | 00.7            | .007 | 30.359   | 30.359             | 1.214 ✓  |
| SPAN    | 50.4              | .504 | 1260 | 50.0            | .500 | 1250.200 | -9.800             | -0.392 ✓ |

POST RUN Audit: by: A. Wadlington Time: 1810 Temp: 77 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |          | ± Conc. Difference | Δ %      |
|---------|-------------------|------|------|-----------------|------|----------|--------------------|----------|
|         | Meter             | DVM  | PPM  | Meter           | DVM  | %        |                    |          |
| ZERO    | 00.0              | .000 | 00.0 | 00.4            | .004 | 22.936   | 22.936             | .917 ✓   |
| SPAN    | 50.4              | .504 | 1260 | 49.6            | .496 | 1240.302 | -19.698            | -0.788 ✓ |

± Conc. Difference = Act % - Exp (Std) %

Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





### QUALITY CHECKS DATA SHEET # 16

UNIT: F400 RUN: 1 DATE: 4-7-00

**Thermocouple Check :**

|          |             |    |          |             |    |
|----------|-------------|----|----------|-------------|----|
| T/C # 1  | <u>—</u>    | °F | T/C # 13 | <u>62.8</u> | °F |
| T/C # 2  | <u>—</u>    | °F | T/C # 14 | <u>62.2</u> | °F |
| T/C # 3  | <u>61.1</u> | °F | T/C # 15 | <u>63.2</u> | °F |
| T/C # 4  | <u>54.9</u> | °F | T/C # 16 | <u>52.7</u> | °F |
| T/C # 5  | <u>54.0</u> | °F | T/C # 17 | <u>51.5</u> | °F |
| T/C # 6  | <u>53.7</u> | °F | T/C # 18 | <u>67.8</u> | °F |
| T/C # 7  | <u>53.7</u> | °F | T/C # 19 | <u>55.8</u> | °F |
| T/C # 8  | <u>53.3</u> | °F | T/C # 20 | <u>51.1</u> | °F |
| T/C # 9  | <u>54.5</u> | °F | T/C # 21 | <u>—</u>    | °F |
| T/C # 10 | <u>54.8</u> | °F | T/C # 22 | <u>—</u>    | °F |
| T/C # 11 | <u>51.0</u> | °F | T/C # 23 | <u>55.5</u> | °F |
| T/C # 12 | <u>72.0</u> | °F | T/C # 24 | <u>—</u>    | °F |

**Thermocouple Readout :**

Pretest zero and span check and calibration

ZERO: -2.3 °F Adj. to 0.0 °F

SPAN: 2001.3 °F Adj. to 2000.0 °F

post test zero and span

% difference

ZERO 2.6 °F Difference .130 %

SPAN 2004.8 °F Difference .240 %

**Thermocouple Readout Pretest Linearity Check**

|      |                    |      |                    |      |                    |
|------|--------------------|------|--------------------|------|--------------------|
| 0    | = <u>0.0</u> °F    | 200  | = <u>202.0</u> °F  | 400  | = <u>399.3</u> °F  |
| 600  | = <u>601.6</u> °F  | 800  | = <u>801.7</u> °F  | 1000 | = <u>1000.7</u> °F |
| 1200 | = <u>1198.3</u> °F | 1400 | = <u>1399.2</u> °F | 1600 | = <u>1599.8</u> °F |
| 1800 | = <u>1800.0</u> °F | 2000 | = <u>2000.0</u> °F |      |                    |

Sample Train Leak Check

Pre

Post

C-gas Train Leak Check

Pre

Post

SO<sub>2</sub> Train Leak Check

Pre

Post

Static Gauge Zero Check

Pre

Post

Scale Check Pre: 404.4 - 394.4

Post: 403.1 - 393.1

Stack Cleaned Prior to Test Run : YES  NO









TABLE 1 ----- RAW DATA

CLIENT : Jotul

TEST No. : 3

MODEL: F400

DATE: 11-Apr-00

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| TIME<br>(MIN.) | METER<br>READING<br>(C F) | DELTA<br>H<br>(IN. H2O) | METER<br>TEMP.<br>(DEG. F) | PERCENT<br>CO<br>( % ) | PERCENT<br>CO2<br>( % ) | SO2<br>COCENTR.<br>PPM |
|----------------|---------------------------|-------------------------|----------------------------|------------------------|-------------------------|------------------------|
| 0              | 307.500                   | 0.150                   | 81                         | 1.03                   | 5.10                    | 400                    |
| 5              | 309.000                   | 0.260                   | 81                         | 0.34                   | 2.50                    | 300                    |
| 10             | 311.036                   | 0.110                   | 83                         | 0.61                   | 2.00                    | 450                    |
| 15             | 312.405                   | 0.100                   | 83                         | 0.61                   | 1.80                    | 475                    |
| 20             | 313.702                   | 0.100                   | 83                         | 0.71                   | 1.90                    | 475                    |
| 25             | 314.998                   | 0.110                   | 83                         | 0.80                   | 3.50                    | 450                    |
| 30             | 316.367                   | 0.220                   | 83                         | 0.64                   | 12.90                   | 325                    |
| 35             | 318.261                   | 0.260                   | 83                         | 0.55                   | 9.90                    | 300                    |
| 40             | 320.312                   | 0.370                   | 83                         | 0.11                   | 13.00                   | 250                    |
| 45             | 322.773                   | 0.370                   | 84                         | 0.07                   | 12.00                   | 250                    |
| 50             | 325.242                   | 0.300                   | 86                         | 0.06                   | 13.80                   | 275                    |
| 55             | 327.504                   | 0.300                   | 87                         | 0.05                   | 13.70                   | 275                    |
| 60             | 329.775                   | 0.300                   | 87                         | 0.03                   | 13.70                   | 275                    |
| 65             | 332.046                   | 0.300                   | 87                         | 0.03                   | 14.10                   | 275                    |
| 70             | 334.316                   | 0.300                   | 87                         | 0.07                   | 11.60                   | 275                    |
| 75             | 336.587                   | 0.210                   | 87                         | 0.47                   | 9.00                    | 325                    |
| 80             | 338.509                   | 0.190                   | 87                         | 0.63                   | 8.30                    | 350                    |
| 85             | 340.294                   | 0.160                   | 87                         | 0.60                   | 8.00                    | 375                    |
| 90             | 341.960                   | 0.190                   | 87                         | 0.60                   | 7.80                    | 350                    |
| 95             | 343.745                   | 0.190                   | 87                         | 0.56                   | 7.60                    | 350                    |
| 100            | 345.530                   | 0.190                   | 86                         | 0.59                   | 7.40                    | 350                    |
| 105            | 347.308                   | 0.190                   | 86                         | 0.65                   | 7.30                    | 350                    |
| 110            | 349.087                   | 0.190                   | 86                         | 0.55                   | 7.60                    | 350                    |
| 115            | 350.865                   | 0.190                   | 86                         | 0.69                   | 6.90                    | 350                    |
| 120            | 352.644                   | 0.160                   | 86                         | 0.71                   | 6.70                    | 375                    |
| 125            | 354.305                   | 0.160                   | 86                         | 0.86                   | 6.30                    | 375                    |
| 130            | 355.966                   | 0.140                   | 86                         | 1.29                   | 5.70                    | 400                    |
| 135            | 357.524                   | 0.140                   | 86                         | 1.42                   | 5.50                    | 400                    |
| 140            | 359.081                   | 0.140                   | 86                         | 1.49                   | 5.30                    | 400                    |
| 145            | 360.639                   | 0.140                   | 86                         | 1.52                   | 5.50                    | 400                    |
| 150            | 362.197                   | 0.140                   | 86                         | 1.66                   | 5.20                    | 400                    |
| 155            | 363.754                   | 0.140                   | 86                         | 1.76                   | 5.00                    | 400                    |
| 160            | 365.312                   | 0.140                   | 86                         | 1.76                   | 4.90                    | 400                    |
| 165            | 366.869                   | 0.130                   | 86                         | 1.41                   | 5.50                    | 425                    |
| 170            | 368.335                   | 0.100                   | 86                         | 1.46                   | 5.30                    | 475                    |
| 175            | 369.647                   | 0.100                   | 88                         | 1.53                   | 5.30                    | 475                    |
| 180            | 370.969                   | 0.090                   | 90                         | 1.27                   | 5.30                    | 500                    |
| 185            | 372.233                   | 0.070                   | 90                         | 1.38                   | 5.00                    | 575                    |
| 190            | 373.333                   | 0.060                   | 90                         | 1.23                   | 4.70                    | 600                    |
| 195            | 374.387                   | 0.050                   | 91                         | 1.17                   | 4.90                    | 650                    |
| 200            | 375.364                   | 0.050                   | 91                         | 1.17                   | 4.90                    | 650                    |
| 205            | 376.340                   | 0.050                   | 91                         | 1.28                   | 4.70                    | 650                    |
| 210            | 377.317                   | 0.050                   | 91                         | 1.31                   | 4.70                    | 675                    |
| 215            | 378.257                   | 0.050                   | 91                         | 1.51                   | 4.70                    | 675                    |



|     |         |       |    |      |      |     |
|-----|---------|-------|----|------|------|-----|
| 220 | 379.198 | 0.050 | 91 | 1.61 | 4.40 | 700 |
| 225 | 380.105 | 0.050 | 91 | 1.69 | 4.20 | 700 |
| 230 | 381.011 | 0.050 | 91 | 1.84 | 4.10 | 700 |
| 235 | 381.918 | 0.040 | 91 | 1.82 | 3.90 | 725 |
| 240 | 382.794 | 0.040 | 91 | 1.80 | 4.10 | 725 |
| 245 |         |       |    |      |      |     |





TABLE 2---RAW DATA

CLIENT : Jotul

TEST No. 3

MODEL: F400

DATE: 11-Apr-00

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|                                |       |                               |      |     |
|--------------------------------|-------|-------------------------------|------|-----|
| METER CAL.<br>FACTOR (Y) ----- | 0.989 | Wt. WOOD<br>BURNED (LB) ----- | 13.0 | Lbs |
|--------------------------------|-------|-------------------------------|------|-----|

|                                 |             |                               |        |   |
|---------------------------------|-------------|-------------------------------|--------|---|
| BAROMETRIC<br>PRESS. (Pb) ----- | 30.09 in Hg | WET, FUEL<br>MOISTURE % ----- | 16.994 | % |
|---------------------------------|-------------|-------------------------------|--------|---|

|                              |           |                              |        |   |
|------------------------------|-----------|------------------------------|--------|---|
| LEAK RATE<br>POST (Lp) ----- | 0.002 cfm | Wt. PART.<br>COLLECTED ----- | 0.5022 | g |
|------------------------------|-----------|------------------------------|--------|---|

|                           |          |                          |        |     |
|---------------------------|----------|--------------------------|--------|-----|
| WATER<br>VOL. (V1c) ----- | 121.3 ML | METER<br>VOLUME Vm ----- | 75.294 | mcf |
|---------------------------|----------|--------------------------|--------|-----|

|                          |         |                           |        |  |
|--------------------------|---------|---------------------------|--------|--|
| TEST<br>TIME (MIN) ----- | 240 min | HC MOLE<br>FRACTION ----- | 0.0132 |  |
|--------------------------|---------|---------------------------|--------|--|



TABLE 3 -----FIELD DATA AVERAGES

CLIENT :Jotul

TEST No. 3

MODEL: F400

DATE: 11-Apr-00

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|           |                   |           |            |   |
|-----------|-------------------|-----------|------------|---|
| AVG DELTA |                   | AVG PRCNT |            |   |
| H         | ----- 0.15 in H2O | CO        | ----- 0.96 | % |
| AVG METER |                   | AVG PRCNT |            |   |
| TEMP. Tm  | ----- 87 deg F    | CO2       | ----- 6.68 | % |
| AVG PPM   |                   | AVG BAL   |            |   |
| SO2       | ----- 442 PPM     | CO2/CO    | ----- 6.96 | % |



TABLE 4 ----- CALCULATIONS

CLIENT : Jotul

TEST No. 3

MODEL: F400

DATE: 11-Apr-00

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|                     |  |                   |                                       |
|---------------------|--|-------------------|---------------------------------------|
| STD SAMPLE          |  | STACK GAS         |                                       |
| VOL. Vm(std) -----  | 72.35 dscf                                 | FLOW Qsd -----    | 492.252 dscf/Hr<br>&<br>8.20 dscf/min |
| VOL. WATER          |  | PARTICULATE       |                                       |
| VAPOR Vw(std) ----- | 5.710 scf                                  | CONCTR. Cs -----  | 0.0069 g/dscf                         |
| PRCNT               |  | PARTC. EMISS.     |                                       |
| MSTR Bws -----      | 7.31 %                                     | RATE E -----      | 3.42 g/Hr                             |
| BURN                |  | MOLES OF GAS      |                                       |
| RATE BR -----       | 1.22 Kg/Hr                                 | PER Lb WOOD Nt -- | 0.47 Lb-mole/Lb                       |
| CO EMISSION         |  | PART. EMISS.      |                                       |
| RATE -----          | 158.12 g/Hr<br>&<br>129.18 g/Kgdry<br>fuel | RATE -----        | 2.79 g/Kgdry<br>fuel                  |





TABLE 5 ----- PROPORTIONAL RATE VARIATION

CLIENT : Jotul

TEST No. : 3

MODEL: F400

DATE: 11-Apr-00

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| TIME<br>INTEVAL<br>Ti | PPM<br>*<br>Vm | PROPRTN.<br>RATE VAR.<br>PR | PROPRTN<br>RATE VAR.<br>AVERAGE |
|-----------------------|----------------|-----------------------------|---------------------------------|
| 5                     | 582.7          | 97                          | 100                             |
| 10                    | 592.3          | 99                          |                                 |
| 15                    | 596.1          | 99                          |                                 |
| 20                    | 596.1          | 99                          |                                 |
| 25                    | 595.6          | 99                          |                                 |
| 30                    | 596.1          | 99                          |                                 |
| 35                    | 595.7          | 99                          |                                 |
| 40                    | 595.6          | 99                          |                                 |
| 45                    | 595.1          | 99                          |                                 |
| 50                    | 595.4          | 99                          |                                 |
| 55                    | 598.3          | 100                         |                                 |
| 60                    | 600.1          | 100                         |                                 |
| 65                    | 600.1          | 100                         |                                 |
| 70                    | 599.9          | 100                         |                                 |
| 75                    | 600.1          | 100                         |                                 |
| 80                    | 600.1          | 100                         |                                 |
| 85                    | 600.2          | 100                         |                                 |
| 90                    | 600.1          | 100                         |                                 |
| 95                    | 600.2          | 100                         |                                 |
| 100                   | 600.7          | 100                         |                                 |
| 105                   | 598.9          | 100                         |                                 |
| 110                   | 599.3          | 100                         |                                 |
| 115                   | 598.9          | 100                         |                                 |
| 120                   | 599.3          | 100                         |                                 |
| 125                   | 599.4          | 100                         |                                 |
| 130                   | 599.4          | 100                         |                                 |
| 135                   | 599.7          | 100                         |                                 |
| 140                   | 599.3          | 100                         |                                 |
| 145                   | 599.7          | 100                         |                                 |
| 150                   | 599.7          | 100                         |                                 |
| 155                   | 599.3          | 100                         |                                 |
| 160                   | 599.7          | 100                         |                                 |
| 165                   | 599.3          | 100                         |                                 |
| 170                   | 599.6          | 100                         |                                 |
| 175                   | 598.6          | 100                         |                                 |
| 180                   | 600.9          | 100                         |                                 |
| 185                   | 603.7          | 101                         |                                 |
| 190                   | 604.1          | 101                         |                                 |
| 195                   | 603.5          | 101                         |                                 |
| 200                   | 605.4          | 101                         |                                 |
| 205                   | 604.8          | 101                         |                                 |
| 210                   | 605.4          | 101                         |                                 |
| 215                   | 604.9          | 101                         |                                 |
| 220                   | 605.6          | 101                         |                                 |



|     |       |     |
|-----|-------|-----|
| 225 | 605.3 | 101 |
| 230 | 604.6 | 101 |
| 235 | 605.3 | 101 |
| 240 | 605.5 | 101 |
| 245 |       |     |
| 250 |       |     |



COMPUTER INPUT DATA SHEET #1

3,5723

Client: JOTUL U.S.A., INC.

Address: 400 RIVERSIDE STREET  
PORTLAND, ME. 04104

3.42  
at 1.22 kg/hr

Phone: 207-999-5912 Fax: 207-772-0523

Run No.: 3 Date of Test: 4-11-2000 Burn Rate: 1.224

Model No.: F400  min  min-1.25  fan

Stove Type:  Cat  Non Cat  Pellet  1.25-1.9  max  insert

Dry Gas Meter: Y Factor: .989 Post Leak Rate: .002 cfm Time: 240 min.  
(0.000) (Data Sheet #2) (.000) (Data Sheet #2) (000) (Data Sheet #2)

Dry Gas Meter Volume: 75.294 cf  
(00.000) (Data Sheet #2)

Stack Flow: 8.570<sup>8.2</sup> dscfm  $\Delta$  H: .155 in. H<sub>2</sub>O  
(00.000) (Data Sheet #2) (.000) (Data Sheet #2)

Barometric Pressure: 30.09 in. Hg  
(00.00) (Data Sheet #2)

H<sub>2</sub>O Captured: 121.3 g  
(00.0) (Data Sheet #3)

Total Particulate Catch: .5022 g  
(0.0000) (Data Sheet #6)

Flue Gas Moisture: 7.3204 %  
(00.000) (Data Sheet #7)

Particulate Emission: 11072 gr/dscf  
(0.0000) (Data Sheet #7)

Ambient Moisture: 1.25 %  
(0.00) (Data Sheet #8)

Stove Weight: — lbs  
(000) (Data Sheet #8)

Total Fuel Consumed During Burn: 13.0 lbs  
(00.0) (Data sheet #8)

Fuel Higher Heating Value (dry): — BTU/lb  
(0000) (Data Sheet #8)

Fuel % Moisture (dry): 20.473 % (wet): 16.994 %  
(00.00) (Data Sheet #10)

Stack Static Pressure: -.041 in. H<sub>2</sub>O  
(0.000) (Data Sheet #12)

Temperature (Average Room) Combustion Air: 80 °F  
(00) Data Sheet #14)

Stove Temperature Change: -41.2 °F  
(00.0) (Data Sheet #14)





METER BOX DATA SHEET PAGE # 2

Page: 1 of 3

UNIT: F400 RUN: 3 DATE: 4-11-2000

Meter Box: 5H Y Factor: .989

Leak checks: 17 " Hg @ .001 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm

<sup>st</sup> 15 " Hg @ .002 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm

Inject SO<sub>2</sub> @ 100 cc/min. Nozzle: Probe @ 3/8" od Initial Volume: 1.500

| ROTO: PRESS: <u>.15</u> |      |               | SAMPLING RATIO: <u>29</u> : 1 |             |         | BP: <u>30.10</u> |         |            |           |  |
|-------------------------|------|---------------|-------------------------------|-------------|---------|------------------|---------|------------|-----------|--|
| MIN                     | TIME | METER READING | SAMPLE MDCF                   | STACK DSCFM | DELTA H | METER TEMP       | SO2 PPM | ROTO TEMP  | PUMP VACC |  |
| 0                       | 1400 | 307.500       | —                             | 8.673       | .15     | 81               | 400     | 81         | 1.0       |  |
| 5                       | 05   | 309.000       | —                             | 11.564      | .26     | 81               | 300     | 81         | 2.0       |  |
| 10                      | 10   | 311.036       | 311.036                       | 7.681       | .11     | 83               | 450     | 83         | 1.0       |  |
| 15                      | 15   | 312.405       | 312.405                       | 7.277       | .10     | 83               | 475     | 83         | 1.0       |  |
| 20                      | 20   | 313.702       | 313.702                       | 7.277       | .10     | 83               | 475     | 83         | 1.0       |  |
| 25                      | 25   | 314.998       | 314.998                       | 7.681       | .11     | 83               | 450     | 83         | 1.0       |  |
| 30                      | 30   | 316.367       | 316.367                       | 10.635      | .22     | 83               | 325     | 83         | 3.0       |  |
| 35                      | 35   | 318.261       | 318.261                       | 11.521      | .26     | 83               | 300     | 83         | 3.0       |  |
| 40                      | 40   | 320.312       | 320.312                       | 13.826      | .37     | 83               | 250     | 83         | 3.0       |  |
| 45                      | 45   | 322.773       | 322.773                       | 13.800      | .37     | 84               | 250     | 84         | 3.0       |  |
| 50                      | 50   | 325.242       | 325.242                       | 18.500      | .30     | 86               | 275     | 86         | 4.0       |  |
| 55                      | 55   | 327.504       | 327.504                       | 12.477      | .30     | 87               | 275     | 87         | 4.0       |  |
| ROTO PRESS: <u>.14</u>  |      |               | TOTALS: 124.912               |             |         | 2.65             | 1000    | BP.: 30.10 |           |  |
| 60                      | 1500 | 329.775       | 329.775                       | 12.477      | .30     | 87               | 275     | 87         | 4.0       |  |
| 65                      | 05   | 332.046       | 332.046                       | 12.477      | .30     | 87               | 275     | 87         | 4.0       |  |
| 70                      | 10   | 334.316       | 334.316                       | 12.477      | .30     | 87               | 275     | 87         | 4.0       |  |
| 75                      | 15   | 336.587       | 336.587                       | 10.557      | .21     | 87               | 325     | 87         | 4.0       |  |
| 80                      | 20   | 338.509       | 338.509                       | 9.803       | .19     | 87               | 350     | 87         | 3.0       |  |
| 85                      | 25   | 340.294       | 340.294                       | 9.149       | .16     | 87               | 375     | 87         | 3.0       |  |
| 90                      | 30   | 341.960       | 341.960                       | 9.803       | .19     | 87               | 350     | 87         | 3.0       |  |
| 95                      | 35   | 343.745       | 343.745                       | 9.803       | .19     | 87               | 350     | 87         | 3.0       |  |
| 100                     | 40   | 345.530       | 345.530                       | 9.821       | .19     | 86               | 350     | 86         | 3.0       |  |
| 105                     | 45   | 347.308       | 347.308                       | 9.821       | .19     | 86               | 350     | 86         | 3.0       |  |
| 110                     | 50   | 349.087       | 349.087                       | 9.821       | .19     | 86               | 350     | 86         | 3.0       |  |
| 115                     | 55   | 350.865       | 350.865                       | 9.821       | .19     | 86               | 350     | 86         | 2.0       |  |
|                         |      |               | TOTALS: 25.830                |             |         | 2.60             | 1040    | MAX VACC = |           |  |
| TOTAL Cu Ft.            |      |               | TOTALS: 250.742               |             |         | 5.25             | 2040    | AVG. BP:   |           |  |





METER BOX DATA SHEET PAGE # 2

Page: 2 of 3

UNIT: F400 RUN: 3

DATE: 4-11-00

Meter Box: SH Y Factor: .989

Leak checks: 17 " Hg @ .001 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm  
15 " Hg @ .002 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm

Inject SO<sub>2</sub> @ 100 cc/min. Nozzle : Probe @ 3/8 " od Initial Volume: 1.500

| ROTO: PRESS: <u>.14</u> |      | SAMPLING RATIO: <u>29</u> : 1 |             |             |         | BP: <u>30.08</u> |             |                       |           |  |
|-------------------------|------|-------------------------------|-------------|-------------|---------|------------------|-------------|-----------------------|-----------|--|
| MIN                     | TIME | METER READING                 | SAMPLE MDCF | STACK DSCFM | DELTA H | METER TEMP       | SO2 PPM     | ROTO TEMP             | PUMP VACC |  |
| 120                     | 1600 | 352.644                       | 352.644     | 9.160       | .16     | 86               | 375         | 86                    | 2.0       |  |
| 125                     | 05   | 354.305                       | 354.305     | 9.160       | .16     | 86               | 375         | 86                    | 2.0       |  |
| 130                     | 10   | 355.966                       | 355.966     | 8.588       | .14     | 86               | 400         | 86                    | 2.0       |  |
| 135                     | 15   | 357.524                       | 357.524     | 8.588       | .14     | 86               | 400         | 86                    | 2.0       |  |
| 140                     | 20   | 359.081                       | 359.081     | 8.588       | .14     | 86               | 400         | 86                    | 2.0       |  |
| 145                     | 25   | 360.639                       | 360.639     | 8.588       | .14     | 86               | 400         | 86                    | 2.0       |  |
| 150                     | 30   | 362.197                       | 362.197     | 8.588       | .14     | 86               | 400         | 86                    | 2.0       |  |
| 155                     | 35   | 363.754                       | 363.754     | 8.588       | .14     | 86               | 400         | 86                    | 2.0       |  |
| 160                     | 40   | 365.312                       | 365.312     | 8.588       | .14     | 86               | 400         | 86                    | 2.0       |  |
| 165                     | 45   | 366.869                       | 366.869     | 8.082       | .13     | 86               | 425         | 86                    | 2.0       |  |
| 170                     | 50   | 368.335                       | 368.335     | 7.232       | .10     | 86               | 475         | 86                    | 2.0       |  |
| 175                     | 55   | 369.647                       | 369.647     | 7.205       | .10     | 88               | 475         | 88                    | 2.0       |  |
| ROTO PRESS: <u>.14</u>  |      | TOTALS: <u>100.955</u>        |             |             |         | <u>1.63</u>      | <u>1034</u> | BP: <u>30.08</u>      |           |  |
| 180                     | 1700 | 370.969                       | 370.969     | 6.820       | .09     | 90               | 500         | 90                    | 2.0       |  |
| 185                     | 05   | 372.233                       | 372.233     | 5.931       | .07     | 90               | 525         | 90                    | 2.0       |  |
| 190                     | 10   | 373.333                       | 373.333     | 5.683       | .06     | 90               | 600         | 90                    | 2.0       |  |
| 195                     | 15   | 374.387                       | 374.387     | 5.237       | .05     | 91               | 650         | 91                    | 2.0       |  |
| 200                     | 20   | 375.364                       | 375.364     | 5.237       | .05     | 91               | 650         | 91                    | 2.0       |  |
| 205                     | 25   | 376.340                       | 376.340     | 5.237       | .05     | 91               | 650         | 91                    | 2.0       |  |
| 210                     | 30   | 377.317                       | 377.317     | 5.043       | .05     | 91               | 675         | 91                    | 2.0       |  |
| 215                     | 35   | 378.257                       | 378.257     | 5.043       | .05     | 91               | 675         | 91                    | 2.0       |  |
| 220                     | 40   | 379.198                       | 379.198     | 4.863       | .05     | 91               | 700         | 91                    | 2.0       |  |
| 225                     | 45   | 380.105                       | 380.105     | 4.863       | .05     | 91               | 700         | 91                    | 2.0       |  |
| 230                     | 50   | 381.011                       | 381.011     | 4.863       | .05     | 91               | 700         | 91                    | 2.0       |  |
| * 235                   | 55   | 381.918                       | 381.918     | 4.695       | .04     | 91               | 725         | 91                    | 2.0       |  |
|                         |      | TOTALS: <u>63,515</u>         |             |             |         | <u>1.660</u>     | <u>1089</u> | MAX VACC =            |           |  |
| TOTAL Cu Ft.            |      | TOTALS: <u>164,470</u>        |             |             |         | <u>2.29</u>      | <u>2123</u> | AVG. BP: <u>30.09</u> |           |  |



METER BOX DATA SHEET PAGE # 2

Page: 3 of 3

UNIT: F400 RUN: 3 DATE: 4-11-00

Meter Box: 5H Y Factor: .989

Leak checks: 17 " Hg @ .001 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm  
15 " Hg @ .002 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm

Inject SO<sub>2</sub> @ 100 cc/min. Nozzle: Probe @ 3/8 " od Initial Volume: 1.500

| ROTO: PRESS: <u>.14</u> |      | SAMPLING RATIO: <u>29</u> : 1 |             |             |         | BP: <u>30.08</u> |            |                |           |
|-------------------------|------|-------------------------------|-------------|-------------|---------|------------------|------------|----------------|-----------|
| MIN                     | TIME | METER READING                 | SAMPLE MDCF | STACK DSCFM | DELTA H | METER TEMP       | SO2 PPM    | ROTO TEMP      | PUMP VACC |
| 240                     | 1800 | 382.794                       | 382.794     | 4.695       | .04     | 91               | 725        | 91             | 2.0       |
| 245                     |      |                               |             |             |         |                  |            |                |           |
| 250                     |      |                               |             |             |         |                  |            |                |           |
| 255                     |      |                               |             |             |         |                  |            |                |           |
| 260                     |      |                               |             |             |         |                  |            |                |           |
| 265                     |      |                               |             |             |         |                  |            |                |           |
| 270                     |      |                               |             |             |         |                  |            |                |           |
| 275                     |      |                               |             |             |         |                  |            |                |           |
| 280                     |      |                               |             |             |         |                  |            |                |           |
| 285                     |      |                               |             |             |         |                  |            |                |           |
| 290                     |      |                               |             |             |         |                  |            |                |           |
| 295                     |      |                               |             |             |         |                  |            |                |           |
| ROTO PRESS:             |      |                               | TOTALS:     |             |         | BP.:             |            |                |           |
| 300                     |      |                               |             |             |         |                  |            |                |           |
| 305                     |      |                               |             |             |         |                  |            |                |           |
| 310                     |      |                               |             |             |         |                  |            |                |           |
| 315                     |      |                               |             |             |         |                  |            |                |           |
| 320                     |      |                               |             |             |         |                  |            |                |           |
| 325                     |      |                               |             |             |         |                  |            |                |           |
| 330                     |      |                               |             |             |         |                  |            |                |           |
| 335                     |      |                               |             |             |         |                  |            |                |           |
| 340                     |      |                               |             | 4.49        |         |                  |            |                |           |
| 345                     |      |                               |             |             |         |                  |            |                |           |
| 350                     |      |                               |             |             |         |                  |            |                |           |
| 355                     |      |                               |             | 419.907     | 7.58    | 4254             |            |                |           |
|                         |      |                               | TOTALS:     |             |         | 87               | MAX VACC = |                | 4.0       |
| TOTAL Cu Ft.            |      | 75.294                        | TOTALS:     |             | 8.570   | .155             | 547        | AVG. BP: 30.09 |           |





**PARTICULATE CATCH / MOISTURE DATA SHEET # 3**

UNIT: F400 RUN: 3 DATE: 4/11/00

| SCALE CHECK | LEVEL | ZEROED |
|-------------|-------|--------|
| INITIAL :   | ✓     | ✓      |
| FINAL :     | ✓     | ✓      |

| SCALE   | WEIGHT |
|---------|--------|
| 295.0 g | 295.0  |
| 590.0 g | 590.0  |
| 885.0 g | 885.0  |

| IMPINGER     | #1    | #2    | #3    | #4    |
|--------------|-------|-------|-------|-------|
| FINAL WT     | 685.4 | 601.0 | 516.2 | 882.8 |
| INITIAL WT   | 589.8 | 593.6 | 513.6 | 867.1 |
| NET WT GRAMS | 95.6  | 7.4   | 2.6   | 15.7  |

TOTAL CATCH: 121.3 GRAMS H<sub>2</sub>O

**FRONT HALF**

|              |       |  |
|--------------|-------|--|
| FILTER #     | 20F   |  |
| FINAL WT g   | .7509 |  |
| INITIAL WT g | .6655 |  |
| NET WT g     | .0854 |  |

|               |         |
|---------------|---------|
| BEAKER #      | 61      |
| DESC.         | ACETONE |
| FINAL WT g    | 99.3877 |
| INITIAL WT g  | 99.3467 |
| NET WT g      | .0410   |
| VOL. DESC. ml | 100     |

**BACK HALF**

|              |       |  |
|--------------|-------|--|
| FILTER #     | 20B   |  |
| FINAL WT g   | .4940 |  |
| INITIAL WT g | .4340 |  |
| NET WT g     | .0600 |  |

| BEAKER #     | 62      | 63        | 64               | 65               |       |
|--------------|---------|-----------|------------------|------------------|-------|
| DESC.        | ACETONE | METHCHLOR | H <sub>2</sub> O | H <sub>2</sub> O |       |
| FINAL WT g   | 98.0370 | 93.2640   | 104.8304         | 98.5022          |       |
| INITIAL WT g | 97.8657 | 93.2146   | 104.7866         | 98.4461          |       |
| NET WT g     | .1713   | .0494     | .0438            | .0561            | .0999 |
| VOL. DESC ml | 175     | 75        | 150              | 175              | (325) |



**WOODSTOVE DATA SHEET #4-1  
INITIAL FILTER WEIGHTS (TARE WEIGHTS)**

Into Dessicator: Date 10-28-99 Time: 1725 By: MAJ  
 Manufacturer: S+S Grade: #25 GLASS Front Size: 11CM Lot No.: ZB921  
 Back Size: 8.2CM Lot No.: ZB911

| FILTER # | FIRST WEIGHT | TIME | SECOND WEIGHT | TIME | THIRD WEIGHT   | TIME |
|----------|--------------|------|---------------|------|----------------|------|
| 11B      | .4291        | 1911 | .4291         | 1818 | TOTAL #3CB R#4 |      |
| 12B      | .4316        | 1912 | .4313         | 1819 | TOTAL #3CB R#1 |      |
| 13B      | .4299        | 1913 | .4298         | 1820 | TOTAL #3CB R#2 |      |
| 14B      | .4306        | 1914 | .4306         | 1821 | TOTAL #3CB R#3 |      |
| 15B      | .4313        | 1915 | .4313         | 1822 | TOTAL #3CB R#4 |      |
| 16B      | .4319        | 1916 | .4315         | 1822 |                |      |
| 17B      | .4278        | 1916 | .4277         | 1823 |                |      |
| 18B      | .4302        | 1917 | .4300         | 1824 | TOTAL F400 R#1 |      |
| 19B      | .4288        | 1918 | .4285         | 1825 | TOTAL F400 R#2 |      |
| 20B      | .4340        | 1919 | .4340         | 1826 | TOTAL F400 R#3 |      |

|     |       |      |       |      |                |  |
|-----|-------|------|-------|------|----------------|--|
| 11F | .6660 | 1928 | .6659 | 1835 | TOTAL #3CB R#4 |  |
| 12F | .6837 | 1929 | .6833 | 1836 | TOTAL #3CB R#1 |  |
| 13F | .6707 | 1930 | .6704 | 1837 | TOTAL #3CB R#2 |  |
| 14F | .6719 | 1931 | .6722 | 1838 | TOTAL #3CB R#3 |  |
| 15F | .6672 | 1932 | .6674 | 1839 | TOTAL #3CB R#4 |  |
| 16F | .6809 | 1933 | .6806 | 1840 |                |  |
| 17F | .6657 | 1934 | .6654 | 1840 |                |  |
| 18F | .6693 | 1935 | .6690 | 1841 | TOTAL F400 R#1 |  |
| 19F | .6744 | 1935 | .6745 | 1842 | TOTAL F400 R#2 |  |
| 20F | .6654 | 1936 | .6655 | 1843 | TOTAL F400 R#3 |  |

Checked by: Optimizing Date: 11-4-99 Time: 1905

**BALANCE ROOM ENVIRONMENTAL CONDITIONS**

| DATE | TIME | BY  | WB | DB | % RH |
|------|------|-----|----|----|------|
| 11-1 | 1815 | MAJ | 5  | 73 | 46   |
| 11-4 | 1805 | MAJ | 5  | 70 | 46   |











WOODSTOVE DATA SHEET # 4-3 : CONSTANT WEIGHTS

4.11-00

F400

RUN : 3

DATE :

UNIT :

| Beaker # | Date | Time | By             | First Weight | Date | Time | By             | Second Weight | Date | Time | By             | Third Weight | Date | Time | By |
|----------|------|------|----------------|--------------|------|------|----------------|---------------|------|------|----------------|--------------|------|------|----|
| 61       | 4-12 | 1040 | <del>RAW</del> | 99.3874      | 4-13 | 2146 | <del>RAW</del> | 99.3877       | 4-15 | 1645 | <del>RAW</del> |              |      |      |    |
| 62       | 4-12 | 1040 | <del>RAW</del> | 98.0374      | 4-13 | 2141 | <del>RAW</del> | 98.0370       | 4-15 | 1647 | <del>RAW</del> |              |      |      |    |
| 63       | 4-12 | 1645 | <del>RAW</del> | 93.2638      | 4-13 | 2143 | <del>RAW</del> | 93.2640       | 4-15 | 1648 | <del>RAW</del> |              |      |      |    |
| 64       | 4-12 | 1040 | <del>RAW</del> | 104.8300     | 4-13 | 2144 | <del>RAW</del> | 104.8304      | 4-15 | 1649 | <del>RAW</del> |              |      |      |    |
| 65       | 4-12 | 1040 | <del>RAW</del> | 98.5018      | 4-13 | 2145 | <del>RAW</del> | 98.5022       | 4-15 | 1650 | <del>RAW</del> |              |      |      |    |

| Filter # | Date | Time | By | First Weight | Date | Time | By             | Second Weight | Date | Time | By             | Third Weight | Date | Time | By |
|----------|------|------|----|--------------|------|------|----------------|---------------|------|------|----------------|--------------|------|------|----|
| 20F      | 4-11 | 1840 | CP | .7514        | 4-12 | 1739 | <del>RAW</del> | .7509         | 4-13 | 2147 | <del>RAW</del> |              |      |      |    |
| 20B      | 4-11 | 1840 | CP | .4942        | 4-12 | 1740 | <del>RAW</del> | .4940         | 4-13 | 2148 | <del>RAW</del> |              |      |      |    |

SCALE ROOM ENVIRONMENTAL CONDITIONS

| Weighing Session | Date | Time | By             | WB | DB | %RH |
|------------------|------|------|----------------|----|----|-----|
| 1                | 4-12 | 1730 | <del>RAW</del> |    | 77 | 49  |
| 2                | 4-13 | 2130 | <del>RAW</del> |    | 76 | 48  |
| 3                | 4-14 | 1640 | <del>RAW</del> |    | 75 | 49  |
| 4                |      |      |                |    |    |     |

| Weighing Session | Date | Time | By | WB | DB | %RH |
|------------------|------|------|----|----|----|-----|
| 5                |      |      |    |    |    |     |
| 6                |      |      |    |    |    |     |
| 7                |      |      |    |    |    |     |
| 8                |      |      |    |    |    |     |



### BLANK PROCESSING DATA SHEET # 5

UNIT: F400 RUN: 3 DATE: 4-11-2000

BLANKS DONE: 12-27-99

| BEAKER       | A              | B             | C            |
|--------------|----------------|---------------|--------------|
|              | 200 ml ACETONE | 75 ml DICHLOR | 200 ml WATER |
|              | FISHER OPTIMA  | FISHER OPTIMA |              |
|              | LOT #          | LOT #         |              |
| FINAL WEIGHT | 108.9011       | 106.3073      | 106.9666     |
| TARE WEIGHT  | 108.9003       | 106.3062      | 106.9651     |
| NET WEIGHT   | .0008          | .0011         | .0015        |

TARE BEAKERS INTO DESC: TIME: 11:30 DATE: 12-20-99

DATE: 1222 BY: NW DATE: 1223 BY: NW DATE: \_\_\_\_\_ BY: \_\_\_\_\_

| BEAKER | 1 ST WT  | TIME | 2 ND WT  | TIME | 3 RD WT | TIME |
|--------|----------|------|----------|------|---------|------|
| A      | 108.8999 | 1940 | 108.9003 | 1948 | ✓       |      |
| B      | 106.3058 | 1941 | 106.3062 | 1949 | ✓       |      |
| C      | 106.9647 | 1942 | 106.9651 | 1950 | ✓       |      |

FINAL BEAKERS INTO DESC: TIME: 1330 DATE: 12-24-99

DATE: 12-24 BY: NW DATE: 12-25 BY: NW DATE: 12-27 BY: NW

| BEAKER | 1 ST WT  | TIME | 2 ND WT  | TIME | 3 RD WT  | TIME   |
|--------|----------|------|----------|------|----------|--------|
| A      | 108.8999 | 2021 | 108.9016 | 1816 | 108.9011 | 1224 ✓ |
| B      | 106.3061 | 2022 | 106.3077 | 1817 | 106.3073 | 1225 ✓ |
| C      | 106.9643 | 2023 | 106.9670 | 1818 | 106.9666 | 1226 ✓ |

**TARE QC**

| DATE  | TIME | BY | WB | DB | %  |
|-------|------|----|----|----|----|
| 12-22 | 1935 | NW | }  | 77 | 47 |
| 12-23 | 1945 | NW |    | 75 | 48 |
|       |      |    |    |    |    |

**FINAL QC**

| DATE  | TIME | BY | WB | DB | %  |
|-------|------|----|----|----|----|
| 12-24 | 1945 | NW | }  | 76 | 45 |
| 12-25 | 1740 | NW |    | 75 | 38 |
| 12-27 | 1210 | NW |    | 76 | 46 |





# NET PARTICULATE CATCH CALCULATION DATA SHEET #6

UNIT: F400 RUN: 3 DATE: 4-11-2000

## BLANK CALCULATIONS

Acetone : .0008 g ÷ 200 ml = .000004 g/ml  
 Dichloromethane : .0011 g ÷ 75 ml = .000015 g/ml  
 Distilled Water : .0015 g ÷ 200 ml = .000008 g/ml

## FRONT HALF CATCH

FILTERS : .0854 g - 1 (# of Filters) (.0000 g) = .0854 g  
Total Catch Blank Value / Filter

BEAKERS : .0410 g - 100 ml Acetone (.00004 g) = .0406 g  
Total Catch Blank Value / ml Acetone

TOTAL FRONT HALF CATCH : .1260 g

## BACK HALF CATCH

FILTERS : .0600 g - 1 (# of Filters) (.0000 g) = .0600 g  
Total Catch Blank Value / Filter

BEAKERS :

Acetone : .1713 g - 175 ml Acetone (.00004 g) = .1706 g  
Total Catch Blank Value / ml Acetone

Extract : .0494 g - 75 ml Dichloromethane (.000015 g) = .0483 g  
Total Catch Blank Value / Dichloromethane

Water : .0999 g - 325 ml Water (.000008 g) = .0973 g  
Total Catch Blank Value / Water

TOTAL BACK HALF CATCH : .3762 g

TOTAL CATCH : .5022 g

% FRONT HALF : 25.09 %





CALCULATIONS DATA SHEET # 7

UNIT: F400 RUN: 3 DATE: 4-11-2000

$$1) Vm(\text{std}) = \frac{(75.294 \text{ Vm})(17.64)(.989 \text{ mcf}) \left( \overset{30.1014}{30.09} \text{ " Hg} + \frac{.155 \text{ " H}_2\text{O}}{13.6} \right)}{(\underline{547} \text{ TmA})} = \frac{72.2861}{000.0000} \text{ dscf}$$

$$2) Vw(\text{std}) = (.04707)(\underline{121.3} \text{ ml H}_2\text{O}) = \frac{5.7096}{00.0000} \text{ scf}$$

$$3) Asw = \frac{(\underline{5.7096} \text{ scf})}{(\underline{5.7096} \text{ scf} + \frac{72.2861}{77.9957} \text{ dscf})} = \frac{.0732}{.0000} \text{ Bws} \times 100 = \frac{7.3204}{00.0000} \% \text{ H}_2\text{O}$$

$$4) Cs = \frac{(\underline{.5022} \text{ g.})}{(\underline{72.2861} \text{ dscf})} (15.43) = \frac{.1072}{0.0000} \text{ gr / dscf}$$

$$5) \text{ Estimated g / hr} = \frac{(\underline{.5022} \text{ g.})}{(\underline{72.2861} \text{ dscf})} (\underline{8.570} \text{ dscfm}) (60) = \frac{3.5723}{00.0000} \text{ g / hr}$$

|                       |   |        |                             |
|-----------------------|---|--------|-----------------------------|
| Vm =                  | total cubic feet pulled on meter box during test                | (p. 2) | (000.000 Vm)                |
| mcf =                 | meter correction factor ( Y factor ) of meter box used for test | (p. 2) | (0.000 mcf)                 |
| " Hg =                | average barometric pressure during test                         | (p. 2) | (00.00 " Hg)                |
| " H <sub>2</sub> O =  | average delta H for test  | (p. 2) | (.000 " H <sub>2</sub> O)   |
| TmA =                 | average meter temperature for test in degrees Absolute          | (p. 2) | (000 TmA)                   |
| ml H <sub>2</sub> O = | total water caught during test                                  | (p. 3) | (000.0 ml H <sub>2</sub> O) |
| g. =                  | total particulate catch for test                                | (p. 6) | (00.0000 g.)                |
| dscfm =               | average stack flow during test                                  | (p. 2) | (00.000 dscf)               |



## TEST DATA SHEET # 8

UNIT : F400 RUN : 3 DATE : 4-11-2000

Test Chamber Air Velocity Start : ∅ Stop : ∅ Avg.: ∅

Wet Bulb / Dry Bulb Pre : WB : 60 DB : 74 = 43 % RH 1.3 % H<sub>2</sub>O

Post : WB : 61 DB : 78 = 36 % RH 1.2 % H<sub>2</sub>O

Average : 39.5 %RH 1.25 % H<sub>2</sub>O

Empty Stove Weight (lbs) : - w/ stack & oil seal : Wet : - Dry : 390.0

Kindling Weight (lbs) : Paper : .1 Wood : 3.2

Preburn Fuel Weight : 14.7 + 11.7 + 8.5 + 3.5 Total : 38.4

Kindling & Preburn Fuel Weight (wood only) (lbs) : Total : 41.6

Coal Bed Wt Range (lbs) : 3.2 - 2.6 Scale : 393.2 - 392.6

Upper : .25 x fuel weight : Always round DOWN to nearest tenth  
 Lower : .20 x fuel weight : Always round UP to nearest tenth Actual Coal Bed Weight : 2.8

Maximum Coal Bed Removal (lbs) :  $((\frac{3.2}{\text{Upper}} + \frac{2.6}{\text{Lower}}) \div 2) \cdot .25 =$  .7

Test Fuel (.75" x 1.5" x 5" spacers) = 20 pcs

| Dimensions | Length in inches | No. Pcs | Weight in lbs | % of Load |
|------------|------------------|---------|---------------|-----------|
| 2" x 4"    | 13               | 3       | 5.3           | 40.8      |
| 4" x 4"    | 13               | 2       | 7.7           | 59.2      |

Test Fuel Weight : 13.0 lbs

Estimated Dry Burn Rate :  $\frac{13.0 - (13.0 \times \frac{2209}{16994})}{2.2046} \times \frac{60}{\frac{240}{\text{TIME}}} =$  1.224 kg/hr

Estimated BTU's/hr :  $19,140 \times \frac{63}{100} \times \frac{1.224}{\text{DBR}} =$  14,759.24 BTU's/hr





WOOD STOVE OPERATING DATA PAGE #9

Unit: F400 Run: 3 Date: 4-11-2000

FIRE STARTED: 0835

WARM UP AND PREBURN:

PRIMARY AIR: Set wide open for all warm-up / preburn fuel charges. Then set to 1/8" at start of preburn.

SECONDARY AIR: N/A CAT BYPASS: N/A

CHARCOAL BED PREPARATION:

Raked and leveled prior to each warm-up / preburn charge. At 1 1/2 min. prior to loading last fuel, raked and leveled. In stove 35 sec.

TEST:

DOOR wide open during loading 0 min. 55 sec.

PRIMARY AIR: Opened full for first 5 min., then set to run setting of 1/8"

SECONDARY AIR: N/A CAT BYPASS: N/A

FAN:

ON / OFF during warm-up

ON / OFF during preburn

ON / OFF first        minutes of test

ON / OFF balance of test run

Fan speed set at N/A

WOOD DATA: KINDLING: A mix of the grades listed below:

|          | SIZE | MILL         | GRADE          | SPECIES      |
|----------|------|--------------|----------------|--------------|
| PREBURN: | 2x4  | Manke/Tacoma | Std. or better | s. grn D fir |
| TEST:    | 2x4  | Packwood     | # 2 or better  | s. grn D fir |
|          | 4x4  | Packwood     | # 2 or better  | s. grn D fir |

PELLET FUEL MANUFACTURER: N/A BRAND: N/A

All Grades WCLB rules:

WARM UP INFORMATION:

All pre-burn / warm up fuel pieces were either 12 or 16 inches.

1st warm up / pre-burn fuel charge (14.7 lbs.) added at 0845

2nd warm up / pre-burn fuel charge (11.7 lbs.) added at 0955

3rd warm up / pre-burn fuel charge (8.5 lbs.) added at 1110

4th warm up / pre-burn fuel charge (3.5 lbs.) added at 1240

5th warm up / pre-burn fuel charge (       lbs.) added at



### TEST DATA SHEET #10

Unit : F400 Run : 3 Date : 4 - -2000

Room Temperature : 71 °F Correction Factor : 4

Uncorrected Values are corrected for room temperature : Yes \_\_\_\_\_ No ✓

Time Test Fuel moisture reading taken : 1105

Calibration Checks : X ✓ Y ✓ 12.0 12.2 22.0 22.0

| pc # | Dimen.   | Use | TOP   |      | BOTTOM |      | SIDE   |      | Avg Corrected |
|------|----------|-----|-------|------|--------|------|--------|------|---------------|
|      |          |     | Uncor | Cor. | Uncor. | Cor. | Uncor. | Cor. |               |
| 1    | 2"x4"x8' | K   | 14.5  | 15.5 | 16.0   | 17.0 | 15.5   | 16.5 | 16.333        |
| 2    |          |     |       |      |        |      |        |      |               |
| 3    |          |     |       |      |        |      |        |      |               |
| 4    | 2"x4"x8' | P   | 18.5  | 19.8 | 19.0   | 20.3 | 19.0   | 20.3 | 20.133        |
| 5    | 2"x4"x8' | P   | 20.0  | 21.4 | 20.0   | 21.4 | 20.0   | 21.4 | 21.400        |
| 6    | 2"x4"x8' | P   | 22.0  | 23.7 | 21.0   | 22.5 | 20.5   | 22.0 | 22.733        |
| 7    | 2"x4"x8' | P   |       |      |        |      |        |      | 64.266        |
| 8    | 2"x4"x8' | P   |       |      |        |      |        |      |               |
| 9    |          |     |       |      |        |      |        |      |               |
| 10   |          |     |       |      |        |      |        |      |               |
| 11   |          |     |       |      |        |      |        |      |               |
| 12   | 2x4x13   | T   | 19.5  | 20.9 | 19.0   | 20.3 | 19.5   | 20.9 | 20.700        |
| 13   | "        | T   | 18.0  | 19.2 | 17.5   | 18.7 | 18.0   | 19.2 | 19.033        |
| 14   | "        | T   | 20.0  | 21.4 | 19.5   | 20.9 | 20.0   | 21.4 | 21.233        |
| 15   | 4x4x13   | T   | 21.0  | 22.5 | 20.5   | 22.0 | 21.5   | 23.1 | 22.533        |
| 16   | "        | T   | 18.0  | 19.2 | 17.5   | 18.7 | 17.5   | 18.7 | 18.867        |
| 17   |          |     |       |      |        |      |        |      | 102.366       |
| 18   |          |     |       |      |        |      |        |      |               |
| 19   |          |     |       |      |        |      |        |      |               |
| 20   | Spacers  | T   | 18.5  | 19.8 | 19.0   | 20.3 | 18.0   | 19.2 | 19.767        |

Key for Use : K = Kindling P = Pretest Fuel T = Test Fuel

|                  | KINDLING | PRETEST FUEL | TEST FUEL |
|------------------|----------|--------------|-----------|
| Dry Moisture % : | 16.333 % | 21.422 %     | 20.473 %  |
| Wet Moisture % : | 14.040 % | 17.643 %     | 16.994 %  |

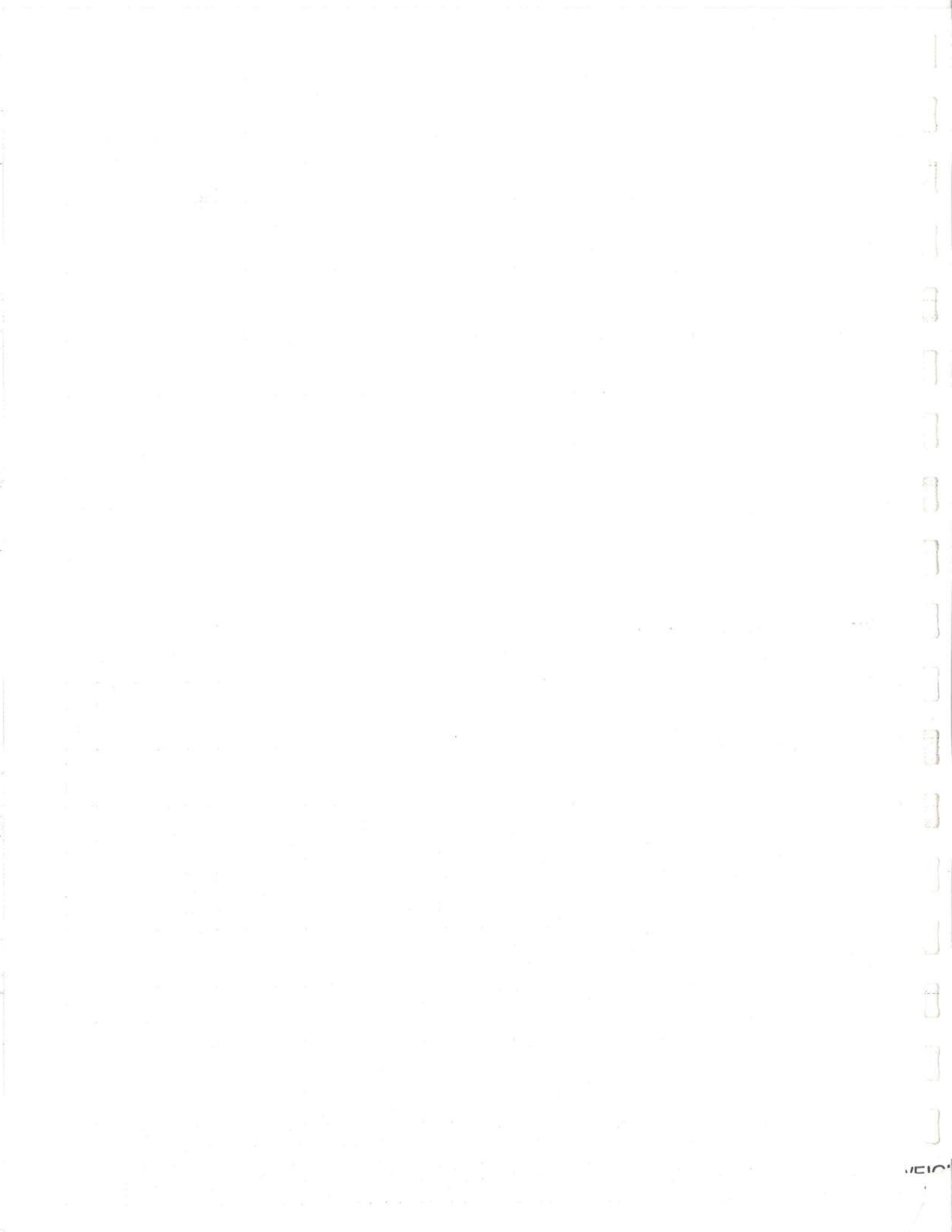
To obtain Wet from Dry :  $\frac{100 \times \% \text{ Dry Reading}}{100 + \% \text{ Dry Reading}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges : 16 - 20 % wet: 19 - 25 % dry (17.5 - 22.5 on Meter Uncor. reading) at 70°





| TIME  | SCALE | FUEL | DROP | V.   | CO <sub>2</sub> | V.   | O <sub>2</sub> | V.   | CO   | BAL   | WB | DB | % H <sub>2</sub> O | CAL WB | STACK | STATIC | SO <sub>2</sub> PPM |
|-------|-------|------|------|------|-----------------|------|----------------|------|------|-------|----|----|--------------------|--------|-------|--------|---------------------|
| 0     | 405.8 | 13.0 | -    | .203 | 5.1             | .203 | -              | .103 | 1.03 | 4.9   |    |    |                    |        | 300   | 7039   | 400                 |
| 5     | 405.4 | 12.6 | .4   | .103 | 2.5             | .103 |                | .034 | .34  | 7.4   |    |    |                    |        | 334   | 7033   | 300                 |
| 10    | 405.2 | 12.4 | .2   | .081 | 2.0             | .081 |                | .061 | .61  | 3.2   |    |    |                    |        | 255   | 7035   | 450                 |
| 15    | 405.1 | 12.3 | .1   | .075 | 1.8             | .075 |                | .061 | .61  | 3.0   |    |    |                    |        | 228   | 7032   | 475                 |
| 20    | 404.9 | 12.1 | .2   | .078 | 1.9             | .078 |                | .071 | .71  | 2.7   |    |    |                    |        | 217   | 7031   | 475                 |
| 25    | 404.7 | 11.9 | .2   | .141 | 3.5             | .141 |                | .080 | .80  | 4.3   |    |    |                    |        | 221   | 7031   | 450                 |
| 30    | 404.0 | 11.2 | .7   | .517 | 12.9            | .517 |                | .064 | .64  | 20.1  |    |    |                    |        | 467   | .051   | 325                 |
| 35    | 403.2 | 10.4 | .8   | .395 | 9.9             | .395 |                | .055 | .55  | 17.8  |    |    |                    |        | 490   | 7056   | 300                 |
| 40    | 402.2 | 9.4  | 1.0  | .519 | 13.0            | .519 |                | .011 | .11  | 113.9 |    |    |                    |        | 597   | 7063   | 250                 |
| 45    | 401.5 | 8.7  | .7   | .478 | 12.0            | .478 |                | .007 | .07  | 161.6 |    |    |                    |        | 578   | 7062   | 250                 |
| 50    | 400.6 | 7.8  | .9   | .553 | 13.8            | .553 |                | .006 | .06  | 216.3 |    |    |                    |        | 621   | 7065   | 275                 |
| 55    | 399.8 | 7.0  | .8   | .547 | 13.7            | .547 |                | .005 | .05  | 253.5 |    |    |                    |        | 627   | 7066   | 275                 |
| TOTAL |       |      |      |      |                 |      |                |      |      |       |    |    |                    |        | 4935  | -564   |                     |
| 60    | 399.0 | 6.2  | .8   | .546 | 13.7            | .546 |                | .003 | .03  | 401.9 |    |    |                    |        | 619   | 7066   | 275                 |
| 65    | 398.2 | 5.4  | .8   | .562 | 14.1            | .562 |                | .003 | .03  | 413.7 |    |    |                    |        | 627   | 7066   | 275                 |
| 70    | 397.5 | 4.7  | .7   | .465 | 11.6            | .465 |                | .007 | .07  | 157.2 |    |    |                    |        | 542   | 7065   | 275                 |
| 75    | 397.1 | 4.3  | .4   | .361 | 9.0             | .361 |                | .047 | .47  | 19.0  |    |    |                    |        | 524   | 7063   | 325                 |
| 80    | 396.6 | 3.8  | .5   | .334 | 8.3             | .334 |                | .063 | .63  | 13.2  |    |    |                    |        | 481   | 7058   | 350                 |
| 85    | 396.3 | 3.5  | .3   | .320 | 8.0             | .320 |                | .060 | .60  | 13.2  |    |    |                    |        | 452   | 7055   | 375                 |
| 90    | 396.0 | 3.2  | .3   | .312 | 7.8             | .312 |                | .066 | .60  | 12.9  |    |    |                    |        | 439   | 7054   | 350                 |
| 95    | 395.7 | 2.9  | .3   | .305 | 7.6             | .305 |                | .056 | .56  | 13.5  |    |    |                    |        | 425   | 7052   | 350                 |
| 100   | 395.4 | 2.6  | .3   | .297 | 7.4             | .297 |                | .059 | .59  | 12.5  |    |    |                    |        | 414   | 7051   | 350                 |
| 105   | 395.2 | 2.4  | .2   | .291 | 7.3             | .291 |                | .045 | .65  | 11.1  |    |    |                    |        | 406   | 7050   | 350                 |
| 110   | 394.9 | 2.1  | .3   | .306 | 7.6             | .306 |                | .055 | .55  | 13.8  |    |    |                    |        | 408   | 7050   | 350                 |
| 115   | 394.7 | 1.9  | .2   | .276 | 6.9             | .276 |                | .069 | .69  | 9.9   |    |    |                    |        | 389   | 7049   | 350                 |
| TOTAL |       |      |      |      |                 |      |                |      |      |       |    |    |                    |        | 5726  | -679   |                     |
| TOTAL |       |      |      |      |                 |      |                |      |      |       |    |    |                    |        | 10661 | -1.243 |                     |





VEIGHI: 39:28

WAS LUNA UNSET # 12

UNIT: F400

RUN: 3 DATE: 4-11-2000 PAGE: 2 of 3

| TIME  | SCALE | FUEL | DROP | V.    | CO <sub>2</sub> | V.    | O <sub>2</sub> | V.    | CO    | BAL   | WB    | DB    | % H <sub>2</sub> O | CAL WB | STACK | STATIC | SO <sub>2</sub> PPM |
|-------|-------|------|------|-------|-----------------|-------|----------------|-------|-------|-------|-------|-------|--------------------|--------|-------|--------|---------------------|
| 120   | 394.5 | 1.7  | .2   | .268  | 6.7             | -     | -              | .071  | .71   | 9.4   | -     | -     | -                  | -      | 378   | 7048   | 375                 |
| 125   | 394.4 | 1.6  | .1   | .253  | 6.3             | -     | -              | .084  | .86   | 7.3   | -     | -     | -                  | -      | 371   | 7046   | 375                 |
| 130   | 394.3 | 1.5  | .1   | .227  | 5.7             | -     | -              | .129  | 1.29  | 4.4   | -     | -     | -                  | -      | 344   | 7041   | 400                 |
| 135   | 394.2 | 1.4  | .1   | .221  | 5.5             | -     | -              | .142  | 1.42  | 3.9   | -     | -     | -                  | -      | 330   | 7042   | 400                 |
| 140   | 394.1 | 1.3  | .1   | .214  | 5.3             | -     | -              | .149  | 1.49  | 3.6   | -     | -     | -                  | -      | 319   | 7041   | 400                 |
| 145   | 394.0 | 1.2  | .1   | .219  | 5.5             | -     | -              | .152  | 1.52  | 3.6   | -     | -     | -                  | -      | 311   | 7039   | 400                 |
| 150   | 393.9 | 1.1  | .1   | .208  | 5.2             | -     | -              | .146  | 1.66  | 3.1   | -     | -     | -                  | -      | 302   | 7038   | 400                 |
| 155   | 393.8 | 1.0  | .1   | .200  | 5.0             | -     | -              | .176  | 1.76  | 2.8   | -     | -     | -                  | -      | 296   | 7036   | 400                 |
| 160   | 393.7 | .9   | .1   | .197  | 4.9             | -     | -              | .176  | 1.76  | 2.8   | -     | -     | -                  | -      | 292   | 7036   | 400                 |
| 165   | 393.7 | .9   | 0    | .220  | 5.5             | -     | -              | .141  | 1.41  | 3.9   | -     | -     | -                  | -      | 287   | 7035   | 425                 |
| 170   | 393.6 | .8   | .1   | .213  | 5.3             | -     | -              | .146  | 1.46  | 3.6   | -     | -     | -                  | -      | 272   | 7033   | 475                 |
| 175   | 393.5 | .7   | .1   | .211  | 5.3             | -     | -              | .153  | 1.53  | 3.4   | -     | -     | -                  | -      | 267   | 7031   | 475                 |
| TOTAL | ***** | **** | **** | ***** | *****           | ***** | *****          | ***** | ***** | ***** | ***** | ***** | *****              | *****  | 3769  | 7469   | *****               |
| 180   | 393.4 | .6   | .1   | .212  | 5.3             | -     | -              | .127  | 1.27  | 4.1   | -     | -     | -                  | -      | 264   | -0.31  | 500                 |
| 185   | 393.3 | .5   | .1   | .199  | 5.0             | -     | -              | .138  | 1.38  | 3.6   | -     | -     | -                  | -      | 244   | -0.28  | 575                 |
| 190   | 393.3 | .5   | 0    | .189  | 4.7             | -     | -              | .123  | 1.23  | 3.8   | -     | -     | -                  | -      | 234   | 7027   | 600                 |
| 195   | 393.2 | .4   | .1   | .198  | 4.9             | -     | -              | .117  | 1.17  | 4.2   | -     | -     | -                  | -      | 221   | 7025   | 650                 |
| 200   | 393.2 | .4   | 0    | .198  | 4.9             | -     | -              | .117  | 1.17  | 4.2   | -     | -     | -                  | -      | 219   | 7025   | 650                 |
| 205   | 393.2 | .4   | 0    | .190  | 4.7             | -     | -              | .128  | 1.28  | 3.7   | -     | -     | -                  | -      | 216   | 7024   | 650                 |
| 210   | 393.1 | .3   | .1   | .191  | 4.7             | -     | -              | .131  | 1.31  | 3.6   | -     | -     | -                  | -      | 213   | 7024   | 675                 |
| 215   | 393.0 | .2   | .1   | .191  | 4.7             | -     | -              | .151  | 1.51  | 3.1   | -     | -     | -                  | -      | 210   | 7024   | 675                 |
| 220   | 393.0 | .2   | 0    | .179  | 4.4             | -     | -              | .161  | 1.61  | 2.8   | -     | -     | -                  | -      | 208   | 7023   | 700                 |
| 225   | 392.9 | .1   | .1   | .168  | 4.2             | -     | -              | .169  | 1.69  | 2.5   | -     | -     | -                  | -      | 203   | 7022   | 700                 |
| 230   | 392.9 | .1   | 0    | .164  | 4.1             | -     | -              | .184  | 1.84  | 2.2   | -     | -     | -                  | -      | 201   | 7022   | 700                 |
| 235   | 392.9 | .1   | 0    | .158  | 3.9             | -     | -              | .182  | 1.82  | 2.2   | -     | -     | -                  | -      | 198   | 7021   | 725                 |
| TOTAL | ***** | **** | **** | ***** | *****           | ***** | *****          | ***** | ***** | ***** | ***** | ***** | *****              | *****  | 2631  | -296   | *****               |
| TOTAL | ***** | **** | **** | ***** | *****           | ***** | *****          | ***** | ***** | ***** | ***** | ***** | *****              | *****  | 6400  | -765   | *****               |















| TIME  | TOP   | LT SIDE | BACK | RT SIDE | BOTTOM | FIREBOX | SEC/CAT | AMBIENT | FURNACE | SAMPLE | SAMP IMP | C-GAS | GAS IMP | SO <sub>2</sub> IMP |
|-------|-------|---------|------|---------|--------|---------|---------|---------|---------|--------|----------|-------|---------|---------------------|
| 0     | 1400  | 322     | 296  | 298     | 237    | 720     | 668     | 78      | 1336    | 246    | 49       | 243   | 37      | 39                  |
| 5     | 05    | 292     | 295  | 294     | 240    | 626     | 536     | 79      | 1340    | 246    | 43       | 243   | 38      | 39                  |
| 10    | 10    | 283     | 293  | 283     | 239    | 554     | 413     | 77      | 1340    | 245    | 44       | 243   | 38      | 39                  |
| 15    | 15    | 260     | 285  | 267     | 237    | 499     | 380     | 78      | 1342    | 245    | 43       | 243   | 37      | 36                  |
| 20    | 20    | 242     | 270  | 251     | 231    | 515     | 373     | 77      | 1339    | 245    | 44       | 243   | 36      | 35                  |
| 25    | 25    | 233     | 266  | 239     | 225    | 527     | 396     | 78      | 1336    | 244    | 44       | 242   | 36      | 35                  |
| 30    | 30    | 354     | 254  | 229     | 218    | 478     | 1170    | 77      | 1329    | 243    | 45       | 241   | 37      | 35                  |
| 35    | 35    | 491     | 250  | 225     | 213    | 479     | 1046    | 76      | 1328    | 243    | 45       | 241   | 35      | 36                  |
| 40    | 40    | 619     | 244  | 226     | 207    | 507     | 1285    | 76      | 1329    | 244    | 47       | 234   | 35      | 37                  |
| 45    | 45    | 631     | 241  | 232     | 205    | 520     | 1365    | 77      | 1331    | 245    | 46       | 230   | 36      | 38                  |
| 50    | 50    | 638     | 238  | 243     | 202    | 570     | 1398    | 78      | 1333    | 247    | 47       | 235   | 37      | 36                  |
| 55    | 55    | 708     | 233  | 259     | 201    | 622     | 1455    | 78      | 1335    | 247    | 48       | 237   | 37      | 35                  |
| TOTAL | 5123  | 3438    | 3165 | 3046    | 2655   | 6617    | 10491   | 929     | *****   | *****  | *****    | ***** | *****   | *****               |
| 60    | 150   | 725     | 242  | 278     | 202    | 669     | 1467    | 78      | 1338    | 249    | 48       | 241   | 38      | 37                  |
| 65    | 05    | 737     | 249  | 298     | 205    | 720     | 1478    | 80      | 1342    | 249    | 49       | 243   | 36      | 36                  |
| 70    | 10    | 680     | 260  | 325     | 208    | 754     | 1155    | 80      | 1347    | 247    | 49       | 243   | 34      | 35                  |
| 75    | 15    | 644     | 264  | 332     | 209    | 746     | 1215    | 80      | 1348    | 247    | 49       | 245   | 34      | 35                  |
| 80    | 20    | 585     | 259  | 340     | 213    | 741     | 1265    | 80      | 1348    | 246    | 49       | 250   | 35      | 34                  |
| 85    | 25    | 541     | 287  | 343     | 217    | 765     | 1217    | 81      | 1348    | 246    | 49       | 258   | 35      | 34                  |
| 90    | 30    | 528     | 293  | 344     | 220    | 772     | 1185    | 80      | 1348    | 246    | 50       | 258   | 36      | 34                  |
| 95    | 35    | 503     | 302  | 345     | 222    | 775     | 1147    | 81      | 1346    | 245    | 50       | 252   | 38      | 35                  |
| 100   | 40    | 485     | 311  | 346     | 225    | 776     | 1101    | 81      | 1344    | 245    | 50       | 248   | 37      | 35                  |
| 105   | 45    | 473     | 318  | 347     | 228    | 771     | 1089    | 81      | 1343    | 244    | 50       | 247   | 36      | 37                  |
| 110   | 50    | 473     | 323  | 345     | 230    | 773     | 1136    | 81      | 1341    | 244    | 51       | 245   | 36      | 37                  |
| 115   | 55    | 454     | 327  | 344     | 232    | 774     | 1023    | 82      | 1340    | 243    | 51       | 244   | 35      | 34                  |
| TOTAL | 6828  | 4511    | 3435 | 3987    | 2611   | 9036    | 14478   | 9165    | *****   | *****  | *****    | ***** | *****   | *****               |
| TOTAL | 11951 | 7949    | 6600 | 7033    | 5266   | 15659   | 24919   | 1894    | *****   | *****  | *****    | ***** | *****   | *****               |















## ZERO / SPAN CHECK DATA SHEET #15-1

Date: 4-11-2000 Analyte.: CO<sub>2</sub> (15-1)

Source: F400 Run #: 3

Zero Cyl. #: TX 79373 Conc.: 0.00 % CO<sub>2</sub> Cyl. Press.: 960 PSI

Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 12.79 % CO<sub>2</sub> Cyl. Press.: 1750 PSI

Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: HORIBA Model: PIR-2000 SN: 407069

Range: 0 - 25.0 % CO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 25.0 % CO<sub>2</sub>

EPA Control Limits =  $\pm 2.5\%$  of 25.0 % CO<sub>2</sub> =  $\pm 0.625 % CO_2$

Method 28 A =  $\pm .2 %$  of 25.0 % CO<sub>2</sub> =  $\pm .05 % CO_2$

PRE RUN Audit: by: D. Wadsworth Time: 1218 Temp: 84 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |        | ± Conc. Difference | Δ %  |
|---------|-------------------|------|-------|-----------------|------|--------|--------------------|------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %      |                    |      |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | .000 | .048   | -048               | -192 |
| SPAN    | 51.2              | .512 | 12.79 | 50.9            | .509 | 12.736 | -054               | -216 |

POST RUN Audit: by: D. Wadsworth Time: 1820 Temp: 77 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |       |        | ± Conc. Difference | Δ %   |
|---------|-------------------|------|-------|-----------------|-------|--------|--------------------|-------|
|         | Meter             | DVM  | %     | Meter           | DVM   | %      |                    |       |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | -.002 | -.098  | -.098              | -.393 |
| SPAN    | 51.2              | .512 | 12.79 | 51.0            | .510  | 12.761 | -.029              | -.115 |

± Conc. Difference = Act % - Exp (Std) %

Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





## ZERO / SPAN CHECK DATA SHEET #15-2

Date: 4-11-2000 Analyte: O<sub>2</sub> (15-2)

Source: F400 Run #: 3

Zero Cyl. #: TX79373 Conc.: 0.00 % O<sub>2</sub> Cyl. Press.: 960 PSI

Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 12.69 % O<sub>2</sub> Cyl. Press.: 1750 PSI

Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: TELEDYNE Model: 320 A SN: 37400

Range: 0 - 25.0 % O<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 25.0 % O<sub>2</sub>

EPA Control Limits =  $\pm 2.5\%$  of 25.0 % O<sub>2</sub> =  $\pm 0.625 % O_2$

Method 28 A =  $\pm .2 %$  of 25.0 % O<sub>2</sub> =  $\pm .05 % O_2$

PRE RUN Audit: by: D. Wadsworth Time: 1215 Temp: 84 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |          | ± Conc. Difference | Δ %    |
|---------|-------------------|------|-------|-----------------|------|----------|--------------------|--------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %        |                    |        |
| ZERO    | 00.0              | .000 | 00.0  | 00.1            | .002 | .075     | .075 ✓             | .299 ✓ |
| SPAN    | 12.7              | .508 | 12.69 | 12.7            | .510 | 12.737 ✓ | .047 ✓             | .187 ✓ |

POST RUN Audit: by: A. Wadsworth Time: 1820 Temp: 77 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |          | ± Conc. Difference | Δ %     |
|---------|-------------------|------|-------|-----------------|------|----------|--------------------|---------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %        |                    |         |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | .001 | .050 ✓   | .050 ✓             | .200 ✓  |
| SPAN    | 12.7              | .508 | 12.69 | 12.7            | .508 | 12.687 ✓ | -.003 ✓            | -.012 ✓ |

± Conc. Difference = Act % - Exp (Std) %

Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





## ZERO / SPAN CHECK DATA SHEET #15-3

Date: 4-11-2000 Analyte: CO (15-3)

Source: F400 Run #: 3

Zero Cyl. #: TX79373 Conc.: 0.00 % CO Cyl. Press.: 960 PSI

Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 4.75 % CO Cyl. Press.: 1750 PSI

Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: HORIBA Model: PIR-2000 SN: 408005

Range: 0 - 10.0 % CO Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 10.0 % CO

EPA Control Limits =  $\pm 2.5\%$  of 10.0 % CO =  $\pm 0.25$  % CO

Method 28 A =  $\pm .2\%$  of 10.0 % CO =  $\pm .02$  % CO

PRE RUN Audit: by: D. Woodruff Time: 1215 Temp: 84 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |       | ± Conc. Difference | Δ %   |
|---------|-------------------|------|------|-----------------|------|-------|--------------------|-------|
|         | Meter             | DVM  | %    | Meter           | DVM  | %     |                    |       |
| ZERO    | 00.0              | .000 | 00.0 | 00.0            | .000 | .004  | .004               | .042  |
| SPAN    | 47.5              | .475 | 4.75 | 47.4            | .474 | 4.742 | -.008              | -.079 |

POST RUN Audit: by: D. Woodruff Time: 1820 Temp: 77 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |       | ± Conc. Difference | Δ %  |
|---------|-------------------|------|------|-----------------|------|-------|--------------------|------|
|         | Meter             | DVM  | %    | Meter           | DVM  | %     |                    |      |
| ZERO    | 00.0              | .000 | 00.0 | 00.1            | .001 | .014  | .014               | .142 |
| SPAN    | 47.5              | .475 | 4.75 | 47.5            | .475 | 4.752 | .002               | .021 |

± Conc. Difference = Act % - Exp (Std) %

Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$



## ZERO / SPAN CHECK DATA SHEET #15-4

Date: 4-11-2000 Analyte: SO<sub>2</sub> (15-4)

Source: F400 Run #: 3  
 Zero Cyl. #: TX79373 Conc.: 0.00 ppm SO<sub>2</sub> Cyl. Press.: 960 PSI

Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC67475 Conc.: 1260 ppm SO<sub>2</sub> Cyl. Press.: 1650 PSI

Certified by: AIR LIQUIDE Date: 9-22-1998

Analyzer: Make: HORIBA Model: PIR-2000 SN: 403019  
 Range: 0 - 2500 ppm SO<sub>2</sub> Analyzer Output: 0 - 1.0 v.  
 Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 2500 ppm SO<sub>2</sub>  
 EPA Control Limits =  $\pm 2.5\%$  of 2500 ppm SO<sub>2</sub> =  $\pm 62.5$  ppm SO<sub>2</sub>

PRE RUN Audit: by: A. W. [Signature] Time: 1215 Temp: 84 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |            | ± Conc. Difference | Δ %     |
|---------|-------------------|------|------|-----------------|------|------------|--------------------|---------|
|         | Meter             | DVM  | PPM  | Meter           | DVM  | %          |                    |         |
| ZERO    | 00.0              | .000 | 00.0 | 00.4            | .004 | 22.936 ✓   | 22.936 ✓           | .917 ✓  |
| SPAN    | 50.4              | .504 | 1260 | 498             | .498 | 1245.251 ✓ | -14.749 ✓          | -.590 ✓ |

POST RUN Audit: by: A. W. [Signature] Time: 1825 Temp: 76 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |            | ± Conc. Difference | Δ %     |
|---------|-------------------|------|------|-----------------|------|------------|--------------------|---------|
|         | Meter             | DVM  | PPM  | Meter           | DVM  | %          |                    |         |
| ZERO    | 00.0              | .000 | 00.0 | 00.5            | .005 | 25.410 ✓   | 25.410 ✓           | 1.016 ✓ |
| SPAN    | 50.4              | .504 | 1260 | 49.8            | .498 | 1245.251 ✓ | -14.749 ✓          | -.590 ✓ |

± Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





### QUALITY CHECKS DATA SHEET # 16

UNIT : F400 RUN : 3 DATE : 4-11-2000

**Thermocouple Check :**

|                         |                         |
|-------------------------|-------------------------|
| T/C # 1 <u>—</u> °F     | T/C # 13 <u>64.8</u> °F |
| T/C # 2 <u>—</u> °F     | T/C # 14 <u>62.7</u> °F |
| T/C # 3 <u>63.5</u> °F  | T/C # 15 <u>66.3</u> °F |
| T/C # 4 <u>59.0</u> °F  | T/C # 16 <u>62.1</u> °F |
| T/C # 5 <u>58.5</u> °F  | T/C # 17 <u>61.8</u> °F |
| T/C # 6 <u>58.2</u> °F  | T/C # 18 <u>68.0</u> °F |
| T/C # 7 <u>58.2</u> °F  | T/C # 19 <u>59.7</u> °F |
| T/C # 8 <u>57.9</u> °F  | T/C # 20 <u>55.9</u> °F |
| T/C # 9 <u>57.9</u> °F  | T/C # 21 <u>—</u> °F    |
| T/C # 10 <u>59.0</u> °F | T/C # 22 <u>—</u> °F    |
| T/C # 11 <u>56.2</u> °F | T/C # 23 <u>59.3</u> °F |
| T/C # 12 <u>72.3</u> °F | T/C # 24 <u>—</u> °F    |

**Thermocouple Readout :**

Pretest zero and span check and calibration

post test zero and span

% difference

ZERO : -1.1 °F Adj. to 0.0 °F

ZERO 4.3 °F Difference .215 %

SPAN 2004.2 °F Adj. to 2000.0 °F

SPAN 1999.7 °F Difference .015 %

**Thermocouple Readout Pretest Linearity Check**

|                         |                         |                         |
|-------------------------|-------------------------|-------------------------|
| 0 = <u>0.0</u> °F       | 200 = <u>203.7</u> °F   | 400 = <u>400.8</u> °F   |
| 600 = <u>602.9</u> °F   | 800 = <u>802.7</u> °F   | 1000 = <u>1001.5</u> °F |
| 1200 = <u>1198.9</u> °F | 1400 = <u>1399.7</u> °F | 1600 = <u>1600.0</u> °F |
| 1800 = <u>1800.1</u> °F | 2000 = <u>2000.0</u> °F |                         |

Sample Train Leak Check

Pre

Post

C-gas Train Leak Check

Pre

Post

SO<sub>2</sub> Train Leak Check

Pre

Post

Static Gauge Zero Check

Pre

Post

Scale Check Pre : 405.4 - 395.4  
 Post : 402.5 - 392.5

Stack Cleaned Prior to Test Run : YES \_\_\_\_\_ NO X







TABLE 1 ----- RAW DATA

CLIENT : Jotul

TEST No. : 4

MODEL: F400

DATE: 12-Apr-00

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| TIME<br>(MIN.) | METER<br>READING<br>(C F) | DELTA<br>H<br>(IN. H2O) | METER<br>TEMP.<br>(DEG. F) | PERCENT<br>CO<br>( % ) | PERCENT<br>CO2<br>( % ) | SO2<br>COCENTR.<br>PPM |
|----------------|---------------------------|-------------------------|----------------------------|------------------------|-------------------------|------------------------|
| 0              | 384.000                   | 0.150                   | 78                         | 0.57                   | 5.70                    | 325                    |
| 5              | 385.500                   | 0.130                   | 79                         | 0.93                   | 7.10                    | 350                    |
| 10             | 386.916                   | 0.130                   | 79                         | 0.53                   | 9.70                    | 350                    |
| 15             | 388.333                   | 0.150                   | 80                         | 0.26                   | 13.70                   | 325                    |
| 20             | 389.864                   | 0.150                   | 80                         | 0.09                   | 14.00                   | 325                    |
| 25             | 391.395                   | 0.140                   | 81                         | 0.08                   | 14.50                   | 325                    |
| 30             | 392.931                   | 0.120                   | 82                         | 0.10                   | 15.10                   | 350                    |
| 35             | 394.364                   | 0.120                   | 82                         | 0.08                   | 15.10                   | 350                    |
| 40             | 395.796                   | 0.120                   | 82                         | 0.09                   | 14.70                   | 350                    |
| 45             | 397.228                   | 0.120                   | 82                         | 0.08                   | 13.20                   | 350                    |
| 50             | 398.661                   | 0.120                   | 83                         | 0.13                   | 10.60                   | 350                    |
| 55             | 400.098                   | 0.120                   | 83                         | 0.22                   | 9.40                    | 350                    |
| 60             | 401.536                   | 0.110                   | 84                         | 0.48                   | 8.30                    | 375                    |
| 65             | 402.884                   | 0.110                   | 84                         | 0.52                   | 8.00                    | 375                    |
| 70             | 404.231                   | 0.110                   | 84                         | 0.52                   | 7.70                    | 375                    |
| 75             | 405.579                   | 0.110                   | 84                         | 0.58                   | 7.50                    | 375                    |
| 80             | 406.927                   | 0.110                   | 84                         | 0.56                   | 7.50                    | 375                    |
| 85             | 408.274                   | 0.110                   | 84                         | 0.50                   | 7.70                    | 375                    |
| 90             | 409.622                   | 0.090                   | 85                         | 0.63                   | 7.20                    | 400                    |
| 95             | 410.890                   | 0.080                   | 86                         | 0.81                   | 6.60                    | 425                    |
| 100            | 412.088                   | 0.090                   | 87                         | 0.82                   | 6.60                    | 400                    |
| 105            | 413.366                   | 0.100                   | 87                         | 0.86                   | 6.40                    | 375                    |
| 110            | 414.729                   | 0.090                   | 87                         | 0.87                   | 6.20                    | 400                    |
| 115            | 416.006                   | 0.100                   | 87                         | 1.06                   | 6.00                    | 375                    |
| 120            | 417.369                   | 0.100                   | 87                         | 1.12                   | 5.30                    | 375                    |
| 125            | 418.732                   | 0.100                   | 87                         | 1.21                   | 5.20                    | 375                    |
| 130            | 420.094                   | 0.090                   | 89                         | 1.25                   | 4.90                    | 400                    |
| 135            | 421.381                   | 0.090                   | 89                         | 1.40                   | 4.60                    | 400                    |
| 140            | 422.668                   | 0.090                   | 90                         | 1.25                   | 4.90                    | 400                    |
| 145            | 423.960                   | 0.090                   | 90                         | 1.23                   | 4.90                    | 400                    |
| 150            | 425.251                   | 0.090                   | 90                         | 1.06                   | 4.70                    | 400                    |
| 155            | 426.543                   | 0.090                   | 90                         | 1.08                   | 4.70                    | 400                    |
| 160            |                           |                         |                            |                        |                         |                        |





TABLE 2---RAW DATA

CLIENT : Jotul

TEST No. 4

MODEL: F400

DATE: 12-Apr-00

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|                                 |             |                               |        |     |
|---------------------------------|-------------|-------------------------------|--------|-----|
| METER CAL.<br>FACTOR (Y) -----  | 0.989       | Wt. WOOD<br>BURNED (LB) ----- | 12.7   | Lbs |
| BAROMETRIC<br>PRESS. (Pb) ----- | 30.09 in Hg | WET, FUEL<br>MOISTURE % ----- | 16.304 | %   |
| LEAK RATE<br>POST (Lp) -----    | 0.001 cfm   | Wt. PART.<br>COLLECTED -----  | 0.1993 | g   |
| WATER<br>VOL. (V1c) -----       | 77.1 ML     | METER<br>VOLUME Vm -----      | 42.543 | mcf |
| TEST<br>TIME (MIN) -----        | 155 min     | HC MOLE<br>FRACTION -----     | 0.0132 |     |



TABLE 3 -----FIELD DATA AVERAGES

CLIENT :Jotul

TEST No. 4

MODEL: F400

DATE: 12-Apr-00

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|           |                   |           |             |   |
|-----------|-------------------|-----------|-------------|---|
| AVG DELTA |                   | AVG PRCNT |             |   |
| H         | ----- 0.11 in H2O | CO        | ----- 0.66  | % |
| AVG METER |                   | AVG PRCNT |             |   |
| TEMP. Tm  | ----- 85 deg F    | CO2       | ----- 8.37  | % |
| AVG PPM   |                   | AVG BAL   |             |   |
| SO2       | ----- 371 PPM     | CO2/CO    | ----- 12.77 | % |





TABLE 4 ----- CALCULATIONS

CLIENT : Jotul

TEST No. 4

MODEL: F400

DATE: 12-Apr-00

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|                     |   |                   |  |
|---------------------|---|-------------------|--|
| STD SAMPLE          |   | STACK GAS         |  |
| VOL. Vm(std) -----  | 41.05 dscf                                | FLOW Qsd -----    | 649.992 dscf/Hr<br>&<br>10.83 dscf/min |
| VOL. WATER          |   | PARTICULATE       |  |
| VAPOR Vw(std) ----- | 3.629 scf                                 | CONCTR. Cs -----  | 0.0049 g/dscf                          |
| PRCNT               |   | PARTC. EMISS.     |  |
| MSTR Bws -----      | 8.12 %                                    | RATE E -----      | 3.16 g/Hr                              |
| BURN                |   | MOLES OF GAS      |  |
| RATE BR -----       | 1.87 Kg/Hr                                | PER Lb WOOD Nt -- | 0.41 Lb-mole/Lb                        |
| CO EMISSION         |   | PART. EMISS.      |  |
| RATE -----          | 142.64 g/Hr<br>&<br>76.44 g/Kgdry<br>fuel | RATE -----        | 1.69 g/Kgdry<br>fuel                   |



TABLE 5 ----- PROPORTIONAL RATE VARIATION

CLIENT : Jotul

TEST No. : 4

MODEL: F400

DATE: 12-Apr-00

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| TIME<br>INTEVAL<br>Ti | PPM<br>*<br>Vm | PROPRTN.<br>RATE VAR.<br>PR | PROPRTN<br>RATE VAR.<br>AVERAGE |
|-----------------------|----------------|-----------------------------|---------------------------------|
| 5                     | 475.7          | 97                          | 100                             |
| 10                    | 483.1          | 99                          |                                 |
| 15                    | 483.0          | 99                          |                                 |
| 20                    | 484.2          | 99                          |                                 |
| 25                    | 483.7          | 99                          |                                 |
| 30                    | 484.4          | 99                          |                                 |
| 35                    | 486.2          | 100                         |                                 |
| 40                    | 485.9          | 100                         |                                 |
| 45                    | 485.9          | 100                         |                                 |
| 50                    | 485.7          | 100                         |                                 |
| 55                    | 486.6          | 100                         |                                 |
| 60                    | 486.5          | 100                         |                                 |
| 65                    | 488.2          | 100                         |                                 |
| 70                    | 487.8          | 100                         |                                 |
| 75                    | 488.2          | 100                         |                                 |
| 80                    | 488.2          | 100                         |                                 |
| 85                    | 487.8          | 100                         |                                 |
| 90                    | 487.8          | 100                         |                                 |
| 95                    | 488.5          | 100                         |                                 |
| 100                   | 489.4          | 100                         |                                 |
| 105                   | 491.0          | 101                         |                                 |
| 110                   | 490.9          | 101                         |                                 |
| 115                   | 490.6          | 101                         |                                 |
| 120                   | 490.9          | 101                         |                                 |
| 125                   | 490.9          | 101                         |                                 |
| 130                   | 489.7          | 100                         |                                 |
| 135                   | 492.6          | 101                         |                                 |
| 140                   | 492.2          | 101                         |                                 |
| 145                   | 493.6          | 101                         |                                 |
| 150                   | 493.3          | 101                         |                                 |
| 155                   | 493.6          | 101                         |                                 |
| 160                   |                |                             |                                 |
| 165                   |                |                             |                                 |



COMPUTER INPUT DATA SHEET #1

Client: JOTUL U.S.A., INC.

Address: 400 RIVERSIDE STREET  
PORTLAND, ME 04104

3.16  
at 1.87 kg/h

Phone: 207-797-5912 Fax: 207-772-0523

Run No.: 4 Date of Test: 4-12-2000 Burn Rate: 1.866

Model No.: F400  min  min-1.25  fan

Stove Type:  Cat  Non Cat  Pellet  1.25-1.9  max  insert

Dry Gas Meter: Y Factor: .989 Post Leak Rate: .001 cfm Time: 153 min.  
(0.000) (Data Sheet #2) (0.000) (Data Sheet #2) (000) (Data Sheet #2)

Dry Gas Meter Volume: 42.543 cf  
(00.000) (Data Sheet #2)

Stack Flow: 9.336 dscfm  $\Delta$  H: .110 in. H<sub>2</sub>O  
(00.000) (Data Sheet #2) (0.000) (Data Sheet #2)

Barometric Pressure: 30.09 in. Hg  
(00.00) (Data Sheet #2)

H<sub>2</sub>O Captured: 77.1 g  
(00.0) (Data Sheet #3)

Total Particulate Catch: .1993 g  
(0.0000) (Data Sheet #6)

Flue Gas Moisture: 8.1337%  
(00.000) (Data Sheet #7)

Particulate Emission: .0750 gr/dscf  
(0.0000) (Data Sheet #7)

Ambient Moisture: 1.3%  
(0.00) (Data Sheet #8)

Stove Weight: — lbs  
(000) (Data Sheet #8)

Total Fuel Consumed During Burn: 12.7 lbs  
(00.0) (Data sheet #8)

Fuel Higher Heating Value (dry): — BTU/lb  
(0000) (Data Sheet #8)

Fuel % Moisture (dry): 19.480% (wet): 16.304%  
(00.00) (Data Sheet #10)

Stack Static Pressure: -.055 in. H<sub>2</sub>O  
(0.000) (Data Sheet #12)

Temperature (Average Room) Combustion Air: 81 °F  
(00) Data Sheet #14)

Stove Temperature Change: -37.2 °F  
(00.0) (Data Sheet #14)





METER BOX DATA SHEET PAGE # 2

Page: 1 of 2

UNIT: F400 RUN: 4

DATE: 4-12-2000

Meter Box: 5H Y Factor: .989

Leak checks: 15 " Hg @ .003 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm

<sup>20</sup> 15 " Hg @ .001 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm

Inject SO<sub>2</sub> @ 100 cc/min. Nozzle: Probe @ 3/8" od Initial Volume: 1.506

| ROTO PRESS: <u>.13</u> |      |               | SAMPLING RATIO: <u>36</u> : 1 |             |         |            | BP: <u>30.10</u> |                  |           |
|------------------------|------|---------------|-------------------------------|-------------|---------|------------|------------------|------------------|-----------|
| MIN                    | TIME | METER READING | SAMPLE MDCF                   | STACK DSCFM | DELTA H | METER TEMP | SO2 PPM          | ROTO TEMP        | PUMP VACC |
| 0                      | 1250 | 384.000       | —                             | 10.733      | .15     | 78         | 325              | 78               | 1.0       |
| 5                      | 55   | 385.500       | —                             | 9.948       | .13     | 79         | 350              | 79               | 1.0       |
| 10                     | 1300 | 386.916       | 386.916                       | 9.948       | .13     | 79         | 350              | 79               | 1.0       |
| 15                     | 05   | 388.333       | 388.333                       | 10.694      | .15     | 80         | 325              | 80               | 1.0       |
| 20                     | 10   | 389.864       | 389.864                       | 10.694      | .15     | 80         | 325              | 80               | 1.0       |
| 25                     | 15   | 391.395       | 391.395                       | 10.674      | .14     | 81         | 325              | 81               | 2.0       |
| 30                     | 20   | 392.931       | 392.931                       | 9.893       | .12     | 82         | 350              | 82               | 2.0       |
| 35                     | 25   | 394.364       | 394.364                       | 9.893       | .12     | 82         | 350              | 82               | 2.0       |
| 40                     | 30   | 395.796       | 395.796                       | 9.893       | .12     | 82         | 350              | 82               | 2.0       |
| 45                     | 35   | 397.228       | 397.228                       | 9.893       | .12     | 82         | 350              | 82               | 2.0       |
| 50                     | 40   | 398.661       | 398.661                       | 9.875       | .12     | 83         | 350              | 83               | 2.0       |
| 55                     | 45   | 400.098       | 400.098                       | 9.875       | .12     | 83         | 350              | 83               | 2.0       |
| ROTO PRESS: <u>.13</u> |      |               | TOTALS:                       |             | 122.013 | 1.57       | 971              | BP: <u>30.08</u> |           |
| 60                     | 1350 | 401.536       | 401.536                       | 9.194       | .11     | 84         | 375              | 84               | 2.0       |
| 65                     | 55   | 402.884       | 402.884                       | 9.194       | .11     | 84         | 375              | 84               | 2.0       |
| 70                     | 1400 | 404.231       | 404.231                       | 9.194       | .11     | 84         | 375              | 84               | 2.0       |
| 75                     | 05   | 405.579       | 405.579                       | 9.194       | .11     | 84         | 375              | 84               | 2.0       |
| 80                     | 10   | 406.927       | 406.927                       | 9.194       | .11     | 84         | 375              | 84               | 2.0       |
| 85                     | 15   | 408.274       | 408.274                       | 9.194       | .11     | 84         | 375              | 84               | 2.0       |
| 90                     | 20   | 409.622       | 409.622                       | 8.603       | .09     | 85         | 400              | 85               | 2.0       |
| 95                     | 25   | 410.890       | 410.890                       | 8.082       | .08     | 86         | 425              | 86               | 2.0       |
| 100                    | 30   | 412.088       | 412.088                       | 8.572       | .09     | 87         | 400              | 87               | 2.0       |
| 105                    | 35   | 413.366       | 413.366                       | 9.143       | .10     | 87         | 375              | 87               | 2.0       |
| 110                    | 40   | 414.729       | 414.729                       | 8.572       | .09     | 87         | 400              | 87               | 2.0       |
| 115                    | 45   | 416.006       | 416.006                       | 9.143       | .10     | 87         | 375              | 87               | 2.0       |
|                        |      |               | TOTALS:                       |             | 107.279 | 1.21       | 1023             | MAX VACC =       |           |
| TOTAL Cu Ft:           |      |               | TOTALS:                       |             | 229.292 | 2.78       | 1994             | AVG. BP:         |           |





METER BOX DATA SHEET PAGE # 2

Page: 2 of 2

UNIT: F400 RUN: 4 DATE: 4-12-2000

Meter Box: SH Y Factor: .989

Leak checks: 15 " Hg @ 1003 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm

15 " Hg @ .001 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm

Inject SO<sub>2</sub> @ 100 cc/min. Nozzle : Probe @ 3/8" od Initial Volume: 1500

| ROTO: PRESS: <u>13</u>     |      |               | SAMPLING RATIO: <u>36</u> : 1 |             |         |            | BP: <u>30.08</u>      |           |           |  |
|----------------------------|------|---------------|-------------------------------|-------------|---------|------------|-----------------------|-----------|-----------|--|
| MIN                        | TIME | METER READING | SAMPLE MDCF                   | STACK DSCFM | DELTA H | METER TEMP | SO2 PPM               | ROTO TEMP | PUMP VACC |  |
| 120                        | 1450 | 417.369       | 417.369                       | 9.143       | .10     | 87         | 375                   | 87        | 2.0       |  |
| 125                        | 55   | 418.732       | 418.732                       | 9.143       | .10     | 87         | 375                   | 87        | 2.0       |  |
| 130                        | 1500 | 420.094       | 420.094                       | 8.541       | .09     | 89         | 400                   | 89        | 2.0       |  |
| 135                        | 05   | 421.381       | 421.381                       | 8.541       | .09     | 89         | 400                   | 89        | 2.0       |  |
| 140                        | 10   | 422.668       | 422.668                       | 8.525       | .09     | 90         | 400                   | 90        | 2.0       |  |
| 145                        | 15   | 423.960       | 423.960                       | 8.525       | .09     | 90         | 400                   | 90        | 2.0       |  |
| 150                        | 20   | 425.251       | 425.251                       | 8.525       | .09     | 90         | 400                   | 90        | 2.0       |  |
| 155                        | 25   | 426.543       | 426.543                       | 8.525       | .09     | 90         | 400                   | 90        | 2.0       |  |
| 160                        |      |               |                               |             |         |            |                       |           |           |  |
| 165                        |      |               |                               | 69.468      | .740    | 712        |                       |           |           |  |
| 170                        |      |               |                               |             |         |            |                       |           |           |  |
| 175                        |      |               |                               |             |         |            |                       |           |           |  |
| ROTO PRESS:                |      |               | TOTALS:                       |             |         |            | BP.:                  |           |           |  |
| 180                        |      |               |                               |             |         |            |                       |           |           |  |
| 185                        |      |               |                               |             |         |            |                       |           |           |  |
| 190                        |      |               |                               |             |         |            |                       |           |           |  |
| 195                        |      |               |                               |             |         |            |                       |           |           |  |
| 200                        |      |               |                               |             |         |            |                       |           |           |  |
| 205                        |      |               |                               |             |         |            |                       |           |           |  |
| 210                        |      |               |                               |             |         |            |                       |           |           |  |
| 215                        |      |               |                               |             |         |            |                       |           |           |  |
| 220                        |      |               |                               |             |         |            |                       |           |           |  |
| 225                        |      |               |                               |             |         |            |                       |           |           |  |
| 230                        |      |               |                               |             |         |            |                       |           |           |  |
| 235                        |      |               |                               | 298.760     | 3.52    | 2706       | 332                   |           |           |  |
|                            |      |               | TOTALS:                       |             |         |            | MAX VACC = 2.0        |           |           |  |
| TOTAL Cu Fl. <u>42.543</u> |      |               | TOTALS: <u>9.336</u>          |             |         |            | AVG. BP: <u>30.09</u> |           |           |  |





# PARTICULATE CATCH / MOISTURE DATA SHEET # 3

UNIT: F400 RUN: 4 DATE: 4-12-00

| SCALE CHECK | LEVEL | ZEROED |
|-------------|-------|--------|
| INITIAL :   | ✓     | ✓      |
| FINAL :     | ✓     | ✓      |

| SCALE   | WEIGHT |
|---------|--------|
| 295.0 g | 295.0  |
| 590.0 g | 590.0  |
| 885.0 g | 885.0  |

| IMPINGER     | #1    | #2    | #3    | #4    |
|--------------|-------|-------|-------|-------|
| FINAL WT     | 650.9 | 606.3 | 514.7 | 889.9 |
| INITIAL WT   | 586.0 | 602.9 | 513.8 | 882.0 |
| NET WT GRAMS | 64.9  | 3.4   | .9    | 7.9   |

TOTAL CATCH: 77.1 GRAMS H<sub>2</sub>O

### FRONT HALF

|              |       |  |
|--------------|-------|--|
| FILTER #     | 21F   |  |
| FINAL WT g   | .7279 |  |
| INITIAL WT g | .6779 |  |
| NET WT g     | .0500 |  |

|               |         |
|---------------|---------|
| BEAKER #      | 66      |
| DESC.         | ACETONE |
| FINAL WT g    | 96.5429 |
| INITIAL WT g  | 96.5141 |
| NET WT g      | .0288   |
| VOL. DESC. ml | 100     |

### BACK HALF

|              |       |  |
|--------------|-------|--|
| FILTER #     | 21B   |  |
| FINAL WT g   | .4416 |  |
| INITIAL WT g | .4243 |  |
| NET WT g     | .0173 |  |

| BEAKER #     | 67       | 68        | 69               | 70               |       |
|--------------|----------|-----------|------------------|------------------|-------|
| DESC.        | ACETONE  | METHCHLOR | H <sub>2</sub> O | H <sub>2</sub> O |       |
| FINAL WT g   | 106.2949 | 94.1736   | 109.0130         | 107.5004         |       |
| INITIAL WT g | 106.2278 | 94.1628   | 108.9986         | 107.4851         |       |
| NET WT g     | .0671    | .0108     | .0144            | .0153            | .0297 |
| VOL. DESC ml | 125      | 75        | 150              | 150              | (300) |



## FILTER TARE WEIGHTS DATA SHEET #4-1

Into Dessicator : \_\_\_\_\_ Date : 4-10-2000 Time : 1725 By : AKU  
 Manufacturer S & S Grade : # 25 Glass Front Size : 11 cm Lot No. : ZB921  
 Back Size : 8.2 cm Lot No. : ZB911

| DATE: <u>4-11-2000</u> |              | BY: <u>AKU</u> |               | DATE: <u>4-12-2000</u> |                  | BY: <u>AKU</u> |  | DATE: _____ |  | BY: _____ |  |
|------------------------|--------------|----------------|---------------|------------------------|------------------|----------------|--|-------------|--|-----------|--|
| FILTER #               | FIRST WEIGHT | TIME           | SECOND WEIGHT | TIME                   | THIRD WEIGHT     | TIME           |  |             |  |           |  |
| 21B                    | .4240        | 1917           | .4243         | 1103                   | ✓ Total F400 R#4 |                |  |             |  |           |  |
| 22B                    | .4422        | 1918           | .4423         | 1104                   | ✓                |                |  |             |  |           |  |
| 23B                    | .4297        | 1919           | .4300         | 1105                   | ✓                |                |  |             |  |           |  |
| 24B                    | .4333        | 1920           | .4334         | 1106                   | ✓                |                |  |             |  |           |  |
| 25B                    | .4436        | 1921           | .4437         | 1107                   | ✓                |                |  |             |  |           |  |
| 26B                    | .4279        | 1922           | .4282         | 1108                   | ✓                |                |  |             |  |           |  |
| 27B                    | .4249        | 1923           | .4248         | 1109                   | ✓                |                |  |             |  |           |  |
| 28B                    | .4256        | 1924           | .4254         | 1110                   | ✓                |                |  |             |  |           |  |
| 29B                    | .4289        | 1925           | .4292         | 1111                   | ✓                |                |  |             |  |           |  |
| 30B                    | .4397        | 1926           | .4400         | 1112                   | ✓                |                |  |             |  |           |  |

|     |       |      |       |      |                  |  |  |  |  |  |  |
|-----|-------|------|-------|------|------------------|--|--|--|--|--|--|
| 21F | .6776 | 1927 | .6779 | 1113 | ✓ Total F400 R#4 |  |  |  |  |  |  |
| 22F | .6731 | 1928 | .6734 | 1114 | ✓                |  |  |  |  |  |  |
| 23F | .6675 | 1929 | .6679 | 1115 | ✓                |  |  |  |  |  |  |
| 24F | .6838 | 1930 | .6839 | 1116 | ✓                |  |  |  |  |  |  |
| 25F | .6708 | 1931 | .6712 | 1117 | ✓                |  |  |  |  |  |  |
| 26F | .6778 | 1932 | .6774 | 1118 | ✓                |  |  |  |  |  |  |
| 27F | .6783 | 1933 | .6782 | 1119 | ✓                |  |  |  |  |  |  |
| 28F | .6733 | 1934 | .6737 | 1120 | ✓                |  |  |  |  |  |  |
| 29F | .6711 | 1935 | .6713 | 1121 | ✓                |  |  |  |  |  |  |
| 30F | .6812 | 1936 | .6814 | 1122 | ✓                |  |  |  |  |  |  |

Checked by: C. Washington Date: 4-12-00 Time: 1130

### BALANCE ROOM ENVIRONMENTAL CONDITIONS

| DATE | TIME | BY  | WB | DB | % RH |
|------|------|-----|----|----|------|
| 4-11 | 1910 | AKU | }  | 78 | 48   |
| 4-12 | 1100 | AKU |    | 76 | 49   |
|      |      |     |    |    |      |





## BEAKER TARE WEIGHTS DATA SHEET #4-2

Into Dessicator: Date: 3-30-2000 Time: 1650 By: DKW

DATE: 4-02 BY: DKW DATE: 4-03 BY: DKW DATE: \_\_\_\_\_ BY: \_\_\_\_\_

| BEAKER # | FIRST WEIGHT | TIME | SECOND WEIGHT | TIME | THIRD WEIGHT         | TIME |
|----------|--------------|------|---------------|------|----------------------|------|
| 66       | 96.5137      | 2138 | 96.5141       | 0858 |                      |      |
| 67       | 106.2274     | 2139 | 106.2278      | 0859 |                      |      |
| 68       | 94.1625      | 2140 | 94.1628       | 0900 | } TOTAL F4(X)<br>R#4 |      |
| 69       | 108.9982     | 2140 | 108.9986      | 0902 |                      |      |
| 70       | 107.4848     | 2141 | 107.4851      | 0903 |                      |      |
|          |              |      |               |      |                      |      |
| 71       | 105.3708     | 2142 | 105.3711      | 0904 |                      |      |
| 72       | 103.8323     | 2143 | 103.8328      | 0905 |                      |      |
| 73       | 104.3593     | 2143 | 104.3597      | 0906 |                      |      |
| 74       | 107.5138     | 2144 | 107.5141      | 0907 |                      |      |
| 75       | 99.6741      | 2145 | 99.6746       | 0909 |                      |      |
|          |              |      |               |      |                      |      |
| 76       | 103.8082     | 2146 | 103.8086      | 0910 |                      |      |
| 77       | 107.3922     | 2146 | 107.3926      | 0911 |                      |      |
| 78       | 94.5009      | 2147 | 94.5014       | 0912 |                      |      |
| 79       | 97.6250      | 2148 | 97.6255       | 0912 |                      |      |
| 80       | 109.1320     | 2149 | 109.1322      | 0913 |                      |      |
|          |              |      |               |      |                      |      |
| 81       | 101.4684     | 2149 | 101.4687      | 0914 |                      |      |
| 82       | 97.4829      | 2150 | 97.4832       | 0915 |                      |      |
| 83       | 98.3327      | 2151 | 98.3331       | 0917 |                      |      |
| 84       | 105.5598     | 2152 | 105.5603      | 0918 |                      |      |
| 85       | 98.0005      | 2153 | 98.0006       | 0919 |                      |      |
|          |              |      |               |      |                      |      |
| 86       | 104.7508     | 2153 | 104.7512      | 0920 |                      |      |
| 87       | 105.9210     | 2154 | 105.9215      | 0921 |                      |      |
| 88       | 100.0093     | 2155 | 100.0097      | 0922 |                      |      |
| 89       | 120.6786     | 2156 | 120.6788      | 0923 |                      |      |
| 90       | 106.4104     | 2156 | 106.4107      | 0924 |                      |      |

**BALANCE ROOM ENVIRONMENTAL CONDITIONS**

| DATE   | TIME | BY  | WB | DB | % RH |                                 |
|--------|------|-----|----|----|------|---------------------------------|
| 4-00   | 2135 | DKW |    | 78 | 48   | Checked by: <u>C. Wardmeyer</u> |
| 4-3-00 | 0855 | DKW |    | 78 | 48   |                                 |
|        |      |     |    |    |      | Date: <u>4-3-2000</u>           |
|        |      |     |    |    |      | Time: <u>1015</u>               |





WOODSTOVE DATA SHEET # 4-3 : CONSTANT WEIGHTS

UNIT: F40U RUN: 4 DATE: 4-12-00

| Beaker # | Date | Time | By  | First Weight | Date | Time | By  | Second Weight | Date | Time | By  | Third Weight | Date | Time | By |
|----------|------|------|-----|--------------|------|------|-----|---------------|------|------|-----|--------------|------|------|----|
| 66       | 4-13 | 2015 | DKW | 96.5434      | 4-14 | 2137 | DKW | 96.5429       | 4-16 | 1628 | DKW |              |      |      |    |
| 67       | 4-13 | 2015 | DKW | 106.2954     | 4-14 | 2138 | DKW | 106.2949      | 4-16 | 1629 | DKW |              |      |      |    |
| 68       | 4-13 | 2015 | DKW | 94.1740      | 4-14 | 2139 | DKW | 94.1736       | 4-16 | 1630 | DKW |              |      |      |    |
| 69       | 4-13 | 2015 | DKW | 109.0133     | 4-14 | 2140 | DKW | 109.0130      | 4-16 | 1632 | DKW |              |      |      |    |
| 70       | 4-13 | 2015 | DKW | 107.5008     | 4-14 | 2142 | DKW | 107.5004      | 4-16 | 1633 | DKW |              |      |      |    |

| Filter # | Date | Time | By | First Weight | Date | Time | By  | Second Weight | Date | Time | By  | Third Weight | Date | Time | By |
|----------|------|------|----|--------------|------|------|-----|---------------|------|------|-----|--------------|------|------|----|
| 21F      | 4-12 | 1630 | CP | 7283         | 4-13 | 2150 | DKW | 7279          | 4-14 | 1651 | DKW |              |      |      |    |
| 21B      | 4-12 | 1630 | CP | 4420         | 4-13 | 2151 | DKW | 4416          | 4-14 | 1652 | DKW |              |      |      |    |

SCALE ROOM ENVIRONMENTAL CONDITIONS

| Weighing Session | Date | Time | By  | WB | DB | %RH |
|------------------|------|------|-----|----|----|-----|
| 1                | 4-13 | 2130 | DKW |    | 76 | 48  |
| 2                | 4-14 | 1640 | DKW |    | 75 | 49  |
| 3                | 4-14 | 2135 | DKW |    | 76 | 49  |
| 4                | 4-16 | 1625 | DKW |    | 78 | 44  |

| Weighing Session | Date | Time | By | WB | DB | %RH |
|------------------|------|------|----|----|----|-----|
| 5                |      |      |    |    |    |     |
| 6                |      |      |    |    |    |     |
| 7                |      |      |    |    |    |     |
| 8                |      |      |    |    |    |     |



### BLANK PROCESSING DATA SHEET # 5

UNIT: F400 RUN: 4 DATE: 4-12-2000

BLANKS DONE: 12-27-99

| BEAKER       | A              | B             | C            |
|--------------|----------------|---------------|--------------|
|              | 200 ml ACETONE | 75 ml DICHLOR | 200 ml WATER |
|              | FISHER OPTIMA  | FISHER OPTIMA |              |
|              | LOT #          | LOT #         |              |
| FINAL WEIGHT | 108.9011       | 106.3073      | 106.9666     |
| TARE WEIGHT  | 108.9003       | 106.3062      | 106.9651     |
| NET WEIGHT   | .0008          | .0011         | .0015        |

TARE BEAKERS INTO DESC: TIME: 11:30 DATE: 12-20-99

DATE: 1222 BY: NW DATE: 1223 BY: NW DATE: \_\_\_\_\_ BY: \_\_\_\_\_

| BEAKER | 1 ST WT  | TIME | 2 ND WT  | TIME | 3 RD WT | TIME |
|--------|----------|------|----------|------|---------|------|
| A      | 108.8999 | 1940 | 108.9003 | 1948 | ✓       |      |
| B      | 106.3058 | 1941 | 106.3062 | 1949 | ✓       |      |
| C      | 106.9647 | 1942 | 106.9651 | 1950 | ✓       |      |

FINAL BEAKERS INTO DESC: TIME: 1330 DATE: 12-24-99

DATE: 12-24 BY: NW DATE: 12-25 BY: NW DATE: 12-27 BY: NW

| BEAKER | 1 ST WT  | TIME | 2 ND WT  | TIME | 3 RD WT  | TIME   |
|--------|----------|------|----------|------|----------|--------|
| A      | 108.8999 | 2021 | 108.9016 | 1816 | 108.9011 | 1224 ✓ |
| B      | 106.3061 | 2022 | 106.3077 | 1817 | 106.3073 | 1225 ✓ |
| C      | 106.9643 | 2023 | 106.9670 | 1818 | 106.9666 | 1226 ✓ |

#### TARE QC

| DATE  | TIME | BY | WB | DB | %  |
|-------|------|----|----|----|----|
| 12-22 | 1935 | NW | }  | 77 | 47 |
| 12-23 | 1945 | NW |    | 75 | 48 |
|       |      |    |    |    |    |

#### FINAL QC

| DATE  | TIME | BY | WB | DB | %  |
|-------|------|----|----|----|----|
| 12-24 | 1945 | NW | }  | 76 | 45 |
| 12-25 | 1740 | NW |    | 75 | 38 |
| 12-27 | 1210 | NW |    | 76 | 46 |





# NET PARTICULATE CATCH CALCULATION DATA SHEET #6

UNIT: F400 RUN: 4 DATE: 4-12-2000

## BLANK CALCULATIONS

Acetone : .0008 g ÷ 200 ml = .000004 g/ml  
 Dichloromethane : .0011 g ÷ 75 ml = .000015 g/ml  
 Distilled Water : .0015 g ÷ 200 ml = .000008 g/ml

## FRONT HALF CATCH

FILTERS : .0500 g - 1 (.0000 g) = .0500 g  
Total Catch # of Filters Blank Value / Filter

BEAKERS : .0288 g - 100 (.00004 g) = .0284 g  
Total Catch ml Acetone Blank Value / ml Acetone

TOTAL FRONT HALF CATCH : .0784 g

## BACK HALF CATCH

FILTERS : .0173 g - 1 (.0000 g) = .0173 g  
Total Catch # of Filters Blank Value / Filter

BEAKERS :  
 Acetone : .0671 g - 125 (.00004 g) = .0666 g  
Total Catch ml Acetone Blank Value / ml Acetone

Extract : .0108 g - 75 (.000015 g) = .0097 g  
Total Catch ml Dichloromethane Blank Value / Dichloromethane

Water : .0297 g - 300 (.000008 g) = .0273 g  
Total Catch ml Water Blank Value / Water

TOTAL BACK HALF CATCH : .1209 g

TOTAL CATCH : .1993 g

% FRONT HALF : 39.34 %



**CALCULATIONS DATA SHEET # 7**

UNIT: F400 RUN: 4 DATE: 4-12-2000

$$1) Vm (std) = \frac{(42,543 \text{ Vm}) (17.64) (,989 \text{ mcf}) \left( 30.09 \text{ " Hg} + \frac{,110 \text{ " H}_2\text{O}}{13.6} \right)}{(,545 \text{ TmA})} = \frac{40.9888}{000.0000} \text{ dscf}$$

$$2) Vw (std) = (,04707) \left( \frac{77.1}{00.0000} \text{ ml H}_2\text{O} \right) = \frac{3.6291}{00.0000} \text{ scf}$$

$$3) Asw = \frac{(3.6291 \text{ scf})}{(3.6291 \text{ scf} + 40.9888 \text{ dscf})} = \frac{,0813}{,0000} \text{ Bws} \times 100 = \frac{8.1337}{00.0000} \% \text{ H}_2\text{O}$$

$$4) Cs = \frac{(,1993 \text{ g.})}{(40.9888 \text{ dscf})} (15.43) = \frac{,0750}{0.0000} \text{ gr / dscf}$$

$$5) \text{ Estimated g / hr} = \frac{(,1993 \text{ g.})}{(40.9888 \text{ dscf})} (9.336 \text{ dscfm}) (60) = \frac{2.7237}{00.0000} \text{ g / hr}$$

|                       |   |        |                             |
|-----------------------|---|--------|-----------------------------|
| Vm =                  | total cubic feet pulled on meter box during test              | (p. 2) | (000.000 Vm)                |
| mcf =                 | meter correction factor (Y factor) of meter box used for test | (p. 2) | (0.000 mcf)                 |
| " Hg =                | average barometric pressure during test                       | (p. 2) | (00.00 " Hg)                |
| " H <sub>2</sub> O =  | average delta H for test                                      | (p. 2) | (.000 " H <sub>2</sub> O)   |
| TmA =                 | average meter temperature for test in degrees Absolute        | (p. 2) | (000 TmA)                   |
| ml H <sub>2</sub> O = | total water caught during test                                | (p. 3) | (000.0 ml H <sub>2</sub> O) |
| g =                   | total particulate catch for test                              | (p. 6) | (00.0000 g.)                |
| dscfm =               | average stack flow during test                                | (p. 2) | (00.000 dscf)               |



### TEST DATA SHEET # 8

UNIT : F400 RUN : 4 DATE : 4-12-2000

Test Chamber Air Velocity Start : ∅ Stop : ∅ Avg. : ∅

Wet Bulb / Dry Bulb Pre : WB : 60 DB : 74 = 43 % RH 1.3 % H<sub>2</sub>O

Post : WB : 64 DB : 83 = 34 % RH 1.3 % H<sub>2</sub>O

Average : 38.5 %RH 1.3 % H<sub>2</sub>O

Empty Stove Weight (lbs) : \_\_\_\_\_ w/ stack & oil seal : Wet : - Dry : 390.0

Kindling Weight (lbs) : Paper : 1.2 Wood : 3.5

Preburn Fuel Weight : 10.1 + 8.6 + 12.4 + 2.4 + 2.1 Total : 35.6

Kindling & Preburn Fuel Weight (wood only) (lbs) : Total : 39.1

Coal Bed Wt Range (lbs) : 3.1 - 2.6 Scale : 393.1 - 392.6

Upper : .25 x fuel weight : Always round DOWN to nearest tenth

Lower : .20 x fuel weight : Always round UP to nearest tenth Actual Coal Bed Weight : 2.6

Maximum Coal Bed Removal (lbs) :  $((\frac{3.1}{\text{Upper}} + \frac{2.6}{\text{Lower}}) \div 2) \cdot .25 =$  .7

Test Fuel (.75" x 1.5" x 5" spacers) = 20 pcs

| Dimensions | Length in inches | No. Pcs | Weight in lbs | % of Load |
|------------|------------------|---------|---------------|-----------|
| 2" x 4"    | 13               | 3       | 5.2           | 40.9      |
| 4" x 4"    | 13               | 2       | 7.5           | 59.1      |

Test Fuel Weight : 12.7 lbs

Estimated Dry Burn Rate : <sup>2071</sup>  
 $\frac{12.7 - (12.7 \times .16304)}{2.2046} \times \frac{60}{155} =$  1.866 kg/hr

Estimated BTU's/hr :  $19,140 \times \frac{63}{100} \times \frac{\text{TIME } 1.866}{\text{DBR}} =$  22,500.60 BTU's/hr





WOOD STOVE OPERATING DATA PAGE #9

Unit : F400 Run : 4 Date : 4-12-2000

FIRE STARTED: 0835

WARM UP AND PREBURN:

PRIMARY AIR : Set wide open for all warm-up / preburn fuel charges. Then set to .5" at start of preburn.

SECONDARY AIR : N/A CAT BYPASS : N/A

CHARCOAL BED PREPARATION:

Raked and leveled prior to each warm-up / preburn charge. At 1 1/2 min. prior to loading last fuel, raked and leveled. In stove 35 sec.

TEST:

DOOR wide open during loading 0 min. 50 sec.

PRIMARY AIR : Opened full for first 5 min., then set to run setting of .5'

SECONDARY AIR : N/A CAT BYPASS : N/A

FAN:

ON / OFF during warm-up

ON / OFF during preburn

ON / OFF first \_\_\_\_\_ minutes of test

ON / OFF balance of test run

Fan speed set at N/A

WOOD DATA: KINDLING: A mix of the grades listed below:

|          | SIZE | MILL         | GRADE          | SPECIES      |
|----------|------|--------------|----------------|--------------|
| PREBURN: | 2x4  | Manke/Tacoma | Std. or better | s. grn D fir |
| TEST:    | 2x4  | Packwood     | # 2 or better  | s. grn D fir |
|          | 4x4  | Packwood     | # 2 or better  | s. grn D fir |

PELLET FUEL MANUFACTURER : N/A BRAND : N/A

All Grades WCLB rules:

WARM UP INFORMATION:

All pre-burn / warm up fuel pieces were either 12 or 16 inches.

1st warm up / pre-burn fuel charge (10.1 lbs.) added at 0850

2nd warm up / pre-burn fuel charge (8.6 lbs.) added at 0945

3rd warm up / pre-burn fuel charge (12.4 lbs.) added at 1025

4th warm up / pre-burn fuel charge (2.4 lbs.) added at 1145

5th warm up / pre-burn fuel charge (2.1 lbs.) added at 1215



### TEST DATA SHEET #10

Unit : F400 Run : 4 Date : 4-12-2000

Room Temperature : 70 °F Correction Factor : 0

Uncorrected Values are corrected for room temperature : Yes \_\_\_\_\_ No

Time Test Fuel moisture reading taken : 1045

Calibration Checks : X  Y  12.0 12.1 22.0 22.0

| pc # | Dimen.   | Use | TOP   |      | BOTTOM |      | SIDE   |      | Avg Corrected |
|------|----------|-----|-------|------|--------|------|--------|------|---------------|
|      |          |     | Uncor | Cor. | Uncor. | Cor. | Uncor. | Cor. |               |
| 1    | 2"x4"x8' | K   | 17.5  | 18.7 | 16.0   | 17.0 | 15.5   | 16.5 | 17.400        |
| 2    |          |     |       |      |        |      |        |      |               |
| 3    |          |     |       |      |        |      |        |      |               |
| 4    | 2"x4"x8' | P   | 18.0  | 19.2 | 18.5   | 19.8 | 18.5   | 19.8 | 19.600        |
| 5    | 2"x4"x8' | P   | 18.5  | 19.8 | 18.5   | 19.8 | 18.5   | 19.8 | 19.800        |
| 6    | 2"x4"x8' | P   | 21.0  | 22.5 | 22.0   | 23.7 | 21.5   | 23.1 | 23.100        |
| 7    | 2"x4"x8' | P   |       |      |        |      |        |      | 62.500        |
| 8    | 2"x4"x8' | P   |       |      |        |      |        |      |               |
| 9    |          |     |       |      |        |      |        |      |               |
| 10   |          |     |       |      |        |      |        |      |               |
| 11   | 2x4x13   | T   | 18.0  | 19.2 | 18.0   | 19.2 | 18.0   | 19.2 | 19.200        |
| 12   | "        | T   | 18.0  | 19.2 | 18.5   | 19.8 | 18.5   | 19.8 | 19.600        |
| 13   | "        | T   | 18.5  | 19.8 | 18.5   | 19.8 | 18.5   | 19.8 | 19.800        |
| 14   | 4x4x13   | T   | 18.5  | 19.8 | 18.5   | 19.8 | 18.0   | 19.2 | 19.600        |
| 15   | "        | T   | 18.0  | 19.2 | 18.0   | 19.2 | 18.0   | 19.2 | 19.200        |
| 16   |          |     |       |      |        |      |        |      | 97.400        |
| 17   |          |     |       |      |        |      |        |      |               |
| 18   |          |     |       |      |        |      |        |      |               |
| 19   |          |     |       |      |        |      |        |      |               |
| 20   | Spacers  | T   | 18.5  | 19.8 | 19.0   | 20.3 | 19.0   | 20.3 | 20.133        |

Key for Use : K = Kindling P = Pretest Fuel T = Test Fuel

|                  | KINDLING | PRETEST FUEL | TEST FUEL |
|------------------|----------|--------------|-----------|
| Dry Moisture % : | 17.400 % | 20.833 %     | 19.480 %  |
| Wet Moisture % : | 14.821 % | 17.241 %     | 16.304 %  |

To obtain Wet from Dry :  $\frac{100 \times \% \text{ Dry Reading}}{100 + \% \text{ Dry Reading}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges : 16 - 20 % wet: 19 - 25 % dry (17.5 - 22.5 on Meter Uncor. reading) at 70°





| TIME  | SCALE | FUEL | DROP | V.  | CO <sub>2</sub> | V. | O <sub>2</sub> | V.   | CO   | BAL   | WB | DB | % H <sub>2</sub> O | CAL WB | STACK  | STATIC | SO <sub>2</sub> PPM |
|-------|-------|------|------|-----|-----------------|----|----------------|------|------|-------|----|----|--------------------|--------|--------|--------|---------------------|
| 0     | 405.3 | 12.7 | 0    | 228 | 5.7             | -  | -              | .057 | .57  | 9.9   |    |    |                    | 439    | .054   | 325    |                     |
| 5     | 404.8 | 12.2 | .5   | 283 | 7.1             |    |                | .093 | .93  | 7.6   |    |    |                    | 476    | .055   | 350    |                     |
| 10    | 404.0 | 11.4 | .8   | 387 | 9.7             |    |                | .053 | .53  | 18.1  |    |    |                    | 558    | .062   | 350    |                     |
| 15    | 402.9 | 10.3 | 1.1  | 546 | 13.7            |    |                | .024 | .24  | 51.8  |    |    |                    | 646    | .065   | 325    |                     |
| 20    | 401.9 | 9.3  | 1.0  | 558 | 14.0            |    |                | .009 | .09  | 148.6 |    |    |                    | 685    | .067   | 325    |                     |
| 25    | 400.8 | 8.2  | 1.1  | 579 | 14.5            |    |                | .008 | .08  | 172.6 |    |    |                    | 697    | .068   | 325    |                     |
| 30    | 399.8 | 7.2  | 1.0  | 603 | 15.1            |    |                | .010 | .10  | 145.2 |    |    |                    | 706    | .069   | 350    |                     |
| 35    | 398.8 | 6.2  | 1.0  | 602 | 15.1            |    |                | .008 | .08  | 179.4 |    |    |                    | 713    | .070   | 350    |                     |
| 40    | 398.0 | 5.4  | .8   | 587 | 14.7            |    |                | .006 | .06  | 229.6 |    |    |                    | 702    | .070   | 350    |                     |
| 45    | 397.3 | 4.7  | .7   | 528 | 13.2            |    |                | .008 | .08  | 157.3 |    |    |                    | 670    | .068   | 350    |                     |
| 50    | 396.7 | 4.1  | .6   | 422 | 10.6            |    |                | .013 | .13  | 78.7  |    |    |                    | 615    | .066   | 350    |                     |
| 55    | 396.2 | 3.6  | .5   | 376 | 9.4             |    |                | .022 | .22  | 41.9  |    |    |                    | 586    | .064   | 350    |                     |
| TOTAL |       |      |      |     |                 |    |                |      |      |       |    |    |                    | 7493   | .778   |        |                     |
| 60    | 395.8 | 3.2  | .4   | 333 | 8.3             |    |                | .048 | .48  | 12.2  |    |    |                    | 547    | .061   | 375    |                     |
| 65    | 395.5 | 2.9  | .3   | 322 | 8.0             |    |                | .052 | .52  | 15.3  |    |    |                    | 524    | .061   | 375    |                     |
| 70    | 395.2 | 2.6  | .3   | 308 | 7.7             |    |                | .052 | .52  | 14.7  |    |    |                    | 494    | .059   | 375    |                     |
| 75    | 394.8 | 2.2  | .4   | 301 | 7.5             |    |                | .058 | .58  | 12.9  |    |    |                    | 484    | .059   | 375    |                     |
| 80    | 394.6 | 2.0  | .2   | 301 | 7.5             |    |                | .056 | .56  | 13.3  |    |    |                    | 474    | .056   | 375    |                     |
| 85    | 394.3 | 1.7  | .3   | 310 | 7.7             |    |                | .050 | .50  | 15.4  |    |    |                    | 471    | .054   | 375    |                     |
| 90    | 394.0 | 1.4  | .3   | 290 | 7.2             |    |                | .063 | .63  | 11.4  |    |    |                    | 451    | .052   | 400    |                     |
| 95    | 393.8 | 1.2  | .2   | 266 | 6.6             |    |                | .081 | .81  | 8.1   |    |    |                    | 434    | .050   | 425    |                     |
| 100   | 393.7 | 1.1  | .1   | 266 | 6.6             |    |                | .082 | .82  | 8.1   |    |    |                    | 422    | .050   | 400    |                     |
| 105   | 393.5 | .9   | .2   | 257 | 6.4             |    |                | .086 | .86  | 7.4   |    |    |                    | 412    | .048   | 375    |                     |
| 110   | 393.4 | .8   | .1   | 250 | 6.2             |    |                | .087 | .87  | 7.1   |    |    |                    | 404    | .048   | 400    |                     |
| 115   | 393.3 | .7   | .1   | 239 | 6.0             |    |                | .106 | 1.06 | 5.6   |    |    |                    | 392    | .046   | 375    |                     |
| TOTAL |       |      |      |     |                 |    |                |      |      |       |    |    |                    | 5514   | .644   |        |                     |
| TOTAL |       |      |      |     |                 |    |                |      |      |       |    |    |                    | 13007  | -1.422 |        |                     |

















TEMPERATURE DATA SHEET # 14

UNIT: F400

RUN: 4

DATE: 4-12-2000

PAGE 1

of 2

| TIME           | TOP            | LT SIDE        | BACK           | RT SIDE        | BOTTOM         | FIREBOX        | SEC/CAT         | AMBIENT       | FURNACE         | SAMPLE         | SAMP IMP      | C-GAS          | GAS IMP       | SO <sub>2</sub> IMP |
|----------------|----------------|----------------|----------------|----------------|----------------|----------------|-----------------|---------------|-----------------|----------------|---------------|----------------|---------------|---------------------|
| <del>0</del>   | <del>476</del> | <del>378</del> | <del>357</del> | <del>381</del> | <del>257</del> | <del>734</del> | <del>957</del>  | <del>79</del> | <del>1328</del> | <del>249</del> | <del>65</del> | <del>244</del> | <del>38</del> | <del>35</del>       |
| <del>5</del>   | <del>456</del> | <del>371</del> | <del>351</del> | <del>369</del> | <del>258</del> | <del>820</del> | <del>1099</del> | <del>78</del> | <del>1340</del> | <del>250</del> | <del>45</del> | <del>244</del> | <del>37</del> | <del>35</del>       |
| <del>10</del>  | <del>545</del> | <del>350</del> | <del>342</del> | <del>341</del> | <del>256</del> | <del>613</del> | <del>1017</del> | <del>77</del> | <del>1334</del> | <del>251</del> | <del>46</del> | <del>237</del> | <del>36</del> | <del>36</del>       |
| <del>15</del>  | <del>631</del> | <del>337</del> | <del>335</del> | <del>325</del> | <del>252</del> | <del>611</del> | <del>1357</del> | <del>77</del> | <del>1333</del> | <del>250</del> | <del>46</del> | <del>230</del> | <del>37</del> | <del>38</del>       |
| <del>20</del>  | <del>701</del> | <del>333</del> | <del>326</del> | <del>316</del> | <del>246</del> | <del>628</del> | <del>1268</del> | <del>78</del> | <del>1333</del> | <del>250</del> | <del>46</del> | <del>238</del> | <del>38</del> | <del>35</del>       |
| <del>25</del>  | <del>737</del> | <del>341</del> | <del>319</del> | <del>314</del> | <del>241</del> | <del>656</del> | <del>1429</del> | <del>78</del> | <del>1336</del> | <del>251</del> | <del>46</del> | <del>242</del> | <del>37</del> | <del>35</del>       |
| <del>30</del>  | <del>753</del> | <del>361</del> | <del>314</del> | <del>321</del> | <del>237</del> | <del>699</del> | <del>1509</del> | <del>79</del> | <del>1340</del> | <del>251</del> | <del>46</del> | <del>244</del> | <del>37</del> | <del>35</del>       |
| <del>35</del>  | <del>768</del> | <del>383</del> | <del>311</del> | <del>339</del> | <del>232</del> | <del>769</del> | <del>1517</del> | <del>79</del> | <del>1342</del> | <del>249</del> | <del>46</del> | <del>248</del> | <del>35</del> | <del>36</del>       |
| <del>40</del>  | <del>768</del> | <del>399</del> | <del>310</del> | <del>358</del> | <del>230</del> | <del>807</del> | <del>1605</del> | <del>80</del> | <del>1341</del> | <del>250</del> | <del>47</del> | <del>250</del> | <del>35</del> | <del>36</del>       |
| <del>45</del>  | <del>743</del> | <del>411</del> | <del>311</del> | <del>373</del> | <del>229</del> | <del>820</del> | <del>1591</del> | <del>81</del> | <del>1340</del> | <del>249</del> | <del>47</del> | <del>249</del> | <del>35</del> | <del>36</del>       |
| <del>50</del>  | <del>688</del> | <del>426</del> | <del>315</del> | <del>384</del> | <del>228</del> | <del>841</del> | <del>1310</del> | <del>81</del> | <del>1341</del> | <del>249</del> | <del>48</del> | <del>248</del> | <del>36</del> | <del>36</del>       |
| <del>55</del>  | <del>619</del> | <del>431</del> | <del>318</del> | <del>390</del> | <del>228</del> | <del>864</del> | <del>1221</del> | <del>82</del> | <del>1340</del> | <del>248</del> | <del>48</del> | <del>248</del> | <del>36</del> | <del>36</del>       |
| TOTAL          | 7865           | 4521           | 3909           | 4213           | 2894           | 8862           | 15980           | 909           | *****           | *****          | *****         | *****          | *****         | *****               |
| <del>60</del>  | <del>579</del> | <del>432</del> | <del>326</del> | <del>395</del> | <del>228</del> | <del>894</del> | <del>1202</del> | <del>82</del> | <del>1338</del> | <del>247</del> | <del>48</del> | <del>246</del> | <del>36</del> | <del>36</del>       |
| <del>65</del>  | <del>569</del> | <del>428</del> | <del>333</del> | <del>397</del> | <del>230</del> | <del>903</del> | <del>1175</del> | <del>81</del> | <del>1336</del> | <del>246</del> | <del>48</del> | <del>245</del> | <del>36</del> | <del>35</del>       |
| <del>70</del>  | <del>539</del> | <del>420</del> | <del>343</del> | <del>398</del> | <del>231</del> | <del>899</del> | <del>1190</del> | <del>81</del> | <del>1335</del> | <del>245</del> | <del>49</del> | <del>247</del> | <del>37</del> | <del>36</del>       |
| <del>75</del>  | <del>513</del> | <del>415</del> | <del>354</del> | <del>395</del> | <del>233</del> | <del>895</del> | <del>1154</del> | <del>81</del> | <del>1334</del> | <del>244</del> | <del>49</del> | <del>247</del> | <del>36</del> | <del>35</del>       |
| <del>80</del>  | <del>499</del> | <del>411</del> | <del>362</del> | <del>393</del> | <del>233</del> | <del>891</del> | <del>1116</del> | <del>81</del> | <del>1333</del> | <del>244</del> | <del>49</del> | <del>244</del> | <del>35</del> | <del>35</del>       |
| <del>85</del>  | <del>497</del> | <del>403</del> | <del>372</del> | <del>388</del> | <del>237</del> | <del>888</del> | <del>1116</del> | <del>82</del> | <del>1332</del> | <del>244</del> | <del>48</del> | <del>244</del> | <del>35</del> | <del>37</del>       |
| <del>90</del>  | <del>482</del> | <del>398</del> | <del>379</del> | <del>386</del> | <del>239</del> | <del>894</del> | <del>1135</del> | <del>82</del> | <del>1332</del> | <del>244</del> | <del>49</del> | <del>246</del> | <del>37</del> | <del>36</del>       |
| <del>95</del>  | <del>465</del> | <del>395</del> | <del>385</del> | <del>383</del> | <del>241</del> | <del>921</del> | <del>980</del>  | <del>82</del> | <del>1332</del> | <del>245</del> | <del>49</del> | <del>246</del> | <del>37</del> | <del>36</del>       |
| <del>100</del> | <del>444</del> | <del>392</del> | <del>390</del> | <del>381</del> | <del>243</del> | <del>903</del> | <del>987</del>  | <del>82</del> | <del>1332</del> | <del>245</del> | <del>49</del> | <del>251</del> | <del>37</del> | <del>36</del>       |
| <del>105</del> | <del>432</del> | <del>391</del> | <del>375</del> | <del>379</del> | <del>245</del> | <del>828</del> | <del>965</del>  | <del>82</del> | <del>1332</del> | <del>246</del> | <del>49</del> | <del>250</del> | <del>35</del> | <del>34</del>       |
| <del>110</del> | <del>426</del> | <del>389</del> | <del>378</del> | <del>376</del> | <del>247</del> | <del>804</del> | <del>958</del>  | <del>81</del> | <del>1333</del> | <del>246</del> | <del>50</del> | <del>248</del> | <del>36</del> | <del>34</del>       |
| <del>115</del> | <del>413</del> | <del>384</del> | <del>378</del> | <del>369</del> | <del>250</del> | <del>773</del> | <del>902</del>  | <del>81</del> | <del>1333</del> | <del>247</del> | <del>50</del> | <del>246</del> | <del>34</del> | <del>36</del>       |
| TOTAL          | 5878           | 4858           | 4435           | 4646           | 2857           | 10493          | 12880           | 978           | *****           | *****          | *****         | *****          | *****         | *****               |
| TOTAL          | 13743          | 9379           | 8244           | 8853           | 5751           | 19255          | 28860           | 1927          | *****           | *****          | *****         | *****          | *****         | *****               |











## ZERO / SPAN CHECK DATA SHEET #15-1

Date: 4-12-2000 Analyte: CO<sub>2</sub> (15-1)

Source: F400 Run #: 4

Zero Cyl. #: TX 79373 Conc.: 0.00 % CO<sub>2</sub> Cyl. Press.: 960 PSI

Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 12.79 % CO<sub>2</sub> Cyl. Press.: 1750 PSI

Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: HORIBA Model: PIR-2000 SN: 407069

Range: 0 - 25.0 % CO<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 25.0 % CO<sub>2</sub>

EPA Control Limits =  $\pm 2.5\%$  of 25.0 % CO<sub>2</sub> =  $\pm 0.625 % CO_2$

Method 28 A =  $\pm .2 %$  of 25.0 % CO<sub>2</sub> =  $\pm .05 % CO_2$

PRE RUN Audit: by: D. Washington Time: 1140 Temp: 76 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |        | ± Conc. Difference | Δ %   |
|---------|-------------------|------|-------|-----------------|------|--------|--------------------|-------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %      |                    |       |
| ZERO    | 00.0              | .000 | 00.0  | 00.1            | .001 | 7.023  | 7.023              | -0.91 |
| SPAN    | 51.2              | .512 | 12.79 | 51.3            | .513 | 12.837 | .047               | .186  |

POST RUN Audit: by: D. Washington Time: 1540 Temp: 75 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |        | ± Conc. Difference | Δ %  |
|---------|-------------------|------|-------|-----------------|------|--------|--------------------|------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %      |                    |      |
| ZERO    | 00.0              | .000 | 00.0  | 00.2            | .002 | .002   | .002               | .009 |
| SPAN    | 51.2              | .512 | 12.79 | 51.3            | .513 | 12.837 | .047               | .186 |

± Conc. Difference = Act % - Exp (Std) %

Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$



## ZERO / SPAN CHECK DATA SHEET #15-2

Date: 4-12-2000 Analyte: O<sub>2</sub> (15-2)

Source: F400 Run #: 4

Zero Cyl. #: TX79373 Conc.: 0.00 % O<sub>2</sub> Cyl. Press.: 960 PSI

Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 12.69 % O<sub>2</sub> Cyl. Press.: 1750 PSI

Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: TELEDYNE Model: 320 A SN: 37400

Range: 0 - 25.0 % O<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 25.0 % O<sub>2</sub>

EPA Control Limits =  $\pm 2.5\%$  of 25.0 % O<sub>2</sub> =  $\pm 0.625 % O_2$

Method 28 A =  $\pm .2 %$  of 25.0 % O<sub>2</sub> =  $\pm .05 % O_2$

PRE RUN Audit: by: A. U. Wadsworth Time: 1140 Temp: 76 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |        | ± Conc. Difference | Δ %   |
|---------|-------------------|------|-------|-----------------|------|--------|--------------------|-------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %      |                    |       |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | .001 | 0.00   | 0.00               | .000  |
| SPAN    | 12.7              | .508 | 12.69 | 12.6            | .506 | 12.637 | -.053              | -.212 |

POST RUN Audit: by: A. U. Wadsworth Time: 1540 Temp: 75 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |        | ± Conc. Difference | Δ %   |
|---------|-------------------|------|-------|-----------------|------|--------|--------------------|-------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %      |                    |       |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | .000 | .025   | .025               | .100  |
| SPAN    | 12.7              | .508 | 12.69 | 12.7            | .507 | 12.662 | -.028              | -.112 |

± Conc. Difference = Act % - Exp (Std) %

Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





## ZERO / SPAN CHECK DATA SHEET #15-3

Date: 4-12-2000 Analyte: CO (15-3)

Source: F400 Run #: 4

Zero Cyl. #: TX79373 Conc.: 0.00 % CO Cyl. Press.: 960 PSI

Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 4.75 % CO Cyl. Press.: 1750 PSI

Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: HORIBA Model: PIR-2000 SN: 408005

Range: 0 - 10.0 % CO Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 10.0 % CO

EPA Control Limits =  $\pm 2.5\%$  of 10.0 % CO =  $\pm 0.25 % CO$

Method 28 A =  $\pm .2 %$  of 10.0 % CO =  $\pm .02 % CO$

PRE RUN Audit: by: [Signature] Time: 1140 Temp: 76 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |       | ± Conc. Difference | Δ %     |
|---------|-------------------|------|------|-----------------|------|-------|--------------------|---------|
|         | Meter             | DVM  | %    | Meter           | DVM  | %     |                    |         |
| ZERO    | 00.0              | .000 | 00.0 | 00.0            | .000 | .004  | .004 ✓             | .042 ✓  |
| SPAN    | 47.5              | .475 | 4.75 | 47.2            | .472 | 4.722 | -.028 ✓            | -.219 ✓ |

POST RUN Audit: by: [Signature] Time: 1540 Temp: 75 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |       | ± Conc. Difference | Δ %     |
|---------|-------------------|------|------|-----------------|------|-------|--------------------|---------|
|         | Meter             | DVM  | %    | Meter           | DVM  | %     |                    |         |
| ZERO    | 00.0              | .000 | 00.0 | 00.0            | .000 | .004  | .004 ✓             | .042 ✓  |
| SPAN    | 47.5              | .475 | 4.75 | 47.3            | .473 | 4.732 | -.018 ✓            | -.179 ✓ |

± Conc. Difference = Act % - Exp (Std) %

Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





## ZERO / SPAN CHECK DATA SHEET #15-4

Date: 4-12-2000 Analyte: SO<sub>2</sub> (15-4)

Source: F400 Run #: 4

Zero Cyl. #: TX79373 Conc.: 0.00 ppm SO<sub>2</sub> Cyl. Press.: 960 PSI  
 Certified by: AIR LIQUINE Date: 9-22-1998

Span Cyl. #: CC67475 Conc.: 1260 ppm SO<sub>2</sub> Cyl. Press.: 650 PSI  
 Certified by: AIR LIQUINE Date: 9-22-1998

Analyzer: Make: HORIBA Model: PIR-2000 SN: 403019  
 Range: 0 - 2500 ppm SO<sub>2</sub> Analyzer Output: 0 - 1.0 v.  
 Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 2500 ppm SO<sub>2</sub>  
 EPA Control Limits = ± 2.5% of 2500 ppm SO<sub>2</sub> = ± 62.5 ppm SO<sub>2</sub>

PRE RUN Audit: by: D. Wadsworth Time: 1140 Temp: 76 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |            | ± Conc. Difference | Δ %     |
|---------|-------------------|------|------|-----------------|------|------------|--------------------|---------|
|         | Meter             | DVM  | PPM  | Meter           | DVM  | %          |                    |         |
| ZERO    | 00.0              | .000 | 00.0 | 00.3            | .003 | 20.462 ✓   | 20.462 ✓           | .818 ✓  |
| SPAN    | 50.4              | .504 | 1260 | 50.0            | .500 | 1250.200 ✓ | -9.800 ✓           | -3.92 ✓ |

POST RUN Audit: by: D. Wadsworth Time: 1535 Temp: 77 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |            | ± Conc. Difference | Δ %     |
|---------|-------------------|------|------|-----------------|------|------------|--------------------|---------|
|         | Meter             | DVM  | PPM  | Meter           | DVM  | %          |                    |         |
| ZERO    | 00.0              | .000 | 00.0 | 00.3            | .003 | 20.462 ✓   | 20.462 ✓           | .818 ✓  |
| SPAN    | 50.4              | .504 | 1260 | 50.1            | .501 | 1252.674 ✓ | -7.326 ✓           | -2.93 ✓ |

± Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$



## QUALITY CHECKS DATA SHEET # 16

UNIT : F400 RUN : 4 DATE : 4-12-2000

**Thermocouple Check :**

|                          |                           |
|--------------------------|---------------------------|
| T/C # 1 <u>      </u> °F | T/C # 13 <u>68.5</u> °F   |
| T/C # 2 <u>      </u> °F | T/C # 14 <u>67.3</u> °F   |
| T/C # 3 <u>68.1</u> °F   | T/C # 15 <u>69.4</u> °F   |
| T/C # 4 <u>64.2</u> °F   | T/C # 16 <u>60.4</u> °F   |
| T/C # 5 <u>63.7</u> °F   | T/C # 17 <u>60.2</u> °F   |
| T/C # 6 <u>63.5</u> °F   | T/C # 18 <u>70.5</u> °F   |
| T/C # 7 <u>63.6</u> °F   | T/C # 19 <u>64.6</u> °F   |
| T/C # 8 <u>63.3</u> °F   | T/C # 20 <u>61.6</u> °F   |
| T/C # 9 <u>64.3</u> °F   | T/C # 21 <u>      </u> °F |
| T/C # 10 <u>64.5</u> °F  | T/C # 22 <u>      </u> °F |
| T/C # 11 <u>61.2</u> °F  | T/C # 23 <u>65.2</u> °F   |
| T/C # 12 <u>72.0</u> °F  | T/C # 24 <u>      </u> °F |

**Thermocouple Readout :**

Pretest zero and span check and calibration

post test zero and span

% difference

ZERO : .9 °F Adj. to 0.0 °F

ZERO .5 °F Difference .025 %

SPAN : 1998.4 °F Adj. to 2000.0 °F

SPAN 2003.6 °F Difference .180 %

**Thermocouple Readout Pretest Linearity Check**

|                         |                         |                         |
|-------------------------|-------------------------|-------------------------|
| 0 = <u>0.0</u> °F       | 200 = <u>201.6</u> °F   | 400 = <u>399.0</u> °F   |
| 600 = <u>601.2</u> °F   | 800 = <u>801.3</u> °F   | 1000 = <u>1000.4</u> °F |
| 1200 = <u>1198.1</u> °F | 1400 = <u>1399.0</u> °F | 1600 = <u>1599.6</u> °F |
| 1800 = <u>1799.9</u> °F | 2000 = <u>2000.0</u> °F |                         |

**Sample Train Leak Check**

Pre ✓

Post ✓

**C-gas Train Leak Check**

Pre X

Post ✓

**SO<sub>2</sub> Train Leak Check**

Pre X

Post ✓

**Static Gauge Zero Check**

Pre X

Post ✓

Scale Check Pre : 403.6 - 393.6

Post : 402.4 - 392.4

Stack Cleaned Prior to Test Run : YES \_\_\_\_\_ NO X





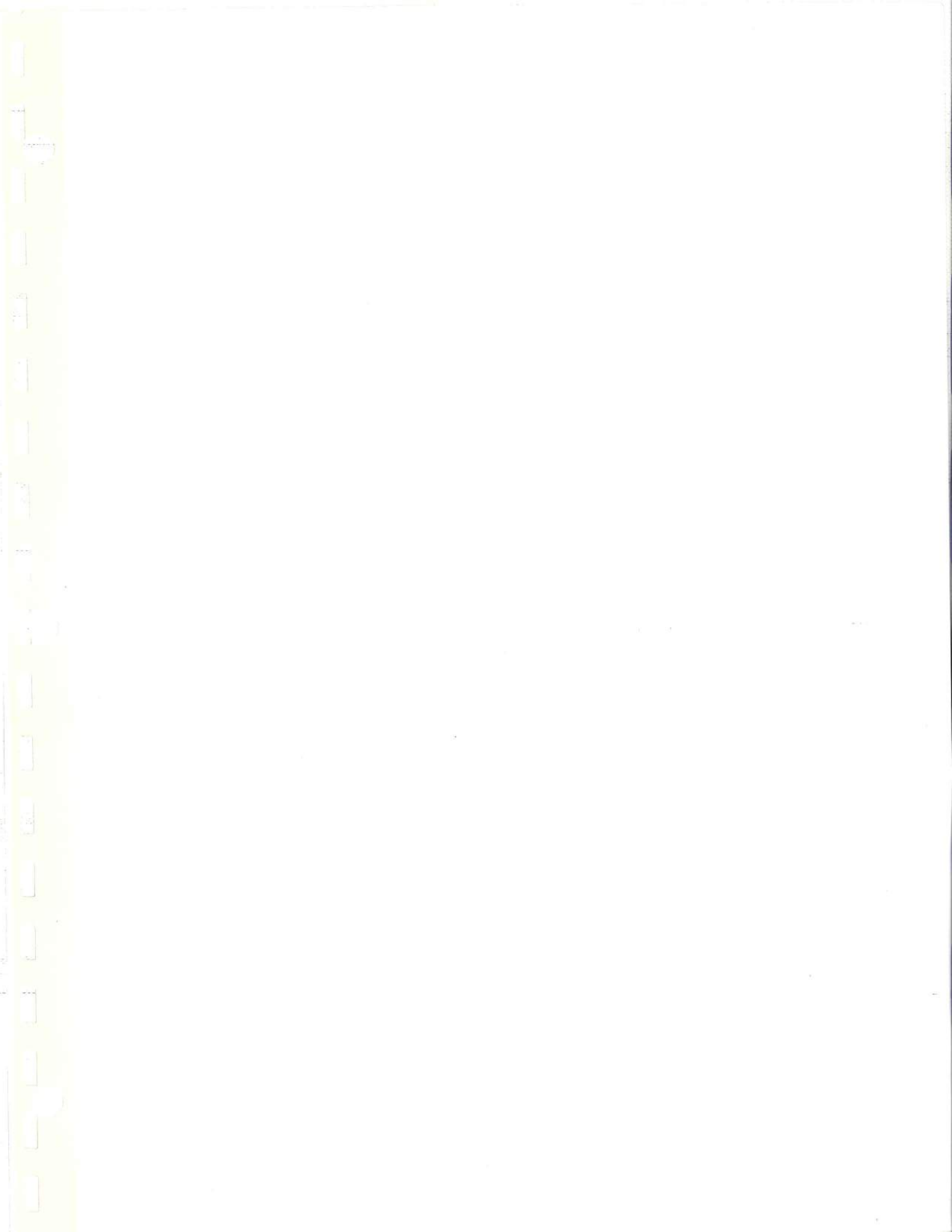




TABLE 1 ----- RAW DATA

CLIENT : Jotul

TEST No. : 2

MODEL: F400

DATE: 10-Apr-00

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| TIME<br>(MIN.) | METER<br>READING<br>(C F) | DELTA<br>H<br>(IN. H2O) | METER<br>TEMP.<br>(DEG. F) | PERCENT<br>CO<br>( % ) | PERCENT<br>CO2<br>( % ) | SO2<br>COCENTR.<br>PPM |
|----------------|---------------------------|-------------------------|----------------------------|------------------------|-------------------------|------------------------|
| 0              | 253.500                   | 0.150                   | 80                         | 0.87                   | 6.30                    | 325                    |
| 5              | 255.500                   | 0.170                   | 80                         | 0.86                   | 11.00                   | 300                    |
| 10             | 257.694                   | 0.170                   | 81                         | 0.30                   | 12.90                   | 300                    |
| 15             | 259.897                   | 0.170                   | 83                         | 0.13                   | 15.30                   | 300                    |
| 20             | 262.115                   | 0.140                   | 84                         | 0.14                   | 16.20                   | 325                    |
| 25             | 264.171                   | 0.140                   | 85                         | 0.12                   | 16.00                   | 325                    |
| 30             | 266.234                   | 0.140                   | 85                         | 0.13                   | 15.40                   | 325                    |
| 35             | 268.298                   | 0.140                   | 87                         | 0.17                   | 15.90                   | 325                    |
| 40             | 270.376                   | 0.140                   | 88                         | 0.06                   | 14.20                   | 325                    |
| 45             | 272.462                   | 0.140                   | 88                         | 0.04                   | 12.00                   | 325                    |
| 50             | 274.549                   | 0.140                   | 89                         | 0.05                   | 10.00                   | 325                    |
| 55             | 276.642                   | 0.140                   | 89                         | 0.34                   | 8.30                    | 325                    |
| 60             | 278.736                   | 0.120                   | 89                         | 0.61                   | 7.80                    | 350                    |
| 65             | 280.681                   | 0.120                   | 89                         | 0.78                   | 7.50                    | 350                    |
| 70             | 282.625                   | 0.120                   | 89                         | 0.89                   | 7.30                    | 350                    |
| 75             | 284.569                   | 0.110                   | 89                         | 0.96                   | 6.90                    | 375                    |
| 80             | 286.384                   | 0.120                   | 89                         | 0.91                   | 6.90                    | 350                    |
| 85             | 288.329                   | 0.120                   | 89                         | 0.71                   | 7.10                    | 350                    |
| 90             | 290.273                   | 0.140                   | 90                         | 0.53                   | 7.50                    | 325                    |
| 95             | 292.375                   | 0.120                   | 90                         | 0.73                   | 6.50                    | 350                    |
| 100            | 294.326                   | 0.140                   | 90                         | 0.82                   | 6.30                    | 325                    |
| 105            | 296.428                   | 0.140                   | 90                         | 0.92                   | 5.70                    | 325                    |
| 110            | 298.529                   | 0.140                   | 90                         | 0.84                   | 5.40                    | 325                    |
| 115            | 300.630                   | 0.140                   | 90                         | 0.88                   | 5.30                    | 325                    |
| 120            | 302.732                   | 0.140                   | 90                         | 1.05                   | 5.00                    | 325                    |
| 125            | 304.833                   | 0.140                   | 90                         | 1.01                   | 5.00                    | 325                    |
| 130            | 306.935                   | 0.140                   | 90                         | 0.77                   | 5.20                    | 325                    |
| 135            |                           |                         |                            |                        |                         |                        |



TABLE 2---RAW DATA

|             |                   |             |                  |
|-------------|-------------------|-------------|------------------|
| CLIENT :    | Jotul             | TEST No.    | 2                |
| MODEL:      | F400              | DATE:       | 10-Apr-00        |
| *****       |                   |             |                  |
| METER CAL.  |                   | Wt. WOOD    |                  |
| FACTOR (Y)  | ----- 0.989       | BURNED (LB) | ----- 13.3 Lbs   |
| BAROMETRIC  |                   | WET, FUEL   |                  |
| PRESS. (Pb) | ----- 30.21 in Hg | MOISTURE %  | ----- 17.164 %   |
| LEAK RATE   |                   | Wt. PART.   |                  |
| POST (Lp)   | ----- 0.006 cfm   | COLLECTED   | ----- 0.1751 g   |
| WATER       |                   | METER       |                  |
| VOL. (V1c)  | ----- 104.1 Ml    | VOLUME Vm   | ----- 53.435 mcf |
| TEST        |                   | HC MOLE     |                  |
| TIME (MIN)  | ----- 130 min     | FRACTION    | ----- 0.0132     |





TABLE 3 -----FIELD DATA AVERAGES

CLIENT :Jotul

TEST No. 2

MODEL: F400

DATE: 10-Apr-00

\*\*\*\*\*

|           |                   |           |             |   |
|-----------|-------------------|-----------|-------------|---|
| AVG DELTA |                   | AVG PRCNT |             |   |
| H         | ----- 0.14 in H2O | CO        | ----- 0.58  | % |
| AVG METER |                   | AVG PRCNT |             |   |
| TEMP. Tm  | ----- 88 deg F    | CO2       | ----- 9.22  | % |
| AVG PPM   |                   | AVG BAL   |             |   |
| SO2       | ----- 330 PPM     | CO2/CO    | ----- 15.93 | % |



TABLE 4 ----- CALCULATIONS

CLIENT : Jotul

TEST No. 2

MODEL: F400

DATE: 10-Apr-00

\*\*\*\*\*

|                    |   |                   |  |
|--------------------|---|-------------------|--|
| STD SAMPLE         |   | STACK GAS         |  |
| VOL. Vm(std) ----- | 51.48 dscf                                | FLOW Qsd -----    | 747.182 dscf/Hr<br>&<br>12.45 dscf/min |
| VOL. WATER         |   | PARTICULATE       |  |
| VAPOR Vw(std) ---- | 4.900 scf                                 | CONCTR. Cs -----  | 0.0034 g/dscf                          |
| PRCNT              |   | PARTC. EMISS.     |  |
| MSTR Bws -----     | 8.69 %                                    | RATE E -----      | 2.54 g/Hr                              |
| BURN               |   | MOLES OF GAS      |  |
| RATE BR -----      | 2.31 Kg/Hr                                | PER Lb WOOD Nt -- | 0.38 Lb-mole/Lb                        |
| CO EMISSION        |   | PART. EMISS.      |  |
| RATE -----         | 144.76 g/Hr<br>&<br>62.77 g/Kgdry<br>fuel | RATE -----        | 1.10 g/Kgdry<br>fuel                   |





TABLE 5 ----- PROPORTIONAL RATE VARIATION

CLIENT : Jotul

TEST No. : 2

MODEL: F400

DATE: 10-Apr-00

\*\*\*\*\*

| TIME<br>INTEVAL<br>Ti | PPM<br>*<br>Vm | PROPRTN.<br>RATE VAR.<br>PR | PROPRTN<br>RATE VAR.<br>AVERAGE |
|-----------------------|----------------|-----------------------------|---------------------------------|
| 5                     | 635.0          | 97                          | 100                             |
| 10                    | 642.4          | 99                          |                                 |
| 15                    | 643.3          | 99                          |                                 |
| 20                    | 645.9          | 99                          |                                 |
| 25                    | 647.4          | 99                          |                                 |
| 30                    | 649.0          | 100                         |                                 |
| 35                    | 648.1          | 99                          |                                 |
| 40                    | 650.7          | 100                         |                                 |
| 45                    | 652.6          | 100                         |                                 |
| 50                    | 652.3          | 100                         |                                 |
| 55                    | 653.6          | 100                         |                                 |
| 60                    | 653.9          | 100                         |                                 |
| 65                    | 654.1          | 100                         |                                 |
| 70                    | 653.7          | 100                         |                                 |
| 75                    | 653.7          | 100                         |                                 |
| 80                    | 653.9          | 100                         |                                 |
| 85                    | 654.1          | 100                         |                                 |
| 90                    | 653.2          | 100                         |                                 |
| 95                    | 655.2          | 101                         |                                 |
| 100                   | 654.9          | 101                         |                                 |
| 105                   | 655.2          | 101                         |                                 |
| 110                   | 654.9          | 101                         |                                 |
| 115                   | 654.9          | 101                         |                                 |
| 120                   | 655.2          | 101                         |                                 |
| 125                   | 654.9          | 101                         |                                 |
| 130                   | 655.2          | 101                         |                                 |
| 135                   |                |                             |                                 |
| 140                   |                |                             |                                 |



COMPUTER INPUT DATA SHEET #1

2,1395

Client: JOTUL U.S.A., INC.

Address: 400 RIVERSIDE STREET  
PORTLAND, ME 04104

2.54  
at 2.31 kg/hr

Phone: 207-797-5912 Fax: 207-772-0523

Run No.: 2 Date of Test: 4-10-2000 Burn Rate: 2.306

Model No.: F400  min  min-1.25  fan

Stove Type:  Cat  Non Cat  Pellet  1.25-1.9  max  insert

Dry Gas Meter: Y Factor: .989 Post Leak Rate: .006 cfm Time: 130 min.  
(0.000) (Data Sheet #2) (0.000) (Data Sheet #2) (000) (Data Sheet #2)

Dry Gas Meter Volume: 53.435 cf  
(00.000) (Data Sheet #2)

Stack Flow: 10.469 dscfm  $\Delta$  H: .138 in. H<sub>2</sub>O  
(00.000) (Data Sheet #2) (0.000) (Data Sheet #2)

Barometric Pressure: 30.21 in. Hg  
(00.00) (Data Sheet #2)

H<sub>2</sub>O Captured: 104.1 g  
(00.0) (Data Sheet #3)

Total Particulate Catch: 1751 g  
(0.0000) (Data Sheet #6)

Flue Gas Moisture: 8.7020%  
(00.000) (Data Sheet #7)

Particulate Emission: .0526 gr/dscf  
(0.0000) (Data Sheet #7)

Ambient Moisture: 1.2%  
(0.00) (Data Sheet #8)

Stove Weight: — lbs  
(000) (Data Sheet #8)

Total Fuel Consumed During Burn: 13.3 lbs  
(00.0) (Data sheet #8)

Fuel Higher Heating Value (dry): — BTU/lb  
(0000) (Data Sheet #8)

Fuel % Moisture (dry): 20.720% (wet): 17.164%  
(00.00) (Data Sheet #10)

Stack Static Pressure: .056 in. H<sub>2</sub>O  
(0.000) (Data Sheet #12)

Temperature (Average Room) Combustion Air: 81 °F  
(00) Data Sheet #14)

Stove Temperature Change: -31.2 °F  
(00.0) (Data Sheet #14)





METER BOX DATA SHEET PAGE # 2

Page: 1 of 2

UNIT: F400 RUN: 2 DATE: 4-10-2000

Meter Box: 5H Y Factor: .989

Leak checks: 16 " Hg @ 1005 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm

16 " Hg @ 1006 cfm \_\_\_\_\_ " Hg @ \_\_\_\_\_ cfm

Inject SO<sub>2</sub> @ 100 cc/min. Nozzle: Probe @ 3/8" od Initial Volume: 2.000

| ROTO: PRESS: <u>.15</u> |      |               | SAMPLING RATIO: <u>36</u> : 1 |             |         |            | BP: <u>30,22</u> |           |           |  |
|-------------------------|------|---------------|-------------------------------|-------------|---------|------------|------------------|-----------|-----------|--|
| MIN                     | TIME | METER READING | SAMPLE MDCF                   | STACK DSCFM | DELTA H | METER TEMP | SO2 PPM          | ROTO TEMP | PUMP VACC |  |
| 0                       | 1420 | 253.500       | —                             | 10.737      | .15     | 80         | 325              | 80        | 2.0       |  |
| 5                       | 25   | 255.500       | —                             | 11.632      | .17     | 80         | 300              | 80        | 2.0       |  |
| 10                      | 30   | 257.694       | 257.694                       | 11.610      | .17     | 81         | 300              | 81        | 3.0       |  |
| 15                      | 35   | 259.897       | 259.897                       | 11.567      | .17     | 83         | 300              | 83        | 3.0       |  |
| 20                      | 40   | 262.115       | 262.115                       | 10.658      | .14     | 84         | 325              | 84        | 3.0       |  |
| 25                      | 45   | 264.171       | 264.171                       | 10.638      | .14     | 85         | 325              | 85        | 3.0       |  |
| 30                      | 50   | 266.234       | 266.234                       | 10.638      | .14     | 85         | 325              | 85        | 3.0       |  |
| 35                      | 55   | 268.298       | 268.298                       | 10.599      | .14     | 87         | 325              | 87        | 3.0       |  |
| 40                      | 1500 | 270.376       | 270.376                       | 10.580      | .14     | 88         | 325              | 88        | 3.0       |  |
| 45                      | 05   | 272.462       | 272.462                       | 10.580      | .14     | 88         | 325              | 88        | 3.0       |  |
| 50                      | 10   | 274.549       | 274.549                       | 10.561      | .14     | 89         | 325              | 89        | 3.0       |  |
| 55                      | 15   | 276.642       | 276.642                       | 10.561      | .14     | 89         | 325              | 89        | 3.0       |  |
| ROTO PRESS: <u>.15</u>  |      |               | TOTALS:                       | 130.361     | 1.78    | 1019       | BP: <u>30,22</u> |           |           |  |
| 60                      | 1520 | 278.736       | 278.736                       | 9.806       | .12     | 89         | 350              | 89        | 3.0       |  |
| 65                      | 25   | 280.681       | 280.681                       | 9.806       | .12     | 89         | 350              | 89        | 3.0       |  |
| 70                      | 30   | 282.625       | 282.625                       | 9.806       | .12     | 89         | 350              | 89        | 3.0       |  |
| 75                      | 35   | 284.569       | 284.569                       | 9.153       | .11     | 89         | 375              | 89        | 3.0       |  |
| 80                      | 40   | 286.384       | 286.384                       | 9.806       | .12     | 89         | 350              | 89        | 3.0       |  |
| 85                      | 45   | 288.329       | 288.329                       | 9.806       | .12     | 89         | 350              | 89        | 3.0       |  |
| 90                      | 50   | 290.273       | 290.273                       | 10.542      | .14     | 90         | 325              | 90        | 3.0       |  |
| 95                      | 55   | 292.375       | 292.375                       | 9.789       | .12     | 90         | 350              | 90        | 3.0       |  |
| 100                     | 1600 | 294.326       | 294.326                       | 10.542      | .14     | 90         | 325              | 90        | 3.0       |  |
| 105                     | 05   | 296.428       | 296.428                       | 10.542      | .14     | 90         | 325              | 90        | 3.0       |  |
| 110                     | 10   | 298.529       | 298.529                       | 10.542      | .14     | 90         | 325              | 90        | 3.0       |  |
| 115                     | 15   | 300.630       | 300.630                       | 10.542      | .14     | 90         | 325              | 90        | 3.0       |  |
| TOTALS:                 |      |               |                               | 120.682     | 1.53    | 1074       | MAX VACC =       |           |           |  |
| TOTAL Cu Ft.            |      |               |                               | TOTALS:     | 251.043 | 3.31       | 2093             | AVG. BP:  |           |  |





METER BOX DATA SHEET PAGE # 2

Page: 2 of 2

UNIT: F400

RUN: 2

DATE: 4-10-2000

Meter Box: 5H

Y Factor: .989

Leak checks: 16 " Hg

@ .005 cfm

         " Hg @          cfm

16 " Hg

@ .006 cfm

         " Hg @          cfm

Inject SO<sub>2</sub> @ 100 cc/min.

Nozzle : Probe @ 3/8" od

Initial Volume: 2.000

| ROTO: PRESS: <u>.15</u> |             |                | SAMPLING RATIO: <u>36</u> : 1 |                |             |             | BP: <u>30.70</u> |              |            |
|-------------------------|-------------|----------------|-------------------------------|----------------|-------------|-------------|------------------|--------------|------------|
| MIN                     | TIME        | METER READING  | SAMPLE MDCF                   | STACK DSCFM    | DELTA H     | METER TEMP  | SO2 PPM          | ROTO TEMP    | PUMP VACC  |
| 120                     | <u>1620</u> | <u>302.732</u> | <u>302.732</u>                | <u>10.542</u>  | <u>.14</u>  | <u>90</u>   | <u>325</u>       | <u>90</u>    | <u>3.0</u> |
| 125                     | <u>25</u>   | <u>304.833</u> | <u>304.833</u>                | <u>10.542</u>  | <u>.14</u>  | <u>90</u>   | <u>325</u>       | <u>90</u>    | <u>3.0</u> |
| 130                     | <u>30</u>   | <u>306.935</u> | <u>306.935</u>                | <u>10.542</u>  | <u>.14</u>  | <u>90</u>   | <u>325</u>       | <u>90</u>    | <u>3.0</u> |
| 135                     |             |                |                               | <u>31.624</u>  | <u>.42</u>  | <u>270</u>  |                  |              |            |
| 140                     |             |                |                               |                |             |             |                  |              |            |
| 145                     |             |                |                               |                |             |             |                  |              |            |
| 150                     |             |                |                               |                |             |             |                  |              |            |
| 155                     |             |                |                               |                |             |             |                  |              |            |
| 160                     |             |                |                               |                |             |             |                  |              |            |
| 165                     |             |                |                               |                |             |             |                  |              |            |
| 170                     |             |                |                               |                |             |             |                  |              |            |
| 175                     |             |                |                               |                |             |             |                  |              |            |
| ROTO PRESS:             |             |                | TOTALS:                       |                |             |             | BP.:             |              |            |
| 180                     |             |                |                               |                |             |             |                  |              |            |
| 185                     |             |                |                               |                |             |             |                  |              |            |
| 190                     |             |                |                               |                |             |             |                  |              |            |
| 195                     |             |                |                               |                |             |             |                  |              |            |
| 200                     |             |                |                               |                |             |             |                  |              |            |
| 205                     |             |                |                               |                |             |             |                  |              |            |
| 210                     |             |                |                               |                |             |             |                  |              |            |
| 215                     |             |                |                               |                |             |             |                  |              |            |
| 220                     |             |                |                               |                |             |             |                  |              |            |
| 225                     |             |                |                               |                |             |             |                  |              |            |
| 230                     |             |                |                               |                |             |             |                  |              |            |
| 235                     |             |                |                               |                |             | <u>2363</u> | <u>1.21</u>      |              |            |
|                         |             |                | TOTALS:                       | <u>282.669</u> | <u>3.73</u> | <u>88</u>   | MAX VACC =       | <u>3.0</u>   |            |
| TOTAL Cu Fl.            |             | <u>53.435</u>  | TOTALS:                       | <u>10.469</u>  | <u>.138</u> | <u>548</u>  | AVG. BP:         | <u>30.21</u> |            |



**PARTICULATE CATCH / MOISTURE DATA SHEET # 3**

UNIT: F 400 RUN: 2 DATE: 4-10-00

|             |       |        |
|-------------|-------|--------|
| SCALE CHECK | LEVEL | ZEROED |
| INITIAL :   | ✓     | ✓      |
| FINAL :     | ✓     | ✓      |

|         |        |
|---------|--------|
| SCALE   | WEIGHT |
| 295.0 g | 295.0  |
| 590.0 g | 590.0  |
| 885.0 g | 885.0  |

|              |        |       |       |        |
|--------------|--------|-------|-------|--------|
| IMPINGER     | #1     | #2    | #3    | #4     |
| FINAL WT     | 684.1  | 589.1 | 515.5 | 868.1  |
| INITIAL WT   | 600.0  | 582.6 | 513.7 | 856.4  |
| NET WT GRAMS | 84.1 ✓ | 6.5 ✓ | 1.8 ✓ | 11.7 ✓ |

TOTAL CATCH: 104.1 ✓ GRAMS H<sub>2</sub>O

**FRONT HALF**

|              |       |   |
|--------------|-------|---|
| FILTER #     | 19F   |   |
| FINAL WT g   | 7202  | ✓ |
| INITIAL WT g | .6745 | ✓ |
| NET WT g     | .0457 | ✓ |

|               |            |
|---------------|------------|
| BEAKER #      | 56         |
| DESC.         | ACETONE    |
| FINAL WT g    | 104.1932 ✓ |
| INITIAL WT g  | 104.1710 ✓ |
| NET WT g      | .0222 ✓    |
| VOL. DESC. ml | 100        |

**BACK HALF**

|              |       |   |
|--------------|-------|---|
| FILTER #     | 19B   |   |
| FINAL WT g   | .4401 | ✓ |
| INITIAL WT g | .4285 | ✓ |
| NET WT g     | .0116 | ✓ |

|              |           |           |                  |                  |         |
|--------------|-----------|-----------|------------------|------------------|---------|
| BEAKER #     | 57        | 58        | 59               | 60               |         |
| DESC.        | ACETONE   | METHCHLOR | H <sub>2</sub> O | H <sub>2</sub> O |         |
| FINAL WT g   | 97.4526 ✓ | 96.9187 ✓ | 105.3735 ✓       | 106.7502 ✓       |         |
| INITIAL WT g | 97.4114 ✓ | 96.8960 ✓ | 105.2557 ✓       | 106.7316 ✓       |         |
| NET WT g     | .0412 ✓   | .0227 ✓   | .0178 ✓          | .0186 ✓          | .0364 ✓ |
| VOL. DESC ml | 140       | 75        | 150              | 175              | (325)   |





**WOODSTOVE DATA SHEET #4-1  
INITIAL FILTER WEIGHTS (TARE WEIGHTS)**

Into Dessicator: Date 10-28-99 Time: 1725 By: MEV  
 Manufacturer: S+S Grade: #25 GLASS Front Size: 11CM Lot No.: ZB921  
 Back Size: 8.2CM Lot No.: ZB911

| FILTER # | DATE: <u>11-1</u> | BY: <u>MEV</u> | DATE: <u>11-4</u> | BY: <u>MEV</u> | DATE:            | BY:  |
|----------|-------------------|----------------|-------------------|----------------|------------------|------|
|          | FIRST WEIGHT      | TIME           | SECOND WEIGHT     | TIME           | THIRD WEIGHT     | TIME |
| 11B      | .4291             | 1911           | .4291             | 1818           | JOTAL #30B R#4   |      |
| 12B      | .4316             | 1912           | .4313             | 1819           | JOTAL #30BIT R#1 |      |
| 13B      | .4299             | 1913           | .4298             | 1820           | JOTAL #30BIT R#2 |      |
| 14B      | .4306             | 1914           | .4306             | 1821           | JOTAL #30BIT R#3 |      |
| 15B      | .4313             | 1915           | .4313             | 1822           | JOTAL #30BIT R#4 |      |
| 16B      | .4319             | 1916           | .4315             | 1822           |                  |      |
| 17B      | .4278             | 1916           | .4277             | 1823           |                  |      |
| 18B      | .4302             | 1917           | .4300             | 1824           | JOTAL F400 R#1   |      |
| 19B      | .4288             | 1918           | .4285             | 1825           | JOTAL F400 R#2   |      |
| 20B      | .4340             | 1919           | .4340             | 1826           | JOTAL F400 R#3   |      |

|     |       |      |       |      |                  |  |
|-----|-------|------|-------|------|------------------|--|
| 11F | .6660 | 1928 | .6659 | 1835 | JOTAL #30B R#4   |  |
| 12F | .6837 | 1929 | .6833 | 1836 | JOTAL #30BIT R#1 |  |
| 13F | .6707 | 1930 | .6704 | 1837 | JOTAL #30BIT R#2 |  |
| 14F | .6719 | 1931 | .6722 | 1838 | JOTAL #30BIT R#3 |  |
| 15F | .6673 | 1932 | .6674 | 1839 | JOTAL #30BIT R#4 |  |
| 16F | .6809 | 1933 | .6806 | 1840 |                  |  |
| 17F | .6657 | 1934 | .6654 | 1840 |                  |  |
| 18F | .6693 | 1935 | .6690 | 1841 | JOTAL F400 R#1   |  |
| 19F | .6744 | 1935 | .6745 | 1842 | JOTAL F400 R#2   |  |
| 20F | .6654 | 1936 | .6655 | 1843 | JOTAL F400 R#3   |  |

Checked by: Opt Washington Date: 11-4-99 Time: 1905

**BALANCE ROOM ENVIRONMENTAL CONDITIONS**

| DATE | TIME | BY  | WB | DB | % RH |
|------|------|-----|----|----|------|
| 11-1 | 1815 | MEV | 5  | 73 | 46   |
| 11-4 | 1805 | MEV | 5  | 76 | 46   |









WOODSTOVE DATA SHEET # 4-3 : CONSTANT WEIGHTS

UNIT: F 400

RUN: 2

DATE: 4-10-00

| Beaker # | Date | Time | By  | First Weight | Date | Time | By  | Second Weight | Date | Time | By    | Third Weight | Date | Time | By    |
|----------|------|------|-----|--------------|------|------|-----|---------------|------|------|-------|--------------|------|------|-------|
| 56       | 4-11 | 1100 | RAW | 104.1928     | 4-12 | 1734 | RAW | 104.1932      | 4-13 | 2133 | RAW ✓ |              |      |      |       |
| 57       | 4-11 | 1145 | RAW | 97.4521      | 4-12 | 1735 | RAW | 97.4526       | 4-13 | 2135 | RAW ✓ |              |      |      |       |
| 58       | 4-11 | 1100 | RAW | 96.9183      | 4-12 | 1736 | RAW | 96.9187       | 4-13 | 2136 | RAW ✓ |              |      |      |       |
| 59       | 4-11 | 1100 | RAW | 105.3724     | 4-12 | 1737 | RAW | 105.3734      | 4-13 | 2137 | RAW   | 105.3735     | 4-14 | 1644 | RAW ✓ |
| 60       | 4-11 | 1100 | RAW | 106.7498     | 4-12 | 1738 | RAW | 106.7502      | 4-13 | 2139 | RAW ✓ |              |      |      |       |

| Filter # | Date | Time | By | First Weight | Date | Time | By  | Second Weight | Date | Time | By    | Third Weight | Date | Time | By |
|----------|------|------|----|--------------|------|------|-----|---------------|------|------|-------|--------------|------|------|----|
| 19F      | 4-10 | 1730 | CP | .7206        | 4-11 | 1155 | RAW | .7202         | 4-11 | 1914 | RAW ✓ |              |      |      |    |
| 19B      | 4-10 | 1730 | CP | .4405        | 4-11 | 1156 | RAW | .4401         | 4-11 | 1915 | RAW ✓ |              |      |      |    |

SCALE ROOM ENVIRONMENTAL CONDITIONS

| Weighing Session | Date | Time | By  | WB | DB | %RH |
|------------------|------|------|-----|----|----|-----|
| 1                | 4-11 | 1150 | RAW |    | 78 | 48  |
| 2                | 4-11 | 1910 | RAW |    | 78 | 48  |
| 3                | 4-12 | 1730 | RAW |    | 77 | 49  |
| 4                | 4-13 | 2130 | RAW |    | 76 | 48  |

| Weighing Session | Date | Time | By  | WB | DB | %RH |
|------------------|------|------|-----|----|----|-----|
| 5                | 4-14 | 1640 | RAW |    | 75 | 49  |
| 6                |      |      |     |    |    |     |
| 7                |      |      |     |    |    |     |
| 8                |      |      |     |    |    |     |





### BLANK PROCESSING DATA SHEET # 5

UNIT: F400 RUN: 2 DATE: 4-10-2000

BLANKS DONE: 12-27-99

| BEAKER       | A              | B             | C            |
|--------------|----------------|---------------|--------------|
|              | 200 ml ACETONE | 75 ml DICHLOR | 200 ml WATER |
|              | FISHER OPTIMA  | FISHER OPTIMA |              |
|              | LOT #          | LOT #         |              |
| FINAL WEIGHT | 108.9011       | 106.3073      | 106.9666     |
| TARE WEIGHT  | 108.9003       | 106.3062      | 106.9651     |
| NET WEIGHT   | .0008          | .0011         | .0015        |

TARE BEAKERS INTO DESC: TIME: 11:30 DATE: 12-20-99

DATE: 1222 BY: NW DATE: 1223 BY: NW DATE: \_\_\_\_\_ BY: \_\_\_\_\_

| BEAKER | 1 ST WT  | TIME | 2 ND WT  | TIME | 3 RD WT | TIME |
|--------|----------|------|----------|------|---------|------|
| A      | 108.8999 | 1940 | 108.9003 | 1948 | ✓       |      |
| B      | 106.3058 | 1941 | 106.3062 | 1949 | ✓       |      |
| C      | 106.9647 | 1942 | 106.9651 | 1950 | ✓       |      |

FINAL BEAKERS INTO DESC: TIME: 1330 DATE: 12-24-99

DATE: 12-24 BY: NW DATE: 12-25 BY: NW DATE: 12-27 BY: NW

| BEAKER | 1 ST WT  | TIME | 2 ND WT  | TIME | 3 RD WT  | TIME   |
|--------|----------|------|----------|------|----------|--------|
| A      | 108.8999 | 2021 | 108.9016 | 1816 | 108.9011 | 1224 ✓ |
| B      | 106.3061 | 2022 | 106.3077 | 1817 | 106.3073 | 1225 ✓ |
| C      | 106.9643 | 2023 | 106.9670 | 1818 | 106.9666 | 1226 ✓ |

#### TARE QC

| DATE  | TIME | BY | WB | DB | %  |
|-------|------|----|----|----|----|
| 12-22 | 1935 | NW | }  | 77 | 47 |
| 12-23 | 1945 | NW |    | 75 | 48 |
|       |      |    |    |    |    |

#### FINAL QC

| DATE  | TIME | BY | WB | DB | %  |
|-------|------|----|----|----|----|
| 12-24 | 1945 | NW | }  | 76 | 45 |
| 12-25 | 1740 | NW |    | 75 | 38 |
| 12-27 | 1210 | NW |    | 76 | 46 |



# NET PARTICULATE CATCH CALCULATION DATA SHEET #6

UNIT: F400 RUN: 2 DATE: 4-10-2000

## BLANK CALCULATIONS

Acetone :  $\frac{.0008 \text{ g}}{200 \text{ ml}} = .000004 \text{ g/ml}$   
 Dichloromethane :  $\frac{.0011 \text{ g}}{75 \text{ ml}} = .000015 \text{ g/ml}$   
 Distilled Water :  $\frac{.0015 \text{ g}}{200 \text{ ml}} = .000008 \text{ g/ml}$

## FRONT HALF CATCH

FILTERS :  $\frac{.0457 \text{ g}}{\text{Total Catch}} - \frac{1}{\text{\# of Filters}} (.0000 \text{ g}) = .0457 \text{ g}$

BEAKERS :  $\frac{.0222 \text{ g}}{\text{Total Catch}} - \frac{100 \text{ ml Acetone}}{\text{ml Acetone}} (.000004 \text{ g}) = .0218 \text{ g}$

TOTAL FRONT HALF CATCH : .0675 g

## BACK HALF CATCH

FILTERS :  $\frac{.0116 \text{ g}}{\text{Total Catch}} - \frac{1}{\text{\# of Filters}} (.0000 \text{ g}) = .0116 \text{ g}$

BEAKERS :  
 Acetone :  $\frac{.0412 \text{ g}}{\text{Total Catch}} - \frac{140 \text{ ml Acetone}}{\text{ml Acetone}} (.000004 \text{ g}) = .0406 \text{ g}$

Extract :  $\frac{.0227 \text{ g}}{\text{Total Catch}} - \frac{75 \text{ ml Dichloromethane}}{\text{ml Dichloromethane}} (.000015 \text{ g}) = .0216 \text{ g}$

Water :  $\frac{.0364 \text{ g}}{\text{Total Catch}} - \frac{325 \text{ ml Water}}{\text{ml Water}} (.000008 \text{ g}) = .0338 \text{ g}$

TOTAL BACK HALF CATCH : .1076 g

TOTAL CATCH : .1751 g

% FRONT HALF : 38.55 %





# CALCULATIONS DATA SHEET # 7

UNIT: F400 RUN: 2 DATE: 4-10-2000

$$1) Vm (std) = \frac{(53.435 Vm) (17.64) (989 mcf) (30.21 \text{ " Hg} + \frac{138 \text{ " H}_2\text{O}}{13.6})}{(548 \text{ TmA})} = \frac{51.4086}{000.0000} \text{ dscf} \quad \checkmark$$

$$2) Vw (std) = (.04707) (104.1 \text{ ml H}_2\text{O}) = \frac{4.9000}{00.0000} \text{ scf} \quad \checkmark$$

$$3) Asw = \frac{(4.9000 \text{ scf})}{(4.9000 \text{ scf} + \frac{51.4086 \text{ dscf}}{56.3086})} = \frac{.0870}{.0000} \text{ Bws} \times 100 = \frac{8.7020}{00.0000} \% \text{ H}_2\text{O} \quad \checkmark$$

$$4) Cs = \frac{(1751 \text{ g.})}{(51.4086 \text{ dscf})} (15.43) = \frac{.0524}{0.0000} \text{ gr / dscf} \quad \checkmark$$

$$5) \text{ Estimated g / hr} = \frac{(.1751 \text{ g.})}{(51.4086 \text{ dscf})} (10.469 \text{ dscfm}) (60) = \frac{2.1395}{00.0000} \text{ g / hr} \quad \checkmark$$

- Vm = total cubic feet pulled on meter box during test (000.000 Vm)
- mcf = meter correction factor (Y factor) of meter box used for test (0.000 mcf)
- " Hg = average barometric pressure during test (00.00 " Hg)
- " H<sub>2</sub>O = average delta H for test (.000 " H<sub>2</sub>O)
- TmA = average meter temperature for test in degrees Absolute (000 TmA)
- ml H<sub>2</sub>O = total water caught during test (000.0 ml H<sub>2</sub>O)
- g. = total particulate catch for test (00.0000 g.)
- dscfm = average stack flow during test (00.000 dscf)



### TEST DATA SHEET # 8

UNIT: F400 RUN: 2 DATE: 4-10-2000

Test Chamber Air Velocity Start: ∅ Stop: ∅ Avg.: ∅

Wet Bulb / Dry Bulb Pre: WB: 61 DB: 78 = 36 % RH 1.2 % H<sub>2</sub>O

Post: WB: 61 DB: 78 = 36 % RH 1.2 % H<sub>2</sub>O

Average: 36 %RH 1.2 % H<sub>2</sub>O

Empty Stove Weight (lbs): ✓ w/ stack & oil seal: Wet: ✓ Dry: 390.3

Kindling Weight (lbs): Paper: 1.2 Wood: 2.8

Preburn Fuel Weight: 12.1 + 14.0 + 12.3 Total: 38.4

Kindling & Preburn Fuel Weight (wood only) (lbs): Total: 41.2

Coal Bed Wt Range (lbs): 3.3 - 2.7 Scale: 393.6 - 393.0

Upper: .25 x fuel weight: Always round DOWN to nearest tenth

Lower: .20 x fuel weight: Always round UP to nearest tenth Actual Coal Bed Weight: 2.7

Maximum Coal Bed Removal (lbs):  $((\frac{3.3}{\text{Upper}} + \frac{2.7}{\text{Lower}}) \div 2) \cdot 25 = \underline{.7}$

Test Fuel (.75" x 1.5" x 5" spacers) = 20 pcs

| Dimensions | Length in inches | No. Pcs | Weight in lbs | % of Load |
|------------|------------------|---------|---------------|-----------|
| 2" x 4"    | 13               | 3       | 5.3           | 39.8      |
| 4" x 4"    | 13               | 2       | 8.0           | 60.2      |

Test Fuel Weight: 13.3 lbs

Estimated Dry Burn Rate: <sup>2.283</sup>  

$$\frac{13.3 - (13.3 \times .17164)}{2.2046} \times \frac{60}{130} = \underline{2.306} \text{ kg/hr}$$

Estimated BTU's/hr:  $19,140 \times \frac{63}{100} \times \frac{2.306}{\text{DBR}} = \underline{27,806.21} \text{ BTU's/hr}$

EPA Default Efficiencies: Non-cat: 63 Cat: 72 Pellet: 78





# WOOD STOVE OPERATING DATA PAGE #9

Unit : F400 Run : 2 Date : 4-10-2000

FIRE STARTED: 1000

### WARM UP AND PREBURN:

PRIMARY AIR : Set wide open for all warm-up / preburn fuel charges. Then set to wide open at start of preburn.

SECONDARY AIR : N/A CAT BYPASS : N/A

### CHARCOAL BED PREPARATION:

Raked and leveled prior to each warm-up / preburn charge. At 1 1/2 min. prior to loading last fuel, raked and leveled. In stove 45 sec.

### TEST:

DOOR wide open during loading 0 min. 50 sec.

PRIMARY AIR : Opened full for first 5 min., then set to run setting of wide open.

SECONDARY AIR : N/A CAT BYPASS : N/A

### FAN:

ON / OFF during warm-up

ON / OFF during preburn

ON / OFF first ALL minutes of test

ON / OFF balance of test run

Fan speed set at N/A

WOOD DATA: KINDLING: A mix of the grades listed below:

|          | SIZE | MILL         | GRADE          | SPECIES      |
|----------|------|--------------|----------------|--------------|
| PREBURN: | 2x4  | Manke/Tacoma | Std. or better | s. grn D fir |
| TEST:    | 2x4  | Packwood     | # 2 or better  | s. grn D fir |
|          | 4x4  | Packwood     | # 2 or better  | s. grn D fir |

PELLET FUEL MANUFACTURER : N/A BRAND : N/A

### All Grades WCLB rules:

### WARM UP INFORMATION:

All pre-burn / warm up fuel pieces were either 12 or 16 inches.

1st warm up / pre-burn fuel charge (12.1 lbs.) added at 1015

2nd warm up / pre-burn fuel charge (14.0 lbs.) added at 1115

3rd warm up / pre-burn fuel charge (12.3 lbs.) added at 1245

4th warm up / pre-burn fuel charge ( \_\_\_\_\_ lbs.) added at \_\_\_\_\_

5th warm up / pre-burn fuel charge ( \_\_\_\_\_ lbs.) added at \_\_\_\_\_





### TEST DATA SHEET #10

Unit : F400 Run : 2 Date : 4-10-2000

Room Temperature : 69 °F Correction Factor : φ

Uncorrected Values are corrected for room temperature : Yes \_\_\_\_\_ No

Time Test Fuel moisture reading taken : 1205

Calibration Checks : X  Y  12.0 12.1 22.0 22.1

| pc # | Dimen.   | Use | TOP   |      | BOTTOM |      | SIDE   |      | Avg Corrected |
|------|----------|-----|-------|------|--------|------|--------|------|---------------|
|      |          |     | Uncor | Cor. | Uncor. | Cor. | Uncor. | Cor. |               |
| 1    | 2"x4"x8' | K   | 12.5  | 13.3 | 14.0   | 14.9 | 14.0   | 14.9 | 14.367        |
| 2    |          |     |       |      |        |      |        |      |               |
| 3    |          |     |       |      |        |      |        |      |               |
| 4    | 2"x4"x8' | P   | 17.5  | 18.7 | 18.0   | 19.2 | 17.5   | 18.7 | 18.867        |
| 5    | 2"x4"x8' | P   | 18.5  | 19.8 | 18.5   | 19.8 | 18.5   | 19.8 | 19.800        |
| 6    | 2"x4"x8' | P   | 19.0  | 20.3 | 19.0   | 20.3 | 19.5   | 20.9 | 20.500        |
| 7    | 2"x4"x8' | P   | 18.3  | 19.8 | 18.0   | 19.2 | 18.5   | 19.8 | 19.600        |
| 8    | 2"x4"x8' | P   |       |      |        |      |        |      | 78.767        |
| 9    |          |     |       |      |        |      |        |      |               |
| 10   |          |     |       |      |        |      |        |      |               |
| 11   |          |     |       |      |        |      |        |      |               |
| 12   |          |     |       |      |        |      |        |      |               |
| 13   | 2x4x13   | T   | 17.5  | 18.7 | 17.5   | 18.7 | 18.0   | 19.2 | 18.867        |
| 14   | "        | T   | 19.0  | 20.3 | 19.5   | 20.9 | 18.5   | 19.8 | 20.333        |
| 15   | "        | T   | 18.5  | 19.8 | 18.5   | 19.8 | 19.0   | 20.3 | 19.967        |
| 16   | 4x4x13   | T   | 18.0  | 19.2 | 18.0   | 19.2 | 18.5   | 19.8 | 19.400        |
| 17   | "        | T   | 23.5  | 25.2 | 23.5   | 25.2 | 23.0   | 24.7 | 25.033        |
| 18   |          |     |       |      |        |      |        |      | 103.600       |
| 19   |          |     |       |      |        |      |        |      |               |
| 20   | Spacers  | T   | 19.5  | 20.9 | 18.0   | 19.2 | 18.0   | 19.2 | 19.767        |

Key for Use : K = Kindling P = Pretest Fuel T = Test Fuel

|                  | KINDLING | PRETEST FUEL | TEST FUEL |
|------------------|----------|--------------|-----------|
| Dry Moisture % : | 14.367 % | 19.692 %     | 20.720 %  |
| Wet Moisture % : | 12.562 % | 16.452 %     | 17.164 %  |

To obtain Wet from Dry :  $\frac{100 \times \% \text{ Dry Reading}}{100 + \% \text{ Dry Reading}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges : 16 - 20 % wet: 19 - 25 % dry (17.5 - 22.5 on Meter Uncor. reading) at 70°





UNIT: F400

RUN: 2

DATE: 4-10-2000

PAGE: 1

of 2

| TIME  | SCALE | FUEL | DROP | V.    | CO <sub>2</sub> | V.    | O <sub>2</sub> | V.    | CO    | BAL   | WB    | DB    | % H <sub>2</sub> O | CAL.WB | STACK | STATIC | SO <sub>2</sub> PPM |
|-------|-------|------|------|-------|-----------------|-------|----------------|-------|-------|-------|-------|-------|--------------------|--------|-------|--------|---------------------|
| 0     | 406.3 | 13.3 | —    | .253  | 6.3             | —     | —              | .087  | .87   | 7.2   |       |       |                    |        | 417   | 7049   | 325                 |
| 5     | 405.4 | 12.4 | .9   | .441  | 11.0            |       |                | .086  | .86   | 12.8  |       |       |                    |        | 490   | 7057   | 300                 |
| 10    | 404.4 | 11.4 | 1.0  | .515  | 12.9            |       |                | .030  | .30   | 424   |       |       |                    |        | 660   | 7062   | 300                 |
| 15    | 403.1 | 10.1 | 1.3  | .616  | 15.3            |       |                | .013  | .13   | 114.0 |       |       |                    |        | 748   | 7066   | 300                 |
| 20    | 401.8 | 8.8  | 1.3  | .647  | 16.2            |       |                | .014  | .14   | 112.5 |       |       |                    |        | 787   | 7068   | 325                 |
| 25    | 400.6 | 7.6  | 1.2  | .640  | 16.0            |       |                | .012  | .12   | 129.2 |       |       |                    |        | 798   | 7069   | 325                 |
| 30    | 399.6 | 6.6  | 1.0  | .616  | 15.4            |       |                | .013  | .13   | 115.1 |       |       |                    |        | 772   | 7067   | 325                 |
| 35    | 398.7 | 5.7  | .9   | .633  | 15.9            |       |                | .017  | .17   | 91.1  |       |       |                    |        | 766   | 7067   | 325                 |
| 40    | 397.7 | 4.7  | 1.0  | .569  | 14.2            |       |                | .066  | .06   | 222.5 |       |       |                    |        | 730   | 7066   | 325                 |
| 45    | 397.1 | 4.1  | .6   | .480  | 12.0            |       |                | .084  | .04   | 272.9 |       |       |                    |        | 780   | 7064   | 325                 |
| 50    | 396.6 | 3.6  | .5   | .400  | 10.0            |       |                | .035  | .05   | 185.2 |       |       |                    |        | 629   | 7062   | 325                 |
| 55    | 396.1 | 3.1  | .5   | .331  | 8.3             |       |                | .034  | .34   | 24.0  |       |       |                    |        | 572   | 7059   | 325                 |
| TOTAL | ----- | ---- | ---- | ----- | -----           | ----- | -----          | ----- | ----- | ----- | ----- | ----- | -----              | -----  | 8049  | 7756   | -----               |
| 60    | 395.8 | 2.8  | .3   | .313  | 7.8             |       |                | .064  | .61   | 12.7  |       |       |                    |        | 541   | 7057   | 350                 |
| 65    | 395.5 | 2.5  | .3   | .301  | 7.5             |       |                | .078  | .78   | 9.6   |       |       |                    |        | 517   | 7056   | 350                 |
| 70    | 395.2 | 2.2  | .3   | .291  | 7.3             |       |                | .081  | .89   | 8.1   |       |       |                    |        | 499   | 7054   | 350                 |
| 75    | 394.9 | 1.9  | .3   | .278  | 6.9             |       |                | .096  | .96   | 7.2   |       |       |                    |        | 487   | 7053   | 375                 |
| 80    | 394.7 | 1.7  | .2   | .277  | 6.9             |       |                | .091  | .91   | 7.6   |       |       |                    |        | 475   | 7053   | 350                 |
| 85    | 394.4 | 1.4  | .3   | .284  | 7.1             |       |                | .071  | .71   | 9.9   |       |       |                    |        | 479   | 7053   | 350                 |
| 90    | 394.1 | 1.1  | .3   | .301  | 7.5             |       |                | .053  | .53   | 14.1  |       |       |                    |        | 492   | 7054   | 325                 |
| 95    | 393.9 | .9   | .2   | .259  | 6.5             |       |                | .073  | .73   | 8.8   |       |       |                    |        | 465   | 7052   | 350                 |
| 100   | 393.7 | .7   | .2   | .253  | 6.3             |       |                | .082  | .82   | 7.7   |       |       |                    |        | 453   | 7051   | 325                 |
| 105   | 393.6 | .6   | .1   | .229  | 5.7             |       |                | .092  | .92   | 6.2   |       |       |                    |        | 430   | 7049   | 325                 |
| 110   | 393.4 | .4   | .2   | .217  | 5.4             |       |                | .084  | .84   | 6.4   |       |       |                    |        | 422   | 7049   | 325                 |
| 115   | 393.3 | .3   | .1   | .211  | 5.3             |       |                | .088  | .88   | 5.9   |       |       |                    |        | 411   | 7047   | 325                 |
| TOTAL | ----- | ---- | ---- | ----- | -----           | ----- | -----          | ----- | ----- | ----- | ----- | ----- | -----              | -----  | 5671  | 7628   | -----               |
| TOTAL | ----- | ---- | ---- | ----- | -----           | ----- | -----          | ----- | ----- | ----- | ----- | ----- | -----              | -----  | 13720 | 1784   | -----               |



























## ZERO / SPAN CHECK DATA SHEET #15-1

Date : 4-10-2000 Analyte: CO<sub>2</sub> (15-1)

Source : F400 Run # : 2

Zero Cyl. # : TX 79373 Conc. : 0.00 % CO<sub>2</sub> Cyl. Press. : 960 PSI

Certified by : AIR LIQUIDE Date : 9-22-1998

Span Cyl. # : CC52330 Conc. : 12.79 % CO<sub>2</sub> Cyl. Press. : 1750 PSI

Certified by : AIR LIQUIDE Date : 2-10-2000

Analyzer : Make : HORIBA Model : PIR-2000 SN : 407069

Range : 0 - 25.0 % CO<sub>2</sub> Analyzer Output : 0 - 1.0 v.

Flow : 1.5 SCFH Measured by : Rotameter

EPA Span Value = 25.0 % CO<sub>2</sub>

EPA Control Limits =  $\pm 2.5\%$  of 25.0 % CO<sub>2</sub> =  $\pm 0.625 % CO_2$

Method 28 A =  $\pm .2 %$  of 25.0 % CO<sub>2</sub> =  $\pm .05 % CO_2$

PRE RUN Audit : by : D. Wadsworth Time : 1230 Temp : 79 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |        | ± Conc. Difference | Δ %  |
|---------|-------------------|------|-------|-----------------|------|--------|--------------------|------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %      |                    |      |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | .002 | -0.98  | -0.98              | .393 |
| SPAN    | 51.2              | .512 | 12.79 | 51.4            | .514 | 12.862 | .072               | .287 |

POST RUN Audit : by : D. Wadsworth Time : 1640 Temp : 79 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |        | ± Conc. Difference | Δ %   |
|---------|-------------------|------|-------|-----------------|------|--------|--------------------|-------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %      |                    |       |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | .003 | -1.23  | -1.23              | -4.93 |
| SPAN    | 51.2              | .512 | 12.79 | 51.4            | .514 | 12.862 | .072               | .287  |

± Conc. Difference = Act % - Exp (Std) %

Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





## ZERO / SPAN CHECK DATA SHEET #15-2

Date: 4-10-2000 Analyte: O<sub>2</sub> (15-2)

Source: F400 Run #: 2

Zero Cyl. #: TX79373 Conc.: 0.00 % O<sub>2</sub> Cyl. Press.: 960 PSI

Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 12.69 % O<sub>2</sub> Cyl. Press.: 1750 PSI

Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: TELEDYNE Model: 320 A SN: 37400

Range: 0 - 25.0 % O<sub>2</sub> Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 25.0 % O<sub>2</sub>

EPA Control Limits =  $\pm 2.5\%$  of 25.0 % O<sub>2</sub> =  $\pm 0.625 % O_2$

Method 28 A =  $\pm .2 %$  of 25.0 % O<sub>2</sub> =  $\pm .05 % O_2$

PRE RUN Audit: by: A. Wadington Time: 1230 Temp: 79 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |          | ± Conc. Difference | Δ %    |
|---------|-------------------|------|-------|-----------------|------|----------|--------------------|--------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %        |                    |        |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | .001 | .050 ✓   | .050 ✓             | .200 ✓ |
| SPAN    | 12.7              | .508 | 12.69 | 12.7            | .510 | 12.737 ✓ | .047 ✓             | .187 ✓ |

POST RUN Audit: by: A. Wadington Time: 1640 Temp: 79 °F

### AUDIT RESULTS

| Point # | Expected Response |      |       | Actual Response |      |          | ± Conc. Difference | Δ %    |
|---------|-------------------|------|-------|-----------------|------|----------|--------------------|--------|
|         | Meter             | DVM  | %     | Meter           | DVM  | %        |                    |        |
| ZERO    | 00.0              | .000 | 00.0  | 00.0            | .000 | .025     | .025 ✓             | .100 ✓ |
| SPAN    | 12.7              | .508 | 12.69 | 12.7            | .509 | 12.712 ✓ | .022 ✓             | .088 ✓ |

± Conc. Difference = Act % - Exp (Std) %

Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$



## ZERO / SPAN CHECK DATA SHEET #15-3

Date: 4-10-2000 Analyte: CO (15-3)

Source: F400 Run #: 2

Zero Cyl. #: TX79373 Conc.: 0.00 % CO Cyl. Press.: 960 PSI  
 Certified by: AIR LIQUIDE Date: 9-22-1998

Span Cyl. #: CC52330 Conc.: 4.75 % CO Cyl. Press.: 1750 PSI  
 Certified by: AIR LIQUIDE Date: 2-10-2000

Analyzer: Make: HORIBA Model: PIR-2000 SN: 408005  
 Range: 0 - 10.0 % CO Analyzer Output: 0 - 1.0 v.  
 Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 10.0 % CO  
 EPA Control Limits =  $\pm 2.5\%$  of 10.0 % CO =  $\pm 0.25 % CO$   
 Method 28 A =  $\pm .2 %$  of 10.0 % CO =  $\pm .02 % CO$

PRE RUN Audit: by: A. Wharton Time: 1230 Temp: 79 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |         | ± Conc. Difference | Δ %     |
|---------|-------------------|------|------|-----------------|------|---------|--------------------|---------|
|         | Meter             | DVM  | %    | Meter           | DVM  | %       |                    |         |
| ZERO    | 00.0              | .000 | 00.0 | 00.0            | .000 | .004    | .004 ✓             | .042 ✓  |
| SPAN    | 47.5              | .475 | 4.75 | 47.3            | .473 | 4.732 ✓ | -.018 ✓            | -.179 ✓ |

POST RUN Audit: by: A. Wharton Time: 1640 Temp: 79 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |         | ± Conc. Difference | Δ %     |
|---------|-------------------|------|------|-----------------|------|---------|--------------------|---------|
|         | Meter             | DVM  | %    | Meter           | DVM  | %       |                    |         |
| ZERO    | 00.0              | .000 | 00.0 | 00.1            | .001 | .014    | .014 ✓             | .142 ✓  |
| SPAN    | 47.5              | .475 | 4.75 | 47.3            | .473 | 4.732 ✓ | -.018 ✓            | -.179 ✓ |

± Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





## ZERO / SPAN CHECK DATA SHEET #15-4

Date: 4-10-2000 Analyte: SO<sub>2</sub> (15-4)

Source: F400 Run #: 2

Zero Cyl. #: TX79373 Conc.: 0.00 ppm SO<sub>2</sub> Cyl. Press.: 960 PSI  
 Certified by: AIR LIQUINE Date: 9-22-1998

Span Cyl. #: 1167475 Conc.: 1260 ppm SO<sub>2</sub> Cyl. Press.: 650 PSI  
 Certified by: AIR LIQUINE Date: 9-22-1998

Analyzer: Make: HORIBA Model: PIR-2000 SN: 403019  
 Range: 0 - 2500 ppm SO<sub>2</sub> Analyzer Output: 0 - 1.0 v.  
 Flow: 1.5 SCFH Measured by: Rotameter

EPA Span Value = 2500 ppm SO<sub>2</sub>  
 EPA Control Limits = ± 2.5% of 2500 ppm SO<sub>2</sub> = ± 62.5 ppm SO<sub>2</sub>

PRE RUN Audit: by: D. Wadsworth Time: 1240 Temp: 80 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |          | ± Conc. Difference | Δ %     |
|---------|-------------------|------|------|-----------------|------|----------|--------------------|---------|
|         | Meter             | DVM  | PPM  | Meter           | DVM  | %        |                    |         |
| ZERO    | 00.0              | .000 | 00.0 | 00.5            | .005 | 25.410   | 25.410             | 1.016 ✓ |
| SPAN    | 50.4              | .504 | 1260 | 50.5            | .505 | 1262.571 | 2.571              | .103 ✓  |

POST RUN Audit: by: D. Wadsworth Time: 1645 Temp: 78 °F

### AUDIT RESULTS

| Point # | Expected Response |      |      | Actual Response |      |          | ± Conc. Difference | Δ %    |
|---------|-------------------|------|------|-----------------|------|----------|--------------------|--------|
|         | Meter             | DVM  | PPM  | Meter           | DVM  | %        |                    |        |
| ZERO    | 00.0              | .000 | 00.0 | 00.4            | .004 | 22.936   | 22.936             | .917 ✓ |
| SPAN    | 50.4              | .504 | 1260 | 50.6            | .506 | 1265.046 | 5.046              | .202 ✓ |

± Conc. Difference = Act % - Exp (Std) %  
 Zero % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$   
 Span % Difference =  $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$





### QUALITY CHECKS DATA SHEET # 16

UNIT : F400 RUN : 2 DATE : 4-10-2000

**Thermocouple Check :**

|                          |                           |
|--------------------------|---------------------------|
| T/C # 1 <u>      </u> °F | T/C # 13 <u>61.1</u> °F   |
| T/C # 2 <u>      </u> °F | T/C # 14 <u>60.0</u> °F   |
| T/C # 3 <u>60.5</u> °F   | T/C # 15 <u>61.6</u> °F   |
| T/C # 4 <u>57.5</u> °F   | T/C # 16 <u>59.4</u> °F   |
| T/C # 5 <u>56.8</u> °F   | T/C # 17 <u>59.5</u> °F   |
| T/C # 6 <u>56.6</u> °F   | T/C # 18 <u>63.1</u> °F   |
| T/C # 7 <u>56.7</u> °F   | T/C # 19 <u>58.5</u> °F   |
| T/C # 8 <u>56.4</u> °F   | T/C # 20 <u>55.8</u> °F   |
| T/C # 9 <u>56.9</u> °F   | T/C # 21 <u>      </u> °F |
| T/C # 10 <u>57.0</u> °F  | T/C # 22 <u>      </u> °F |
| T/C # 11 <u>55.9</u> °F  | T/C # 23 <u>58.9</u> °F   |
| T/C # 12 <u>63.8</u> °F  | T/C # 24 <u>      </u> °F |

**Thermocouple Readout :**

|  |                         |                          |
|--|-------------------------|--------------------------|
| Pretest zero and span check and calibration      | post test zero and span | % difference             |
| ZERO : <u>1.4</u> °F Adj. to <u>0.0</u> °F       | ZERO <u>2.2</u> °F      | Difference <u>.110</u> % |
| SPAN : <u>1995.4</u> °F Adj. to <u>2000.0</u> °F | SPAN <u>2004.9</u> °F   | Difference <u>.245</u> % |

**Thermocouple Readout Pretest Linearity Check**

|                         |                         |                         |
|-------------------------|-------------------------|-------------------------|
| 0 = <u>0.0</u> °F       | 200 = <u>201.6</u> °F   | 400 = <u>398.9</u> °F   |
| 600 = <u>601.2</u> °F   | 800 = <u>801.4</u> °F   | 1000 = <u>1000.5</u> °F |
| 1200 = <u>1198.1</u> °F | 1400 = <u>1399.1</u> °F | 1600 = <u>1599.6</u> °F |
| 1800 = <u>1800.0</u> °F | 2000 = <u>2000.0</u> °F |                         |

|                                  |              |               |  |
|----------------------------------|--------------|---------------|--|
| Sample Train Leak Check          | Pre <u>✓</u> | Post <u>✓</u> |  |
| C-gas Train Leak Check           | Pre <u>✓</u> | Post <u>✓</u> |  |
| SO <sub>2</sub> Train Leak Check | Pre <u>✓</u> | Post <u>✓</u> |  |
| Static Gauge Zero Check          | Pre <u>X</u> | Post <u>✓</u> |  |

Scale Check Pre : 404.8 - 394.8  
 Post : 402.8 - 392.8

Stack Cleaned Prior to Test Run : YES \_\_\_\_\_ NO X









# INSPECTION CERTIFICATE



**CUSTOMER:** LOKEE TESTING      **DATE OF INSPECTION:** 10-6-99  
**ADDRESS:** 13235 Prairie Circle E  
Sumner, WA 98390      **NEXT INSPECTION DUE:** 4-00  
**TECHNICIAN:** Patrick McKellan  
**AUTHORIZATION SIGNATURE:** \_\_\_\_\_  
**CERTIFICATION TYPE**  
 STANDARD  
 ISO 9000  
 MIL STD-45662

934 Elliott Avenue W.  
 Seattle, WA 98119  
 Ph#(206)284-6090  
 Fax#(206)282-6612

## EQUIPMENT TESTED

| INDICATOR  | BASE   | OPTIONS INSTALLED             |
|--|--|-------------------------------|
| MAKE <u>Weightronix</u>  | _____  | PRINTER _____                 |
| MODEL <u>WI-110</u>  | _____  | SCORE BOARD _____             |
| SR# <u>16409</u>   | _____  | COMPUTER _____                |
| CLASS <u>III</u>   | _____  | OTHER _____                   |
| CAP. <u>1000 x .1 lbs</u>                                      | _____  |                               |
| <b>PRE-TEST</b>  | <b>POST-TEST</b>   | <b>MANUFACTURER TOLERANCE</b> |
| <u>∅</u>   | <u>∅</u>   | _____                         |
| <u>500.3</u>   | <u>499.9</u>   | _____                         |
| <u>1000.6</u>  | <u>1000.0</u>  | _____                         |
| <u>∅</u>   | <u>∅</u>   | _____                         |
| <u> </u>   | <u> </u>   | _____                         |
| <u> </u>   | <u> </u>   | _____                         |
| <b>CORNER TEST</b>   | P <input checked="" type="checkbox"/> F _____                              |                               |
| <b>SHIFT TEST</b>  | P <input checked="" type="checkbox"/> F _____                              |                               |
| <b>STATIC TEST</b>   | 2 MIN. <input type="checkbox"/> 5 MIN. <input checked="" type="checkbox"/> |                               |
| <b>WEIGHT KIT#</b> _____                                       | <b>NIST#</b> _____   |                               |
| <b>SERIAL NUMBERS OF WEIGHTS USED (OR COPY OF CERTIFICATE)</b> |  |                               |
| <u>T07821</u>  | _____  | _____                         |
| <u>T07822</u>  | _____  | _____                         |
| _____  | _____  | _____                         |
| _____  | _____  | _____                         |





CONSUMER & PRODUCER PROTECTION DIVISION  
WEIGHTS & MEASURES SECTION  
METROLOGY LABORATORY  
2747 29TH AVENUE SOUTHWEST  
UMWATER WASHINGTON 98512

## REPORT OF TEST

**Test Item**

Test Weights  
Type: Cast Iron  
Nominal Value/Range: 1000 & 500 lb  
Serial No: See table 1 below  
WO No: L1596

**Submitted By**

Phillips Scale Company  
934 Elliott Ave. W  
Seattle, WA 98119

Purchase Order No: ALEC  
Alec Jorgensen, (206) 284-6090

**Table 1**

| Nominal Value | Manufacture | Qty | Serial Number   |
|---------------|-------------|-----|---|
| 1000 lb       | Rice Lake   | 8   | WA183-9, WA184-0, WA184.1, WA184-2, WA184-3, WA184-4, WA184-5 & WA184-6         |
| 1000 lb       | Toledo      | 1   | WA184-7   |
| 500 lb        | Toledo      | 11  | 117, 401, 407, 1WWM, T07821, T07822, T07823, T07824, WA152-8, WA153-0 & WA153-1 |

**Condition of Test Item:**

**Good** - The test item displays some wear or other degradation.

**Measurement Results:** The test item described above was found/adjusted to be within the National Institute of Standards and Technology (NIST) Tolerance Class F values.

**Measurement Method & Traceability:** Measurements were made IAW the NIST handbook 145, SOP 8, Tolerance Testing of Mass Standards by Modified Substitution. Standards are traceable to the NIST (reports on file) and which are part of a comprehensive measurement assurance program for ensuring continued accuracy and traceability within the level of uncertainty reported by this laboratory.

**General Conditions / Notes:** *Unless otherwise stated or provided for :*

- The results of this test apply only to the test item stated on this report.
- The following test items were found out of tolerance and adjusted: 1000 lb SN: WA184-7; 500 lb SN: 401, T07822, T07823 & 1WWM
- Measurement Room Ambient Conditions: Temperature 21.0 °C ± 1 °C; Relative Humidity 41.0 % ± 5 % RH; Barometric Pressure 758.0 mmHg





# QUALITY CONTROL SERVICES Inc.

2340 S.E. 11Th. Avenue Portland, Oregon 97214-5306

(503) 236-2712 / FAX:(503) 235-2535

## CERTIFICATE OF CALIBRATION

### Customer and Contact

Lokee Testing Labs  
13235 Prairie Circle East  
Sumner, WA. 98390  
Chip Wadington

Report Number: QCS-00002878

### INSTRUMENT INFORMATION

| Item        | Make             | Model    | Serial Number | Units    | Cal. Date      | Last Cal.  | Cal. Due |
|-------------|------------------|----------|---------------|----------|----------------|------------|----------|
| Balance     | Sartorius        | A120S    | 37010004      | Grams    | 12/13/1999     | 05/25/1999 | 05/2000  |
| Readability | Range Calibrated | Location | Customer ID   | SOP Used | Tolerance Used |            |          |
| 0.0001      | 0-100            | Lab      | N/A           | QCS #004 | Factory        |            |          |

### Functional Checks

Cornerload  Linearity 0 - 1/2 - Full Capacity  Reproduceability

### CALIBRATION DATA

| Standard | As Found Instrument | Tolerance +/- | As Left Instrument |
|----------|---------------------|---------------|--------------------|
| 100      | 99.9986             | 0.0002        | 100.0000           |
| 50       | 49.9993             | 0.0002        | 50.0000            |
| 20       | 19.9997             | 0.0002        | 20.0000            |
| 10       | 9.9998              | 0.0002        | 10.0000            |
| 5        | 4.9999              | 0.0002        | 5.0000             |
| 1        | 1.0000              | 0.0002        | 1.0000             |

### CALIBRATION STANDARDS

| Item       | Make            | Model    | Serial Number | Units | Cal. Date  | Cal. Due | NIST Traceable ID# |
|------------|-----------------|----------|---------------|-------|------------|----------|--------------------|
| Weight Set | R.Lake/Troemner | 5MG-25KG | A45           | Grams | 07/09/1999 | 07/2000  | 822/262273-9       |

Comments / Info Concerning This Calibration:

Permanent Information Concerning This Instrument:

12/99 CUSTOMER REQUESTED SPECIFIC 6 POINT CHECK.

Technician: D.Deleasa

Signature: 

CALIBRATIONS ARE PERFORMED UNDER AMBIENT CONDITIONS USING MANUFACTURER'S SPECIFICATIONS FOR THE PASS/FAIL RESULTS. RESULTS MAY BE INFLUENCED BY THE AGE OF THE INSTRUMENT AND ENVIRONMENTAL CONDITIONS. CALIBRATION DATA SHOULD BE REVIEWED TO INSURE THAT THE INSTRUMENT IS PERFORMING TO ITS INTENDED ACCURACY. CALIBRATIONS CONFORM TO ANSI / NCSL Z540-1-1994 SPECIFICATIONS.

THIS CERTIFICATE SHALL NOT BE REPRODUCED, EXCEPT IN FULL, WITHOUT THE WRITTEN APPROVAL OF QUALITY CONTROL SERVICES, INC.





# QUALITY CONTROL SERVICES Inc.

2340 S.E. 11Th. Avenue Portland, Oregon 97214-5306

(503) 236-2712 / FAX:(503) 235-2535

## CERTIFICATE OF CALIBRATION

### Customer and Contact

Lokee Testing Labs.  
13235 Prairie Circle East  
Sumner, WA. 98390  
Chip Wadington

### INSTRUMENT INFORMATION

| Item        | Make             | Model    | Serial Number | Units    | Last Cal. Date | Cal. Date  | Cal. Due |
|-------------|------------------|----------|---------------|----------|----------------|------------|----------|
| Balance     | Sartorius        | A120S    | 37010004      | Grams    | 11/21/1998     | 05/25/1999 | 11/1999  |
| Readability | Range Calibrated | Location | Customer ID   | SOP Used | Limits Used    |            |          |
| 0.0001      | 0-100            | Lab      | N/A           | QCS #004 | Factory        |            |          |

### Functional Checks

Cornerload

Linearity 0 - 1/2 - Full Capacity

Reproduceability

### CALIBRATION DATA

| Standard | As Found Instrument | Limit +/- | As Left Instrument |
|----------|---------------------|-----------|--------------------|
| 100      | 100.0018            | 0.0002    | 100.0000           |
| 50       | 50.0009             | 0.0002    | 50.0000            |
| 20       | 20.0004             | 0.0002    | 20.0000            |
| 10       | 10.0002             | 0.0002    | 10.0000            |
| 5        | 5.0001              | 0.0002    | 5.0000             |
| 1        | 1.0001              | 0.0002    | 1.0000             |

### CALIBRATION STANDARDS

| Item       | Make      | Model    | Serial Number | Units | Cal. Date  | Cal. Due | NIST Traceable ID# |
|------------|-----------|----------|---------------|-------|------------|----------|--------------------|
| Weight Set | Rice Lake | 1MG-20KG | A45           | Grams | 07/07/1998 | 07/1999  | 822/251337         |

Comments / Info:

Technician: D.Deleasa

Signature: 

ALL CALIBRATION STANDARDS ARE TRACEABLE TO THE NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY (N.I.S.T.). ALL WORK IS PERFORMED USING PROPER MANUFACTURER AND/OR INDUSTRIAL SERVICE TECHNIQUES AND IS WARRANTED FOR 30 DAYS. CALIBRATIONS CONFORM TO ANSI / NCSL Z540 / MIL STANDARD 45662A.

THIS CERTIFICATE SHALL NOT BE REPRODUCED, EXCEPT IN FULL, WITHOUT THE WRITTEN APPROVAL OF QUALITY CONTROL SERVICES, INC.



## Thermocouple Calibration Record Semi-Annual

Thermocouples Check against

Reference Thermometer

serial number 9123454

Ice Water Bath

32°

Boiling Water

212°

Room Temperature

73°

Barometric Pressure

30.50

DATE: 11-20-99

| TC | Location      | Ice Bath Temp | Boiling Water Temp |
|----|---------------|---------------|--------------------|
| 1  | Wet Bulb      | 32.1          | 211.7              |
| 2  | Dry Bulb      | 32.2          | 211.6              |
| 3  | Stack         | 32.1          | 211.8              |
| 4  | Stove Top     | 32.1          | 211.2              |
| 5  | Left Side     | 32.0          | 212.0              |
| 6  | Back          | 32.1          | 212.3              |
| 7  | Right Side    | 32.0          | 211.8              |
| 8  | Bottom        | 32.1          | 211.6              |
| 9  | Firebox       | 32.1          | 211.3              |
| 10 | Secondary/Cat | 32.1          | 211.9              |
| 11 | Ambient       | 32.3          | 211.7              |
| 12 | Tube Furnace  | 32.1          | 212.0              |
| 13 | Sample Box    | 32.0          | 211.3              |
| 14 | Impinger Out  | 32.1          | 211.6              |
| 15 | C. Gas Box    | 32.0          | 212.1              |
| 16 | C. Gas Out    | 32.2          | 211.7              |
| 17 | SO2 Out       | 32.2          | 211.7              |
| 18 | Upper Ambient | 32.1          | 211.9              |
| 19 |               |               |                    |
| 20 |               |               |                    |
| 21 |               |               |                    |
| 22 |               |               |                    |
| 23 | Calibrator    | 32.2          | 211.9              |
| 24 | Oven          | 32.1          | 211.5              |





### Thermocouple Readout Semi-Annual Calibration Data Sheet

Date: 11-20-99  
 Ambient Temperature: 75  
 Technician: Chip W.

Thermocouple Number: T/C Readout  
 Barometric Pressure: 30.50  
 Reference: Mercury in glass  
FISHER #9123454  
 Other: OMEGA CL-300

| Reference Point No. <sup>a</sup> | Source <sup>b</sup> | Reference Thermometer Temperature °F | Thermocouple Potentiometer Temperature °F | Difference (%) <sup>c</sup> |
|----------------------------------|---------------------|--------------------------------------|---|-----------------------------|
| 32                               | Ice Water           | 32°                                  | 32°                                       | ∅                           |
| 212                              | Boiling Water       | 212°                                 | 211.9°                                    | .047                        |
| 250                              | Omega               | 250.0                                | 249.8                                     | .080                        |
| 300                              | Omega               | 300.0                                | 299.4                                     | .200                        |
| 400                              | Omega               | 400.0                                | 398.4                                     | .200                        |
| 500                              | Omega               | 500.0                                | 499.2                                     | .160                        |
| 600                              | Omega               | 600.0                                | 601.0                                     | -.167                       |
| 700                              | Omega               | 700.0                                | 698.9                                     | .157                        |
| 800                              | Omega               | 800.0                                | 801.3                                     | -.163                       |
| 900                              | Omega               | 900.0                                | 898.8                                     | .133                        |
| 1000                             | Omega               | 1000.0                               | 1000.2                                    | -.020                       |
| 1200                             | Omega               | 1200.0                               | 1197.8                                    | .183                        |
| 1400                             | Omega               | 1400.0                               | 1398.9                                    | .079                        |
| 1600                             | Omega               | 1600.0                               | 1599.4                                    | .038                        |
| 1800                             | Omega               | 1800.0                               | 1799.9                                    | .006                        |
| 2000                             | Omega               | 2000.0                               | 2000.0                                    | ∅                           |

<sup>a</sup> Every 50°F for each reference point

<sup>b</sup> Type of Calibration System Used

<sup>c</sup> 
$$\frac{(\text{reference temperature}) - (\text{thermocouple temperature})}{\text{reference temperature}} * 100$$



TRACEABILITY DOCUMENTATION Semi-Annual

SO<sub>2</sub> INJECTION ROTAMETER, DRY GAS METER AND SLING PSYCHROMETER  
THERMOMETERS IN LAB. CHECKED AGAINST FISHER SN 9123454 (NIST).

DATE: 11-20-99

SO<sub>2</sub> INJECTION ROTAMETER  
9123454

FISHER SN

NIST Traceable

| Actual | °C = °F | °F    |
|--------|---------|-------|
| 0°     | 32.0    | 32.0  |
| 22.5   | 72.5    | 72.5  |
| 41.0   | 93.5    | 93.1  |
| 68.0   | 154.4   | 154.6 |

DRY GAS METER THERMOCOUPLES

| Actual | °C = °F | 5H in | 5H out | KK    |
|--------|---------|-------|--------|-------|
| 0      | 32°     | 32.2  | 32.4   | 32.2  |
| 22.0   | 71.6    | 71.1  | 71.4   | 71.4  |
| 39.8   | 103.6   | 103.1 | 103.5  | 103.5 |
| 66.9   | 152.4   | 152.0 | 152.1  | 152.5 |

SLING PSYCHROMETER

| Actual | °C = °F | Wet Bulb | Dry Bulb |
|--------|---------|----------|----------|
| 0      | 32°     | 32.0     | 32.0     |
| 10.5   | 51.4    | 51.4     | 51.3     |
| 17.1   | 62.8    | 62.8     | 62.8     |
| 27.3   | 81.1    | 81.2     | 81.1     |

Conversions =

$$°F = (°C \times 1.8) + 32$$

$$°C = (°F - 32) \div 1.8$$





## **VANEOMETER CALIBRATION**

LoKee Testing Lab uses a Dwyer Model #480 Vaneometer to measure test chamber air velocity. The manufacturer's specifications for accuracy are  $\pm 5.0\%$  to 100 FPM and  $\pm 10\%$  from FPM to top of scale. LoKee Testing Lab insures that the instrument is level and clean prior to taking each reading. According to EPA personnel (Westlin, RTP) no further calibration of the instrument is necessary.

## **DRAFT GAUGE CALIBRATION**

LoKee Testing Lab uses a Dwyer model 115-AV 0-0.25" inclined water manometer (readability resolution  $\pm 0.001"$  of water) to measure the static pressure in the stack. Once leveled and zeroed as per the manufacturer's written operating instructions, the Dwyer manometer is a primary standard and requires no additional calibration.

The manometer is leveled and zeroed at the start of each test run, checked as necessary during the run to verify the settings have not changed and again at the end of each test run. The results of each check are recorded on Data Sheet #16 in each test run.

## **BAROMETER CALIBRATION**

LoKee Testing Lab uses a Princo Model 469 NOVA Mercury Barometer to measure barometric pressure. When installed and maintained as per the manufacturer's written operating instruction, the Princo Model 469 Mercury Barometer is a primary standard and needs no further calibration.

## **MOISTURE METER CALIBRATION**

The Delmhorst Model RC-1C, SN 16152 Moisture Meter is calibrated each time the meter is used by adjusting the zero and span calibration. The potentiometers of each calibration point (X = zero, Y = span) are adjusted until the meter is calibrated correctly. The meter is then checked against a calibration block (Delmhorst Model MCS-1, moisture content standard at 12.0% and 22.0%) in its normal operating range of 11-25%.

LoKee Testing Lab also has a second moisture meter, Delmhorst Model G-30, SN 2477 to use as a backup.





POST TEST METER BOX AUDIT DATA SHEET # 32

UNIT: Jotul F400

DATE: 4-14-00

TEST DATA

| RUN #                  | 1                               | 2    | 3    | 4    | 5  | 6 | 7 | 8 | 9 | 10 |
|------------------------|---------------------------------|------|------|------|--|---|---|---|---|----|
| AVG. Δ H               | .138                            | .138 | .155 | .110 |  |   |   |   |   |    |
| MAX VAC                | 3.0                             | 3.0  | 4.0  | 2.0  |  |   |   |   |   |    |
| Avg. Test Series Δ H : | <u>.135</u> in H <sub>2</sub> O |      |      |      | Test Series Max Vac: <u>4.0</u> in Hg        |   |   |   |   |    |
| Audit Dry Gas Meter :  | <u>'K2'</u>                     |      |      |      | Correction ( Y ) Factor : <u>1.014</u> (mcf) |   |   |   |   |    |
| Test Dry Gas Meter :   | <u>H</u>                        |      |      |      | Correction ( Y ) Factor : <u>.989</u> (mcf)  |   |   |   |   |    |

AUDIT DATA

|                 |         | Audit # 1      | Audit # 2      | Audit # 3      |
|-----------------|---------|----------------|----------------|----------------|
| BP              |         | <u>30.04</u>   | <u>30.04</u>   | <u>30.04</u>   |
| VAC             |         | <u>4.0</u>     | <u>4.0</u>     | <u>4.0</u>     |
| AUDIT METER :   |         |                |                |                |
| VOL. (Vw)       | Final   | <u>938.800</u> | <u>944.189</u> | <u>951.378</u> |
|                 | Initial | <u>933.500</u> | <u>938.800</u> | <u>944.189</u> |
|                 | Vol.    | <u>5.300</u>   | <u>5.389</u>   | <u>7.189</u>   |
| TEMP (°F) (Tw)  | Initial | <u>84</u>      | <u>88</u>      | <u>88</u>      |
|                 | Mid     | <u>86</u>      | <u>86</u>      | <u>88</u>      |
|                 | Final   | <u>88</u>      | <u>88</u>      | <u>88</u>      |
| (°F / °A)       | Avg.    | <u>86</u>      | <u>86</u>      | <u>88</u>      |
| Δ H             | Initial | <u>.135</u>    | <u>.135</u>    | <u>.135</u>    |
|                 | Mid     | <u>.135</u>    | <u>.135</u>    | <u>.135</u>    |
|                 | Final   | <u>.135</u>    | <u>.135</u>    | <u>.135</u>    |
|                 | Avg.    | <u>.135</u>    | <u>.135</u>    | <u>.135</u>    |
| DRY GAS METER : |         |                |                |                |
| VOL. (Vd)       | Final   | <u>433.300</u> | <u>438.700</u> | <u>445.900</u> |
|                 | Initial | <u>428.000</u> | <u>433.300</u> | <u>438.700</u> |
|                 | Vol.    | <u>5.300</u>   | <u>5.400</u>   | <u>7.200</u>   |
| TEMP (°F) (Tm)  | Initial | <u>75</u>      | <u>75</u>      | <u>75</u>      |
|                 | Mid     | <u>75</u>      | <u>75</u>      | <u>75</u>      |
|                 | Final   | <u>75</u>      | <u>75</u>      | <u>75</u>      |
| (°F / °A)       | Avg.    | <u>75</u>      | <u>75</u>      | <u>75</u>      |



$$Y = \frac{(V_w)(mcf)(BP)(T_m)}{(V_d) \left( BP + \frac{DH}{13.6} \right) (T_w)}$$

$$Y \text{ Factor } \% \text{ Diff.} = \frac{\text{Act} - \text{Exp}}{\text{Exp}} \times 100$$

NOTE : mcf = meter correction ( Y ) factor for Dry Gas Meter used as a transfer standard

RUN 1

$$Y = \frac{(5.300)(30.04)(.989)(535)}{(5.300) \left( 30.04 + \frac{.135}{13.6} \right) (546)} = \frac{84241.46}{86958.48} = .969$$

$$\Delta \% = \frac{(.969 - .990)}{.990} \times 100 = -2.121 \%$$

RUN 2

$$Y = \frac{(5.389)(30.04)(.989)(535)}{(5.400) \left( 30.04 + \frac{.135}{13.6} \right) (548)} = \frac{85656.08}{88923.74} = .963$$

$$\Delta \% = \frac{(.963 - .990)}{.990} \times 100 = -2.727 \%$$

RUN 3

$$Y = \frac{(7.189)(30.04)(.989)(535)}{(7.200) \left( 30.04 + \frac{.135}{13.6} \right) (548)} = \frac{114266.38}{118564.99} = .964$$

$$\Delta \% = \frac{(.964 - .990)}{.990} \times 100 = -2.626 \%$$

NOTE : The Y factor % difference must be < ± 5.0 % to be acceptable

**INTERPOLATED Y FACTOR**

$$\frac{.1}{(A)} \text{ inch H}_2\text{O } \Delta H = \frac{.993}{(C)}$$

Calculated calibration Y factor from calibrations

$$\frac{.2}{(B)} \text{ inch H}_2\text{O } \Delta H = \frac{.983}{(D)}$$

Calculated calibration Y factor from calibrations

$$\frac{.2}{(B)} - \frac{.1}{(A)} = \frac{.1}{(D)} \times 100 = \frac{10}{(E)}$$

$$\frac{.983}{(D)} - \frac{.993}{(C)} = -.010 + \frac{10}{(E)} = \frac{-.001}{(F)}$$

$$\frac{.135}{\text{Avg } \Delta H} - \frac{.1}{(A)} = \frac{.035}{(G)} \times 100 = \frac{3.5}{(F)}$$

$$\left[ \frac{-.001}{(F)} \times \frac{3.5}{(G)} \right] + \frac{.993}{(C)} = \frac{.990}{\text{Interpolated Y factor}}$$

Volume Metering System Leak Check : 0.000 inch H<sub>2</sub>O in one minute





## DRY GAS METER CALIBRATION

DATE: 11-20-99 DRY GAS METER: H BOX: 5

| BAROMETRIC PRESSURE, Pb  |                    | 30.14   |         | in. Hg.  |         | K <sup>2</sup> mcf = 1.014 |          |
|--|--------------------|---------|---------|----------|---------|----------------------------|----------|
| Orifice Manometer Setting, ΔH, in. H <sub>2</sub> O                                      |                    | .1      | .2      | .3       | .5      | .75                        | 1.0      |
| Gas Volume<br>Wet Test Meter<br>Vw ft <sup>3</sup>                                       | Final              | 801.943 | 866.820 | 871.717  | 876.623 | 881.544                    | 886.474  |
|  | Initial            | 857.075 | 861.943 | 866.820  | 871.717 | 876.623                    | 881.544  |
|  | Vw ft <sup>3</sup> | 4.868   | 4.877   | 4.897    | 4.906   | 4.921                      | 4.935    |
| Gas Volume<br>Dry Test Meter<br>Vd ft <sup>3</sup>                                       | Final              | 950.000 | 955.000 | 960.000  | 965.000 | 970.000                    | 975.000  |
|  | Initial            | 945.000 | 950.000 | 955.000  | 960.000 | 965.000                    | 970.000  |
|  | Vd ft <sup>3</sup> | 5.000   | 5.000   | 5.000    | 5.000   | 5.000                      | 5.000    |
| Wet Test<br>Meter<br>Temperature<br>tw   | Initial            | 67      | 77      | 79       | 81      | 81                         | 81       |
|  | Middle             | 72      | 78      | 80       | 81      | 81                         | 81       |
|  | Final              | 77      | 79      | 81       | 81      | 81                         | 81       |
|  | Average            | 72      | 78      | 81 (54)  | 81      | 81                         | 81       |
| Dry Test<br>Meter<br>Temperature<br>tm   | Initial            | 75      | 75      | 76       | 77      | 78                         | 79       |
|  | Middle             | 75      | 76      | 77       | 78      | 78                         | 79       |
|  | Final              | 75      | 76      | 77       | 78      | 79                         | 79       |
|  | Average            | 75      | 76      | 77 (537) | 78      | 78                         | 79 (539) |
| $Y = \frac{(W_{mcf}) (Vw) (Pb) (tm)}{Vd \left[ Pb + \frac{\Delta H}{13.6} \right] (tw)}$ |                    | .993    | .983    | .985     | .988    | .991                       | .995     |

Average Y = .989



## METER BOX CALIBRATION

**Date :** 06/08/99  
**Calibrated By :** J.C.  
**Dry Gas Meterbox ID :** K2

**Barometric Pressure, Pb =** 27.41 in. Hg  
**Vacuum =** 0.0 in. Hg

**Orifice Manometer  
Setting, Delta H**

|         |      |      |      |      |      |      |
|---------|------|------|------|------|------|------|
| in. H2O | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
|---------|------|------|------|------|------|------|

**Gas Volume Wet Test Meter**

|             |       |       |       |       |       |       |
|-------------|-------|-------|-------|-------|-------|-------|
| Vw, cu. ft. | 5.000 | 5.000 | 5.000 | 5.000 | 5.000 | 5.000 |
|-------------|-------|-------|-------|-------|-------|-------|

**Gas Volume Dry Gas Meter**

|             |         |         |         |         |         |         |
|-------------|---------|---------|---------|---------|---------|---------|
| M Final     | 905.062 | 910.109 | 915.164 | 920.215 | 925.284 | 930.346 |
| M Initial   | 900.000 | 905.062 | 910.109 | 915.164 | 920.215 | 925.284 |
| Vd, cu. ft. | 5.062   | 5.047   | 5.055   | 5.051   | 5.069   | 5.062   |

**Wet Test Meter**

|          |     |     |     |     |     |     |
|----------|-----|-----|-----|-----|-----|-----|
| tw Deg F | 79  | 79  | 80  | 80  | 80  | 80  |
| tw Deg A | 539 | 539 | 540 | 540 | 540 | 540 |

**Dry Gas Meter**

|             |    |    |    |    |    |    |    |
|-------------|----|----|----|----|----|----|----|
| Outlet, tmo | 1) | 88 | 90 | 90 | 91 | 91 | 91 |
|             | 2) | 89 | 90 | 91 | 91 | 91 | 91 |
|             | 3) | 90 | 91 | 91 | 91 | 91 | 91 |

**Dry Gas Meter**

|           |    |    |    |     |     |     |     |
|-----------|----|----|----|-----|-----|-----|-----|
| Inlet tmi | 1) | 91 | 95 | 98  | 101 | 103 | 103 |
|           | 2) | 93 | 97 | 99  | 102 | 103 | 104 |
|           | 3) | 96 | 99 | 101 | 103 | 104 | 104 |

**Mean tm, Deg F**

|                |     |     |     |     |     |     |
|----------------|-----|-----|-----|-----|-----|-----|
| Mean tm, Deg F | 91  | 94  | 95  | 97  | 97  | 97  |
| Mean tm, Deg A | 551 | 554 | 555 | 557 | 557 | 557 |

**Results :**

|     |       |       |       |       |       |       |
|-----|-------|-------|-------|-------|-------|-------|
| Y = | 1.009 | 1.017 | 1.016 | 1.020 | 1.018 | 1.019 |
|-----|-------|-------|-------|-------|-------|-------|

**Averages :**

|     |       |
|-----|-------|
| Y = | 1.017 |
|-----|-------|

*1.014*



## METER BOX CALIBRATION

**Date :** 06/08/99  
**Calibrated By :** J.C.  
**Dry Gas Meterbox ID :** K2

**Barometric Pressure, Pb =** 27.41 in. Hg  
**Vacuum =** 0.0 in. Hg

**Orifice Manometer**

**Setting, Delta H**  
**in. H2O**                      0.20              0.20              0.20              0.20              0.20              0.20

**Gas Volume Wet Test Meter**

**Vw, cu. ft.**                      5.000              5.000              5.000              5.000              5.000              5.000

**Gas Volume Dry Gas Meter**

|                    |         |         |         |         |         |         |
|--------------------|---------|---------|---------|---------|---------|---------|
| <b>M Final</b>     | 935.565 | 940.624 | 945.687 | 950.756 | 955.828 | 960.905 |
| <b>M Initial</b>   | 930.500 | 935.565 | 940.624 | 945.687 | 950.756 | 955.828 |
| <b>Vd, cu. ft.</b> | 5.065   | 5.059   | 5.063   | 5.069   | 5.072   | 5.077   |

**Wet Test Meter**

|                 |     |     |     |     |     |     |
|-----------------|-----|-----|-----|-----|-----|-----|
| <b>tw Deg F</b> | 79  | 80  | 80  | 80  | 80  | 80  |
| <b>tw Deg A</b> | 539 | 540 | 540 | 540 | 540 | 540 |

**Dry Gas Meter**

|                    |    |    |    |    |    |    |    |
|--------------------|----|----|----|----|----|----|----|
| <b>Outlet, tmo</b> | 1) | 91 | 91 | 91 | 92 | 92 | 92 |
|                    | 2) | 91 | 91 | 92 | 92 | 92 | 92 |
|                    | 3) | 91 | 91 | 92 | 92 | 92 | 92 |

**Dry Gas Meter**

|                   |    |    |     |     |     |     |     |
|-------------------|----|----|-----|-----|-----|-----|-----|
| <b>Inlet, tmi</b> | 1) | 94 | 97  | 100 | 102 | 104 | 105 |
|                   | 2) | 95 | 98  | 101 | 104 | 104 | 105 |
|                   | 3) | 97 | 100 | 102 | 104 | 105 | 105 |

|                       |     |     |     |     |     |     |
|-----------------------|-----|-----|-----|-----|-----|-----|
| <b>Mean tm, Deg F</b> | 93  | 95  | 96  | 98  | 98  | 99  |
| <b>Mean tm, Deg A</b> | 553 | 555 | 556 | 558 | 558 | 559 |

**Results :**

|            |       |       |       |       |       |       |
|------------|-------|-------|-------|-------|-------|-------|
| <b>Y =</b> | 1.012 | 1.015 | 1.017 | 1.018 | 1.018 | 1.018 |
|------------|-------|-------|-------|-------|-------|-------|

**Averages :**

|            |              |
|------------|--------------|
| <b>Y =</b> | <b>1.016</b> |
|------------|--------------|





## METER BOX CALIBRATION

**Date :** 06/08/99  
**Calibrated By :** J.C.  
**Dry Gas Meterbox ID :** K2

**Barometric Pressure, Pb =** 27.43 in. Hg  
**Vacuum =** 0.0 in. Hg

### Orifice Manometer

Setting, Delta H

in. H2O                      0.30              0.30              0.30              0.30              0.30              0.30

### Gas Volume Wet Test Meter

Vw, cu. ft.                      5.000              5.000              5.000              5.000              5.000              5.000

### Gas Volume Dry Gas Meter

|             |         |         |         |         |         |         |
|-------------|---------|---------|---------|---------|---------|---------|
| M Final     | 966.054 | 971.113 | 976.179 | 981.252 | 986.332 | 991.415 |
| M Initial   | 961.000 | 966.054 | 971.113 | 976.179 | 981.252 | 986.332 |
| Vd, cu. ft. | 5.054   | 5.059   | 5.066   | 5.073   | 5.080   | 5.083   |

### Wet Test Meter

|          |     |     |     |     |     |     |
|----------|-----|-----|-----|-----|-----|-----|
| tw Deg F | 80  | 80  | 80  | 80  | 80  | 80  |
| tw Deg A | 540 | 540 | 540 | 540 | 540 | 540 |

### Dry Gas Meter

|             |    |    |    |    |    |    |    |
|-------------|----|----|----|----|----|----|----|
| Outlet, tmo | 1) | 89 | 90 | 91 | 91 | 91 | 92 |
|             | 2) | 90 | 91 | 91 | 92 | 92 | 92 |
|             | 3) | 90 | 91 | 91 | 92 | 92 | 92 |

### Dry Gas Meter

|            |    |    |     |     |     |     |     |
|------------|----|----|-----|-----|-----|-----|-----|
| Inlet, tmi | 1) | 95 | 97  | 100 | 103 | 104 | 105 |
|            | 2) | 97 | 99  | 102 | 103 | 104 | 105 |
|            | 3) | 98 | 100 | 103 | 104 | 105 | 105 |

|                |     |     |     |     |     |     |
|----------------|-----|-----|-----|-----|-----|-----|
| Mean tm, Deg F | 93  | 95  | 96  | 98  | 98  | 99  |
| Mean tm, Deg A | 553 | 555 | 556 | 558 | 558 | 559 |

### Results :

|     |       |       |       |       |       |       |
|-----|-------|-------|-------|-------|-------|-------|
| Y = | 1.012 | 1.014 | 1.016 | 1.017 | 1.016 | 1.017 |
|-----|-------|-------|-------|-------|-------|-------|

### Averages :

|     |       |
|-----|-------|
| Y = | 1.015 |
|-----|-------|













## METER BOX CALIBRATION

**Date :** 06/08/99  
**Calibrated By :** J.C.  
**Dry Gas Meterbox ID :** K2

**Barometric Pressure, Pb =** 27.43 in. Hg  
**Vacuum =** 0.0 in. Hg

**Orifice Manometer**

**Setting, Delta H**

**in. H2O**                      1.00              1.00              1.00              1.00              1.00              1.00

**Gas Volume Wet Test Meter**

**Vw, cu. ft.**                      5.000              5.000              5.000              5.000              5.000              5.000

**Gas Volume Dry Gas Meter**

|                    |          |          |          |          |          |          |
|--------------------|----------|----------|----------|----------|----------|----------|
| <b>M Final</b>     | 1058.090 | 1063.183 | 1068.279 | 1073.379 | 1078.486 | 1083.599 |
| <b>M Initial</b>   | 1053.000 | 1058.090 | 1063.183 | 1068.279 | 1073.379 | 1078.486 |
| <b>Vd, cu. ft.</b> | 5.090    | 5.093    | 5.096    | 5.100    | 5.107    | 5.113    |

**Wet Test Meter**

|                 |     |     |     |     |     |     |
|-----------------|-----|-----|-----|-----|-----|-----|
| <b>tw Deg F</b> | 80  | 80  | 80  | 80  | 80  | 80  |
| <b>tw Deg A</b> | 540 | 540 | 540 | 540 | 540 | 540 |

**Dry Gas Meter**

|                    |    |    |    |    |    |    |    |
|--------------------|----|----|----|----|----|----|----|
| <b>Outlet, tmo</b> | 1) | 90 | 91 | 92 | 93 | 94 | 94 |
|                    | 2) | 90 | 91 | 92 | 93 | 94 | 95 |
|                    | 3) | 91 | 91 | 93 | 94 | 94 | 95 |

**Dry Gas Meter**

|                  |    |     |     |     |     |     |     |
|------------------|----|-----|-----|-----|-----|-----|-----|
| <b>Inlet tmi</b> | 1) | 101 | 102 | 103 | 103 | 104 | 105 |
|                  | 2) | 101 | 102 | 103 | 104 | 104 | 106 |
|                  | 3) | 102 | 103 | 103 | 104 | 105 | 106 |

|                       |     |     |     |     |     |     |
|-----------------------|-----|-----|-----|-----|-----|-----|
| <b>Mean tm, Deg F</b> | 96  | 97  | 98  | 99  | 99  | 100 |
| <b>Mean tm, Deg A</b> | 556 | 557 | 558 | 559 | 559 | 560 |

**Results :**

|            |       |       |       |       |       |       |
|------------|-------|-------|-------|-------|-------|-------|
| <b>Y =</b> | 1.009 | 1.009 | 1.011 | 1.011 | 1.011 | 1.012 |
|------------|-------|-------|-------|-------|-------|-------|

**Averages :**

|            |       |
|------------|-------|
| <b>Y =</b> | 1.011 |
|------------|-------|



Wet Test Meter Serial Number AA455 Date 4/16/99

Range of Wet Test Meter Flow Rate 0 - 0.25

Volume of Test Flask  $V_s$  = 37.850 liters

Satisfactory Leak Check? YES

Ambient Temperature of Equilibrate Liquid in Wet Test Meter and Reservoir 69 deg. F

| Test Number | Manometer Reading, a mm H2O | Final Volume (VF), l | Initial Volume (VI), l | Total Volume (Vm), b l | Flask Volume (Vs), l | Percent Error, c % |
|-------------|-----------------------------|----------------------|------------------------|------------------------|----------------------|--------------------|
| 1           | 0                           | 3.0 (12 revs)        | 0*                     | 3.0                    | 3.012                | 0.408              |
| 2           | 0                           | 3.0 (12 revs)        | 0*                     | 3.0                    | 3.008                | 0.288              |
| 3           | 0                           | 3.0 (12 revs)        | 0*                     | 3.0                    | 3.014                | 0.478              |

\*reset for each test

a - Must be less than 10 mm H2O (0.4 "H2O)

Calculations:

b -  $V_m - VF - VI$

c - % error =  $100(V_m - V_s)/V_s = \frac{(100)(3.012-3.000)}{3.000} = (+1\%)$

WET TEST METER CALIBRATION LOG





## SO<sub>2</sub> ROTAMETER CALIBRATION

Last Cal. : 4-10-99 By: C.W. Date : 11-20-99 By: G. Wadlington

Manufacturer : SKC-WEST

SKC ACCUFLOW Digital Flow Calibrator: Model 712

SN : 311325

Barometric Pressure : 30.48 " Hg      Temperature : 69

| RUN #   | 50 CC/MINUTE   | 100 CC/MINUTE  | 150 CC/MINUTE  |
|---------|----------------|----------------|----------------|
|         | DIGITAL VOLUME | DIGITAL VOLUME | DIGITAL VOLUME |
| 1       | 55.0           | 128.0          | 185.0          |
| 2       | 55.2           | 127.8          | 185.1          |
| 3       | 54.9           | 128.1          | 185.3          |
| 4       | 55.2           | 127.9          | 185.0          |
| 5       | 55.0           | 128.1          | 185.3          |
| 6       | 55.1           | 128.4          | 185.6          |
| 7       | 55.2           | 128.5          | 185.5          |
| 8       | 55.4           | 128.3          | 185.4          |
| 9       | 55.1           | 128.1          | 185.6          |
| 10      | 55.2           | 128.4          | 185.3          |
| AVERAGE | 55.1 cc/min    | 128.2 cc/min   | 185.3 cc/min   |

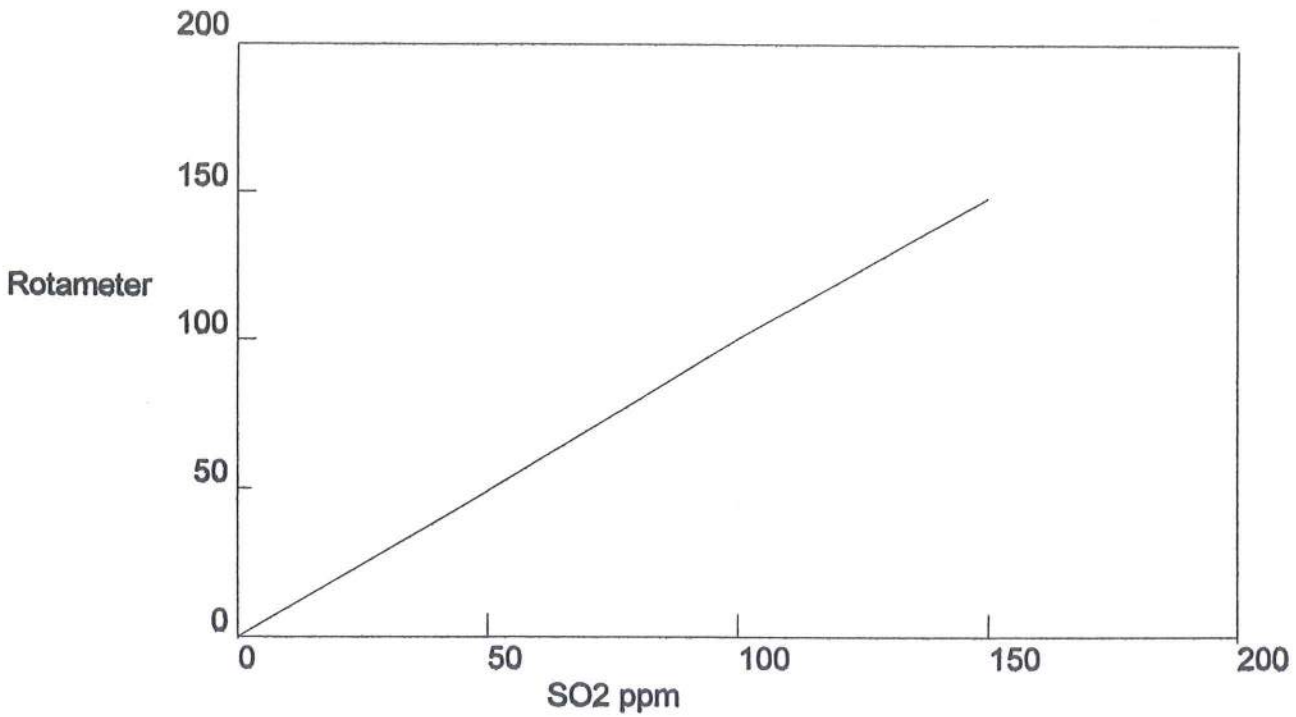
| SETTING | cc/min |
|---------|--------|
| 0       | 0.0    |
| 50      | 55.1   |
| 100     | 128.2  |
| 150     | 185.3  |

Rotometer setting for 100 cc/minute based on regression with this data.

100 CC / MINUTE = 81.2



SO2 Rotameter  
20-Nov-99



Regression Output:

|                     |              |
|---------------------|--------------|
| Constant            | -2.2         |
| Std Err of Y Est    | 5.4221766847 |
| R Squared           | 0.9970364173 |
| No. of Observations | 4            |
| Degrees of Freedom  | 2            |
| X Coefficient(s)    | 1.258        |
| Std Err of Coef.    | 0.0484974226 |









ORSAT ANALYSIS DATA SHEET

DATE: 11-20-99

| Gas             | 1    | 2    | 3     | AVE  | CONC           | TANK ID   |
|-----------------|------|------|-------|------|----------------|-----------|
| CO <sub>2</sub> | 0    | 0    | 0     | 0    | N <sub>2</sub> | TX-79373  |
| O <sub>2</sub>  | 0    | 0    | 0     | 0    | N <sub>2</sub> |           |
| CO              | 0    | 0    | 0     | 0    | N <sub>2</sub> |           |
| CO <sub>2</sub> | 12.4 | 12.4 | 12.4  | 12.4 | 12.4           | CC-52549  |
| O <sub>2</sub>  | 12.5 | 12.5 | 12.5  | 12.5 | 12.51          |           |
| CO              | 5.1  | 5.0  | 5.1   | 5.07 | 5.08           |           |
| CO <sub>2</sub> | 21.0 | 21.0 | 21.0  | 21.0 | 21.00          | AAL 7152  |
| O <sub>2</sub>  | 21.0 | 20.9 | 21.00 | 20.7 | 21.00          |           |
| CO              | 8.5  | 8.5  | 8.5   | 8.5  | 8.51           |           |
| CO <sub>2</sub> | 6.2  | 6.3  | 6.3   | 6.27 | 6.25           | AAL 21084 |
| O <sub>2</sub>  | 6.3  | 6.2  | 6.2   | 6.23 | 6.24           |           |
| CO              | 2.0  | 2.0  | 2.0   | 2.00 | 2.01           |           |
| CO <sub>2</sub> |      |      |       |      |                |           |
| O <sub>2</sub>  |      |      |       |      |                |           |
| CO              |      |      |       |      |                |           |





**CO<sub>2</sub> ANALYZER  
MULTIPOINT CALIBRATION REPORT FORM**

F400

Date: 3-31-2000

Analyzer: Make: HORIBA Model: PIR 2000 SN: 407069

Calibration by: C. Wadlington

Cal Gas Flow: 1.5 SCFH Measured by: Rotameter

BP: 30.50

Instrument ID: PRINCO

Temp: 76

Instrument ID: TR

Analyzer last calibrated: \_\_\_\_\_ By: \_\_\_\_\_

**Cylinders:**

1. # TX 79373 Concentration: 00.00 % CO<sub>2</sub> Cyl. Press.: 960 PSI  
 Certified by: Air Liquide Date: 9-22-98
2. # CC52330 Concentration: 12.79 % CO<sub>2</sub> Cyl. Press.: 1750 PSI  
 Certified by: Air Liquide Date: 2-10-2000
3. # CC55904 Concentration: 21.23 % CO<sub>2</sub> Cyl. Press.: 1610 PSI  
 Certified by: Air Liquide Date: 2-14-2000
4. # AAL 21084 Concentration: 6.25 % CO<sub>2</sub> Cyl. Press.: 1320 PSI  
 Certified by: Scott Specialty Gases Date: 5-15-97

Analyzer: **Calibrated Range:** 0-25.0 %  
**Flow:** 1.5 SCFH

**Output:** 0-1.0 V.  
**Measured by:** Rotameter

**Calibration Results**

| Point # | CYL. # | % CO <sub>2</sub> | EXPE CTED |      | ACT UAL |      | ADJ.  |      | % DIF. | ROTENTIOMETER |      |
|---------|--------|-------------------|-----------|------|---------|------|-------|------|--------|---------------|------|
|         |        |                   | METER     | DVM  | METER   | DVM  | METER | DVM  |        | UNADJ.        | ADJ. |
| 1       | 1      | 0.00              | 0.00      | .000 | 0.00    | .000 | —     | —    |        |               |      |
| 2       | 2      | 12.79             | 51.2      | .512 | 50.8    | .508 | 51.2  | .512 |        |               |      |
| 3       | 3      | 21.23             | 84.9      | .849 | 84.6    | .846 | —     | —    |        |               |      |
| 4       | 4      | 6.25              | 25.0      | .250 | 25.3    | .253 | —     | —    |        |               |      |
| 5       | 1      | 0.00              | 00.0      | .000 | 0.00    | .000 | —     | —    |        |               |      |

.5 = 12.510





**CO<sub>2</sub> Linear Regression Results:**

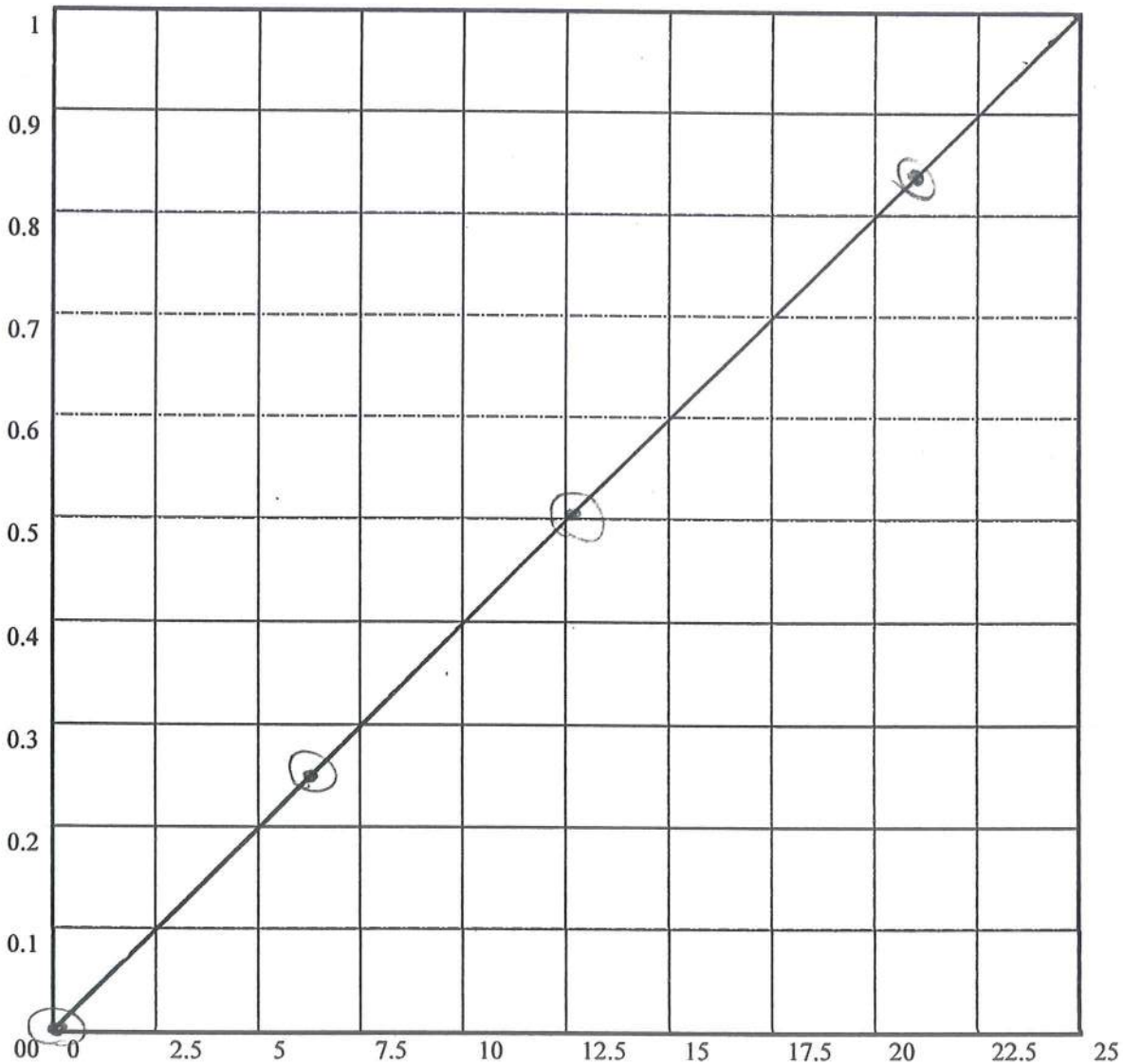
$Y = MX + B$

Slope (M) = 0.0019212

Y Intercept (B) = 0.0398141

Correlation Coefficient (r) = 0.9999862

$r^2 =$  0.9999725



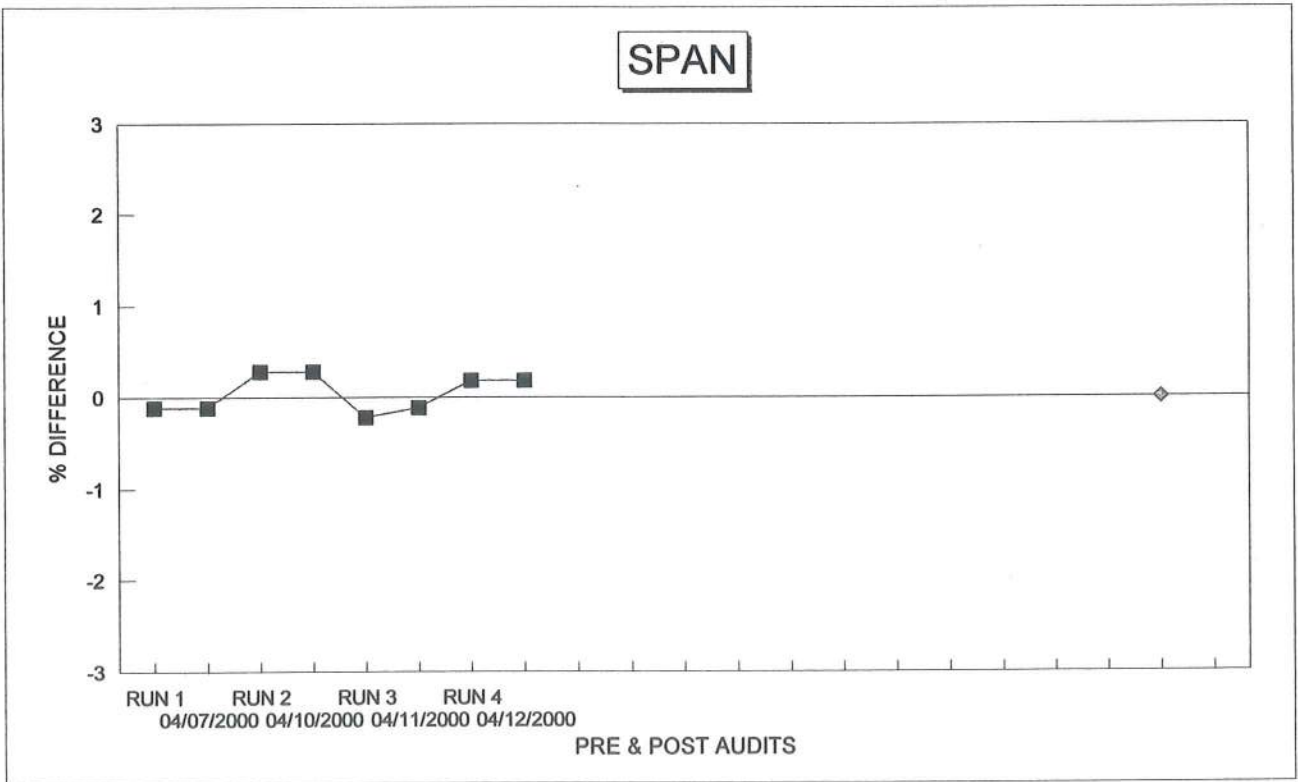
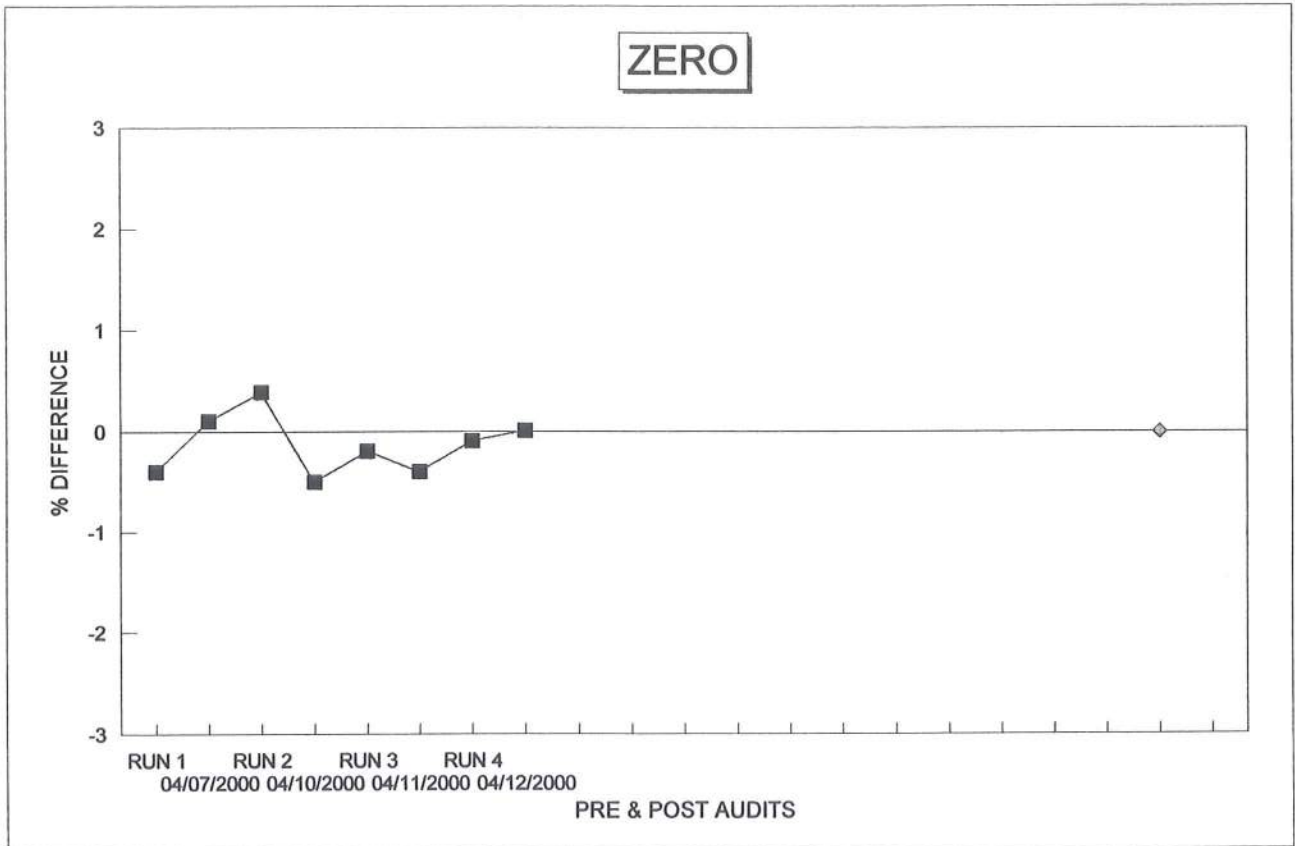
EPA Span Value =  $\pm 2.0\%$  of 25% CO<sub>2</sub> =  $\pm .5\%$

Cal Volts = Cal Volt Conc - Std Conc =  $\pm$  Conc Diff =  $\pm \Delta \%$

$0.846 = 21.133 - 21.23 = -0.097 = -0.386$

$0.7253 = 6.320 - 6.25 = 0.070 = 0.280$









**O<sub>2</sub> ANALYZER  
MULTIPOINT CALIBRATION REPORT FORM**

Date: 3-31-2000

Analyzer: Make: TELEDYNE Model: 320A SN: 37400

Calibration by: C. Wadlington

Cal Gas Flow: 1.5 SCFH Measured by: Rotameter

BP: 30.50

Instrument ID: PRINCO

Temp: 74

Instrument ID: TR

Analyzer last calibrated: \_\_\_\_\_ By: \_\_\_\_\_

**Cylinders:**

1. # TX 79373 Concentration: 00.00% O<sub>2</sub> Cyl. Press.: 960 PSI  
 Certified by: Air Liquide Date: 9-22-98
2. # CC 52330 Concentration: 12.69% O<sub>2</sub> Cyl. Press.: 1750 PSI  
 Certified by: Air Liquide Date: 2-10-2000
3. # CC 55904 Concentration: 21.10% O<sub>2</sub> Cyl. Press.: 1610 PSI  
 Certified by: Air Liquide Date: 2-14-2000
4. # AAL 21084 Concentration: 6.24% O<sub>2</sub> Cyl. Press.: 1320 PSI  
 Certified by: Scott Specialty Gases Date: 5-15-97

Analyzer: **Calibrated Range:** 0-25.0 % **Output:** 0-1.0 V.  
**Flow:** 1.5 SCFH **Measured by:** Rotameter

**Calibration Results**

| Point # | CYL. # | % O <sub>2</sub> | EXPE CTED |      | ACT UAL |      | ADJ.  |     | % DIF. | ROTENTIOMETER |      |
|---------|--------|------------------|-----------|------|---------|------|-------|-----|--------|---------------|------|
|         |        |                  | METER     | DVM  | METER   | DVM  | METER | DVM |        | UNADJ.        | ADJ. |
| 1       | 1      | 0.00             | 0.00      | .000 | 0.00    | .000 | -     | -   |        |               |      |
| 2       | 2      | 12.69            | 12.7      | .508 | 12.7    | .508 | -     | -   |        |               |      |
| 3       | 3      | 21.10            | 21.1      | .844 | 21.2    | .846 | -     | -   |        |               |      |
| 4       | 4      | 6.24             | 6.24      | .250 | 6.2     | .248 | -     | -   |        |               |      |
| 5       | 1      | 0.00             | 0.00      | .000 | 0.00    | .000 | -     | -   |        |               |      |

**.5 = 12.488**



**O<sub>2</sub> Linear Regression Results:**

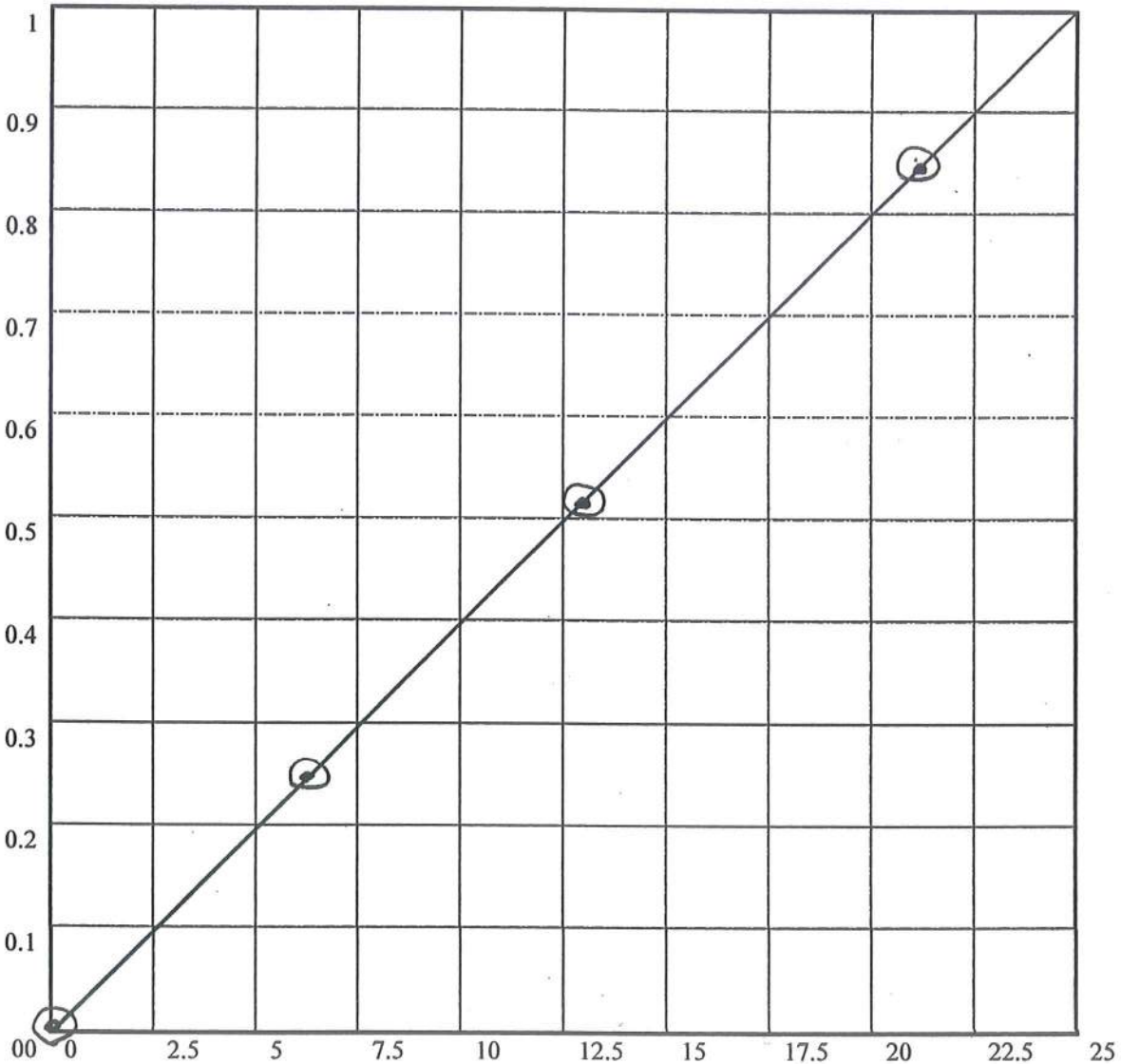
$Y = MX + B$

Slope (M) = -0.0009983

Y Intercept (B) = 0.0401197

Correlation Coefficient (r) = -0.9999961

$r^2 =$  0.9999922



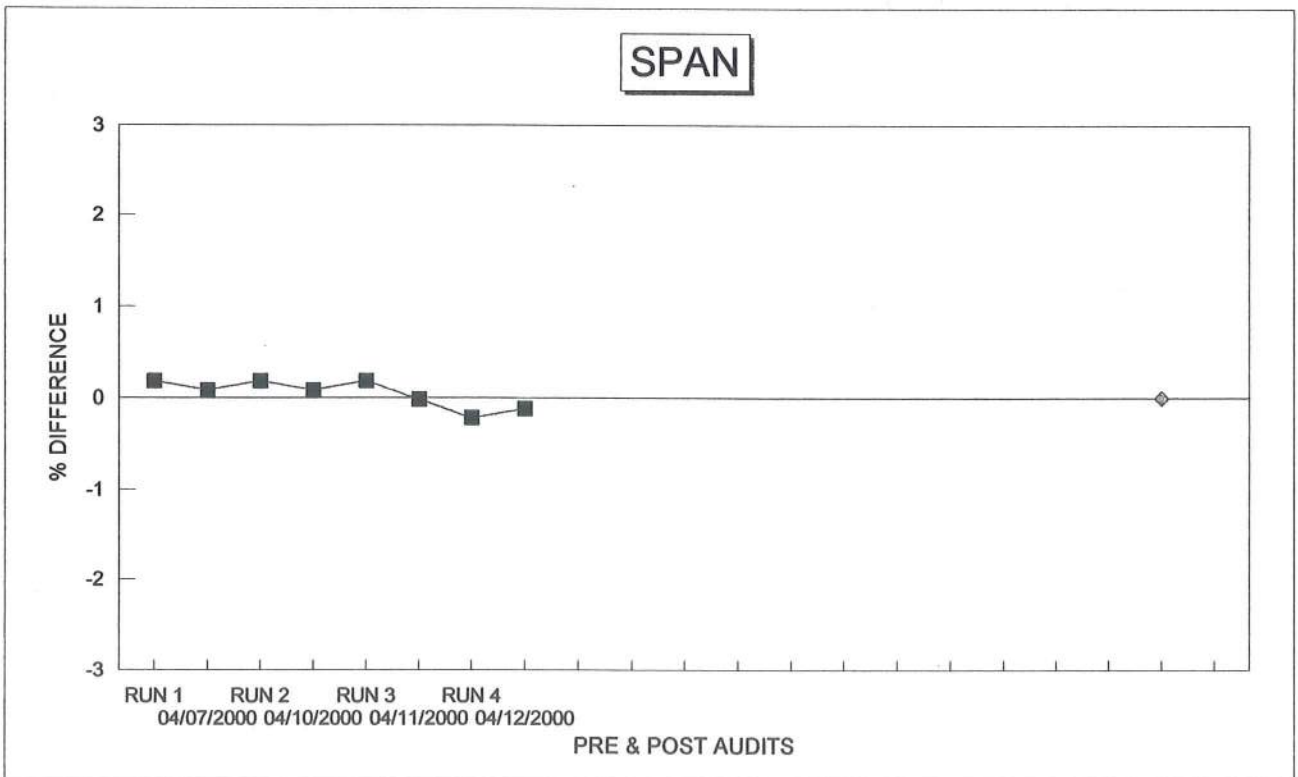
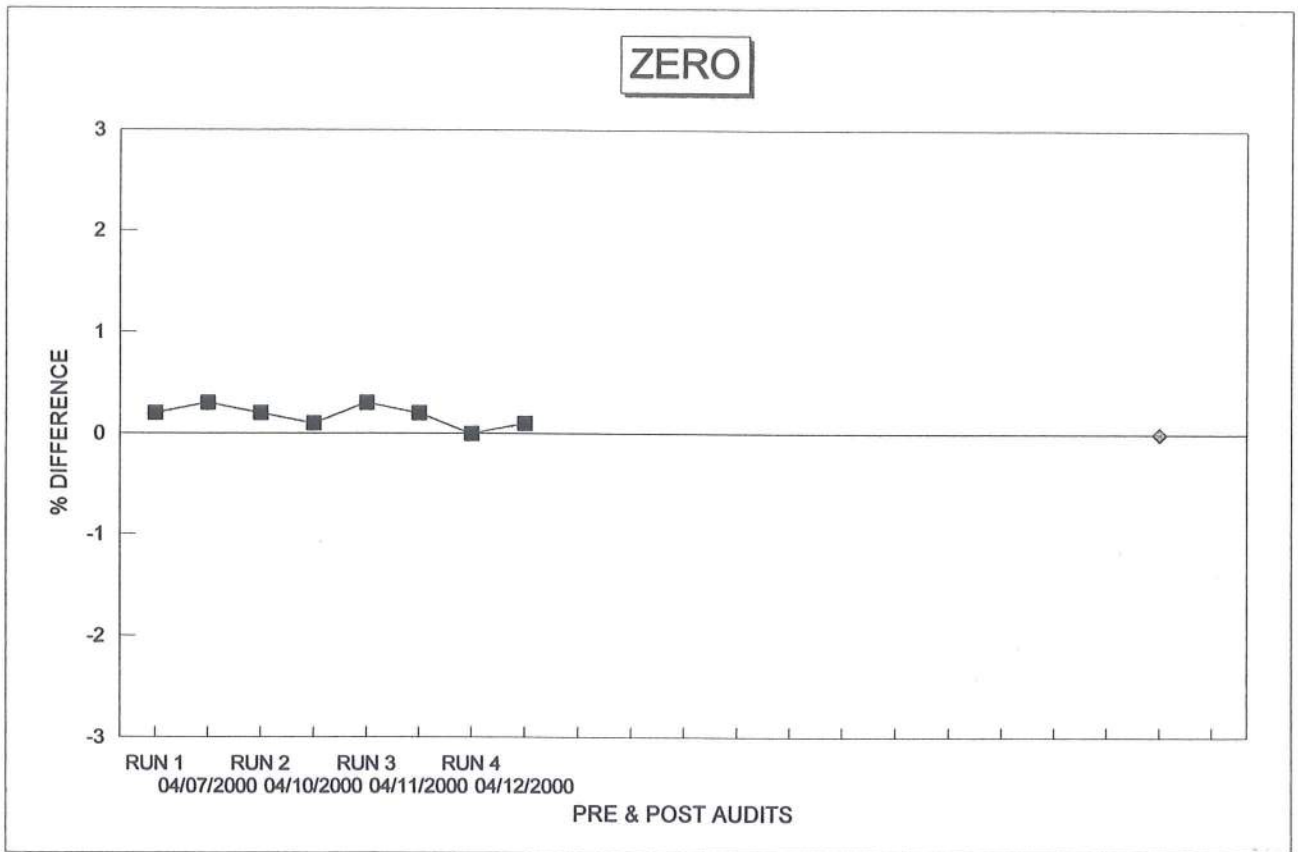
EPA Span Value =  $\pm 2.0\%$  of  $25\% \text{ CO}_2 = \pm .5\%$

Cal Volts = Cal Volt Conc - Std Conc =  $\pm$  Conc Diff =  $\pm \Delta\%$

$.846 = 21.133 - 21.100 = .033 = .132$

$.248 = 6.195 - 6.240 = -.045 = -.180$









**CO ANALYZER  
MULTIPOINT CALIBRATION REPORT FORM**

Date: 3-31-2000  
 Analyzer: Make: HORIBA Model: PIR 2000 SN: 408005  
 Calibration by: G Wadlington  
 Cal Gas Flow: 1.5 SCFH Measured by: Rotameter  
 BP: 30.50 Instrument ID: PRINCO  
 Temp: 76 Instrument ID: TR  
 Analyzer last calibrated: \_\_\_\_\_ By: \_\_\_\_\_

**Cylinders:**

1. # TX 79373 Concentration: 00.00 % CO Cyl. Press.: 960 PSI  
 Certified by: Air Liquide Date: 9-22-98
2. # CC 52330 Concentration: 4.75 % CO Cyl. Press.: 1750 PSI  
 Certified by: Air Liquide Date: 2-10-2000
3. # CC 55904 Concentration: 8.60 % CO Cyl. Press.: 1610 PSI  
 Certified by: Air Liquide Date: 2-14-2000
4. # AAL 21084 Concentration: 2.01 % CO Cyl. Press.: 1320 PSI  
 Certified by: Scott Specialty Gases Date: 5-15-97

Analyzer: **Calibrated Range:** 0-10.0 % **Output:** 0-1.0 V.  
**Flow:** 1.5 SCFH **Measured by:** Rotameter

**Calibration Results**

| Point # | CYL. # | % CO | EXPECTED |      | ACTUAL |      | ADJ.  |      | % DIF. | ROTENTIOMETER |      |
|---------|--------|------|----------|------|--------|------|-------|------|--------|---------------|------|
|         |        |      | METER    | DVM  | METER  | DVM  | METER | DVM  |        | UNADJ.        | ADJ. |
| 1       | 1      | 0.00 | 0.00     | .000 | 0.00   | .000 | —     | —    |        |               |      |
| 2       | 2      | 4.75 | 47.5     | .475 | 49.1   | .491 | 47.5  | .475 |        |               |      |
| 3       | 3      | 8.60 | 86.0     | .860 | 86.0   | .860 | —     | —    |        |               |      |
| 4       | 4      | 2.01 | 20.1     | .201 | 20.0   | .200 | —     | —    |        |               |      |
| 5       | 1      | 0.00 | 0.00     | .000 | 0.00   | .000 | —     | —    |        |               |      |

.5 = 5.002



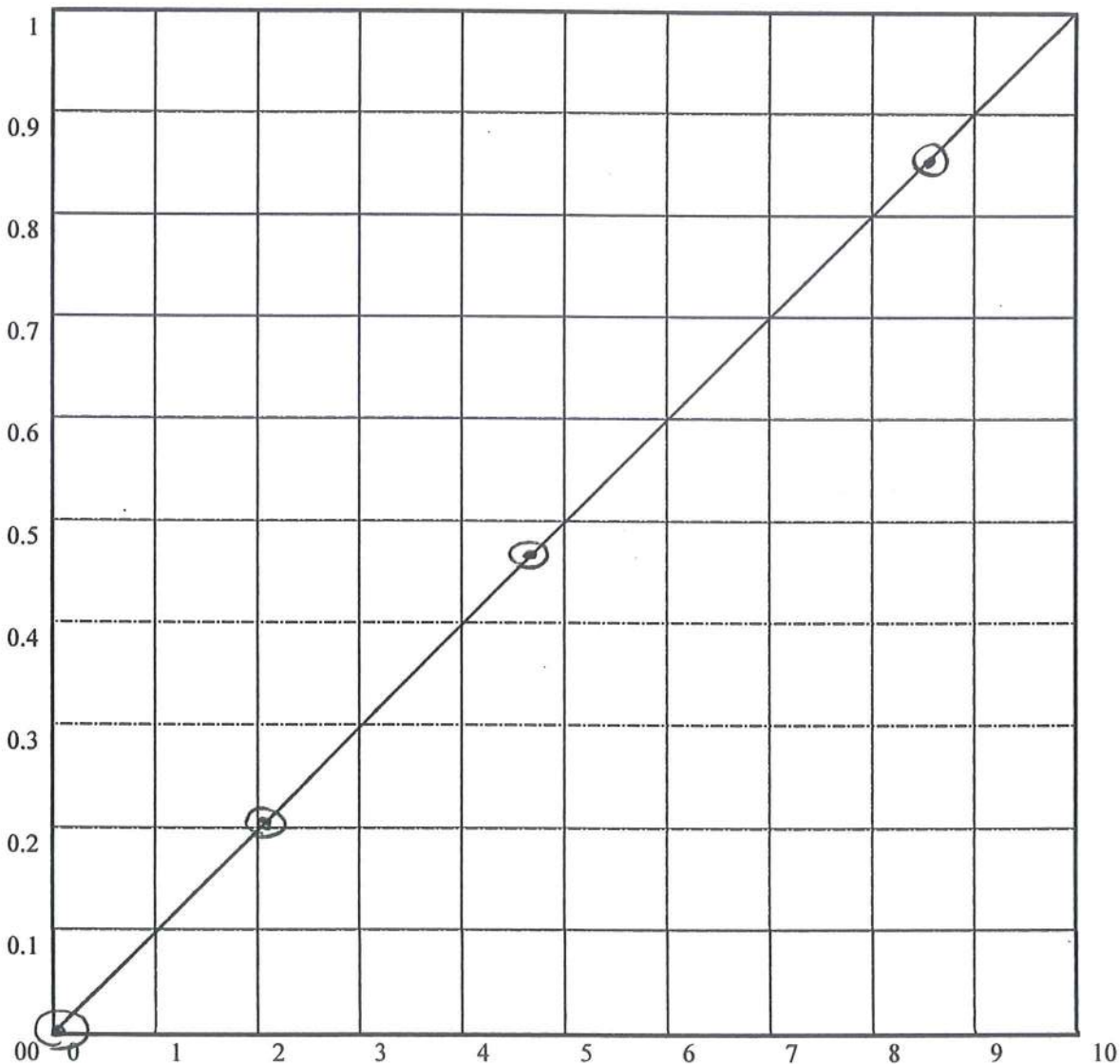
### CO Linear Regression Results:

$$Y = MX + B$$
$$\text{Slope (M)} = \underline{-,0004190}$$

$$\text{Y Intercept (B)} = \underline{,1000440}$$

$$\text{Correlation Coefficient (r)} = \underline{,9999992}$$

$$r^2 = \underline{,9999984}$$



EPA Span Value =  $\pm 2.0\%$  of 10% CO =  $\pm .2\%$

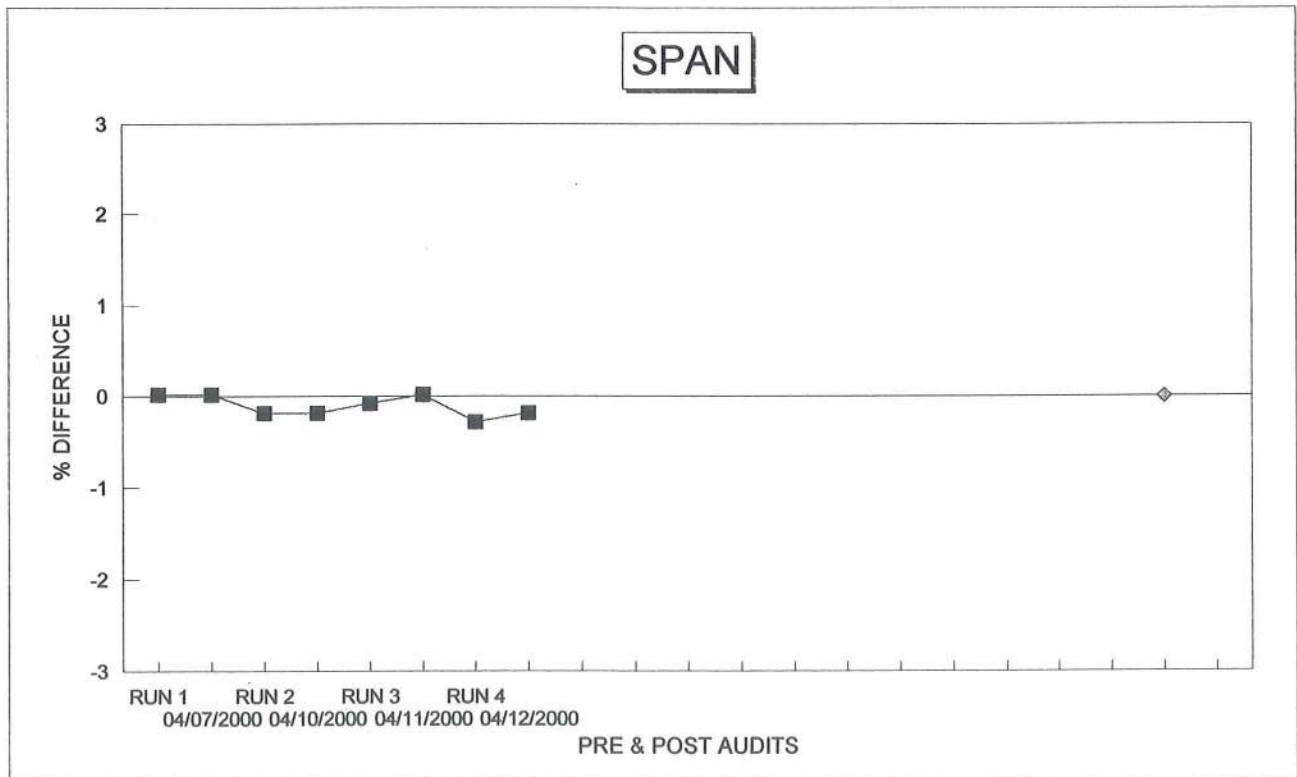
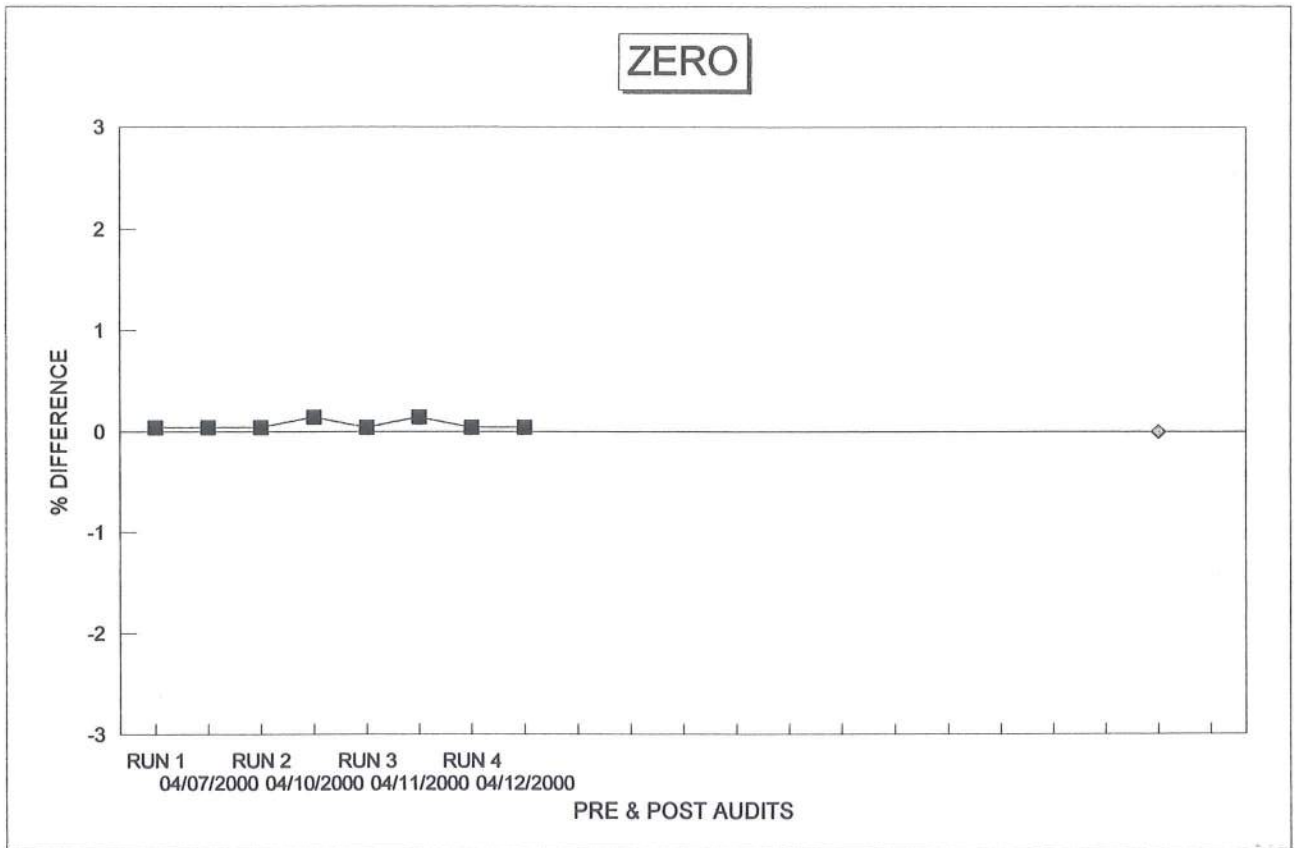
Cal Volts = Cal Volt Conc - Std Conc =  $\pm$  Conc Diff =  $\pm \Delta\%$

$$.860 = 8.600 - 8.600 = 0 = \phi$$

$$.200 = 2.000 - 2.010 = -.010 = -.100$$









**SO<sub>2</sub> ANALYZER  
MULTIPOINT CALIBRATION REPORT FORM**

Date: 3-31-2000

Analyzer: Make: HORIBA Model: PIR 2000 SN: 403019

Calibration by: C. Wadington

Cal Gas Flow: 1.5 SCFH

Measured by: Rotameter

BP: 30.50

Instrument ID: PRINCO

Temp: 76

Instrument ID: TR

Analyzer last calibrated: \_\_\_\_\_ By: \_\_\_\_\_

Cylinders:

1. # TX 79373 Concentration: 00.00 % SO<sub>2</sub> Cyl. Press.: 960 PSI  
 Certified by: Air Liquide Date: 9-22-98
2. # CC 67475 Concentration: 1260 % SO<sub>2</sub> Cyl. Press.: 650 PSI  
 Certified by: Air Liquide Date: 9-22-98
3. # ALMO 49127 Concentration: 1770 % SO<sub>2</sub> Cyl. Press.: 1150 PSI  
 Certified by: Scott Specialty Gases Date: 5-15-97
4. # ALMO 52285 Concentration: 506 % SO<sub>2</sub> Cyl. Press.: 1000 PSI  
 Certified by: Scott Specialty Gases Date: 5-15-97

Analyzer: **Calibrated Range:** 0-2500 PPM  
**Flow:** 1.5 SCFH

**Output:** 0-1.0 V.  
**Measured by:** Rotameter

**Calibration Results**

| Point # | CYL. # | PPM SO <sub>2</sub> | EXPECTED |      | ACTUAL |      | ADJ.  |      | % DIF. | POTENTIOMETER |      |
|---------|--------|---------------------|----------|------|--------|------|-------|------|--------|---------------|------|
|         |        |                     | METER    | DVM  | METER  | DVM  | METER | DVM  |        | UNADJ.        | ADJ. |
| 1       | 1      | 0.00                | 0.00     | .000 | 00.0   | .000 | —     | —    |        |               |      |
| 2       | 2      | 1260                | 50.4     | .504 | 50.8   | .508 | 50.4  | .504 |        |               |      |
| 3       | 3      | 1770                | 70.8     | .708 | 71.2   | .712 | —     | —    |        |               |      |
| 4       | 4      | 506                 | 20.2     | .202 | 19.2   | .192 | —     | —    |        |               |      |
| 5       | 1      | 0.00                | 0.00     | .000 | 0.00   | .000 | —     | —    |        |               |      |

.5 = 1250.200



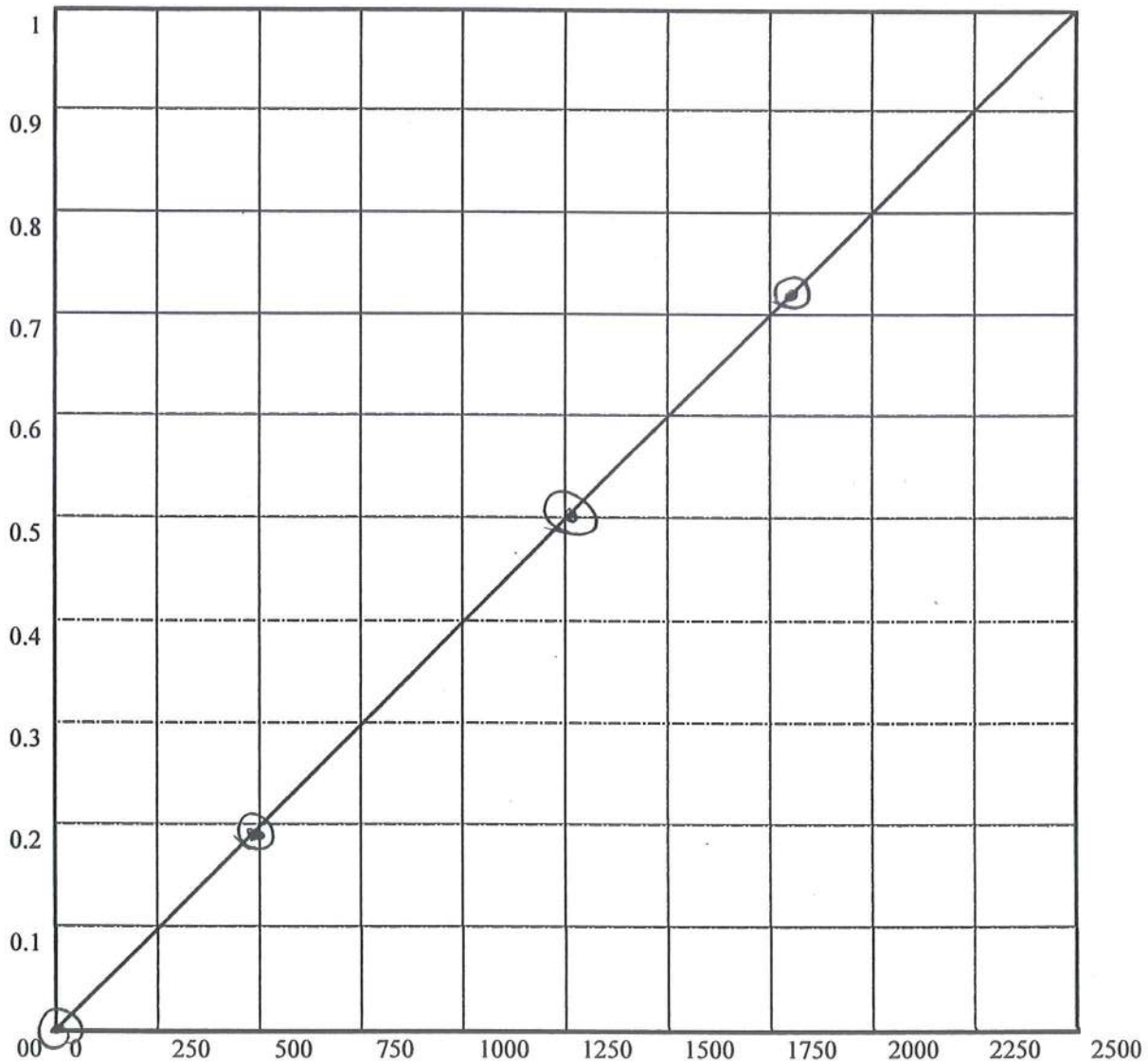
**SO<sub>2</sub> Linear Regression Results:**

$Y = MX + B$   
 Slope (M) = - .0051706

Y Intercept (B) = .0004040

Correlation Coefficient (r) = .9998615

$r^2 =$  .9997229



EPA Span Value =  $\pm 2.0\%$  of 2500 PPM SO<sub>2</sub> =  $\pm 50$  PPM

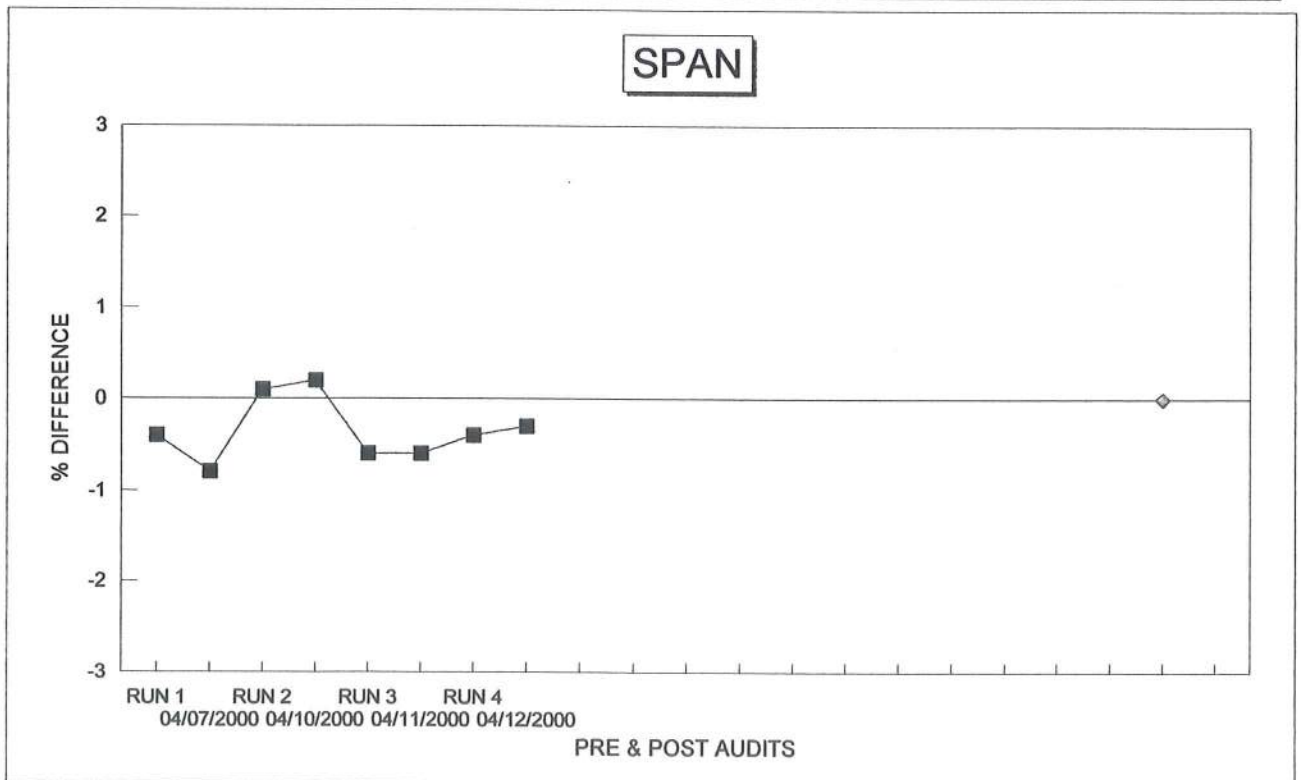
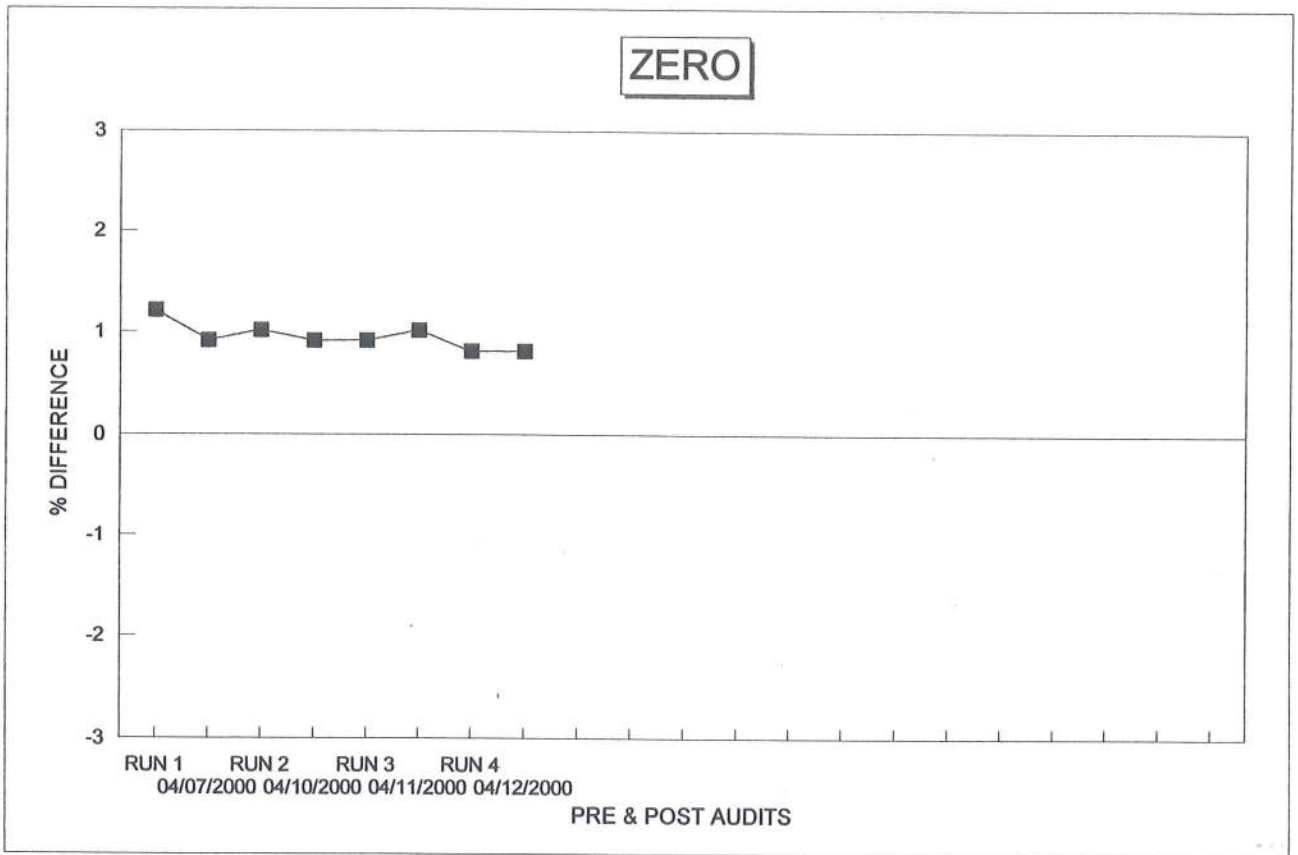
Cal Volts = Cal Volt Conc - Std Conc =  $\pm$  Conc Diff =  $\pm \Delta \%$

$.712 = 1780.000 - 1770.0 = 10.000 = .400$

$.192 = 480.000 - 506.0 = -26.000 = -1.04$











# Scott Specialty Gases

Shipped  
From:

500 WEAVER PARK RD  
LONGMONT CO 80501  
Phone: 303-442-4700

Fax: 303-772-7673

## CERTIFICATE OF ANALYSIS

ENERGY & ENV MEASUREMENT

PROJECT #: 08-34135-005

PO#: VERBAL

C/O ED WADINGTON  
3730 N. PELLEGRINO DR.  
TUCSON

AZ 85749

ITEM #: 08024520 4AL

DATE: 4/24/97

CYLINDER #: AAL21084

ANALYTICAL ACCURACY: +/-2%

FILL PRESSURE: 2015 PSIA

PRODUCT EXPIRATION: 4/24/2000

BLEND TYPE : CERTIFIED MASTER GAS

**COMPONENT**

**REQUESTED GAS**

**ANALYSIS**

CARBON DIOXIDE  
CARBON MONOXIDE  
OXYGEN  
NITROGEN

CONC MOLES

(MOLES)

6.25 %  
2. %  
6.25 %  
BALANCE

6.25 %  
2.01 %  
6.24 %  
BALANCE

CBA 590

2015 PSIA

ANALYST:

*Diana Beehler*  
DIANA BEEHLER







**AIR LIQUIDE**

1451 THORNE RD.  
TACOMA, WA 98421  
TEL: (253) 383-3637

THE ONLY LIABILITY OF THIS  
COMPANY FOR GAS WHICH FAILS TO  
COMPLY WITH THE ANALYSIS SHALL  
BE REPLACEMENT THEREOF BY THE  
COMPANY WITHOUT EXTRA COST.

**DO NOT REMOVE  
THIS TAG**

**AIR LIQUIDE**

**GASES FOR RESEARCH AND DEVELOPMENT**

CYL # QC52330 CGA 590

PRES 1650 VOL 150 CF

TEST # 04100 DATE 02-10-00

Analytical Method GC + Paramagnetic

|                 | Requested    | Analyzed      |
|-----------------|--------------|---------------|
| Hydrogen        |              |               |
| Nitrogen        | <u>bal.</u>  | <u>bal.</u>   |
| Argon           |              |               |
| Air             |              |               |
| Carbon Monoxide | <u>5%</u>    | <u>4.75%</u>  |
| Methane         |              |               |
| Oxygen          | <u>12.5%</u> | <u>12.69%</u> |
| Helium          |              |               |
| Carbon Dioxide  | <u>12.5%</u> | <u>12.79%</u> |
|                 |              |               |
|                 |              |               |
|                 |              |               |

mb  
SIGNED











# Scott Specialty Gases

500 WEAVER PARK RD, LONGMONT, CO 80501

Phone: 303-442-4700

Fax: 303-772-7673

## CERTIFICATE OF ANALYSIS: Interference-Free™ Multi-Component EPA Protocol Gas

**Customer**  
ENERGY & ENV MEASUREMENT

**Assay Laboratory**  
SCOTT SPECIALTY GASES  
500 WEAVER PARK RD  
LONGMONT, CO 80501

**Project No.:** 08-34135-001  
**P.O. No.:** VERBAL

C/O ED WADINGTON  
3730 N. PELLEGRINO DR.  
TUCSON, AZ 85749

### ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards; Procedure #G1; September, 1993.

**Cylinder Number:** ALM052285      **Certification Date:** 4/21/97      **Exp. Date:** 4/21/2000  
**Cylinder Pressure\*\*\*:** 1996 PSIG

### COMPONENT

SULFUR DIOXIDE \*  
NITROGEN

**CERTIFIED CONCENTRATION**

506 PPM  
BALANCE

**ANALYTICAL ACCURACY**

+/- 1% NIST Traceable

Do not use when cylinder pressure is below 150 psig.

Analytical accuracy is inclusive of usual known error sources which at least include precision of the measurement processes.

Product certified as +/- 1% analytical accuracy is directly traceable to NIST standards.

This Protocol has been certified using corrected NIST SO2 standard values, per EPA guidance dated 7/24/86 and will not correlate with uncorrected protocols.

### REFERENCE STANDARD

| TYPE/BRM NO. | EXPIRATION DATE | CYLINDER NUMBER | CONCENTRATION | COMPONENT |
|--------------|-----------------|-----------------|---------------|-----------|
| NTRM 1881    | 9/27/98         | ALM059505       | 488.5 PPM     | SO2/N2    |

### INSTRUMENTATION

**INSTRUMENT/MODEL/SERIAL#**  
FTIR System/8220/AA89400251

**LAST DATE CALIBRATED**

03/20/97

**ANALYTICAL PRINCIPLE**

Scott Enhanced FTIR

### ANALYZER READINGS

(Z = Zero Gas    R = Reference Gas    T = Test Gas    r = Correlation Coefficient)

First Triad Analysis

Second Triad Analysis

Calibration Curve

### SULFUR DIOXIDE \*

| Date: 04/14/97      | Response Unit: PPM         |
|---------------------|----------------------------|
| Z1 = 0.3847         | R1 = 487.72    T1 = 505.77 |
| R2 = 488.78         | Z2 = 1.8201    T2 = 505.88 |
| Z3 = 1.8428         | T3 = 505.78    R3 = 488.89 |
| Avg. Concentration: | 505.8 PPM                  |

| Date: 04/21/97      | Response Unit: PPM         |
|---------------------|----------------------------|
| Z1 = 0.3241         | R1 = 488.29    T1 = 505.43 |
| R2 = 488.83         | Z2 = 1.8088    T2 = 505.75 |
| Z3 = 0.5340         | T3 = 505.74    R3 = 488.68 |
| Avg. Concentration: | 505.8 PPM                  |

| Concentration = A + Bx + Cx2 + Dx3 + Ex4 |                              |
|--|------------------------------|
| r = 0.999990                             |                              |
| Constants:                               | A = 0.000000                 |
|  | B = 1.000000    C = 0.000000 |
|  | D = 0.000000    E = 0.000000 |

Special Notes:

ANALYST:

*Devon VonFeldt*  
Devon VonFeldt







# CERTIFICATE of ANALYSIS

## Interference-Free Multi-Component EPA Protocol Gases

|                                    |                                     |                                   |                          |                                   |                               |
|------------------------------------|-------------------------------------|-----------------------------------|--------------------------|-----------------------------------|-------------------------------|
| <b>Cyl. Number:</b><br>CC67475     | <b>Cyl. Pressure:*</b><br>1900 psig | <b>Lot Number:</b><br>N.A.        | <b>COMPONENT</b><br>Name | <b>REQUESTED</b><br>Concentration | <b>ASSAY</b><br>Concentration |
| <b>Assay Date:</b><br>04/02/98     | <b>Expiration Date:</b><br>04/01/01 | <b>Document Number:</b><br>881463 | Sulfur Dioxide           | 1250 ppm                          | 1260 ± 11 ppm                 |
| <b>Customer:</b><br>AL COMPRESSED  | <b>P.O. Number:</b><br>031798CS     | <b>Item Number:</b><br>N.A.       | Nitrogen                 | Balance                           | Balance                       |
| *Mixture is valid only to 150 psig |                                     |                                   |                          |                                   |                               |

|  |   |              |              |                   |              |                |                 |                  |                   |
|--|---|--------------|--------------|-------------------|--------------|----------------|-----------------|------------------|-------------------|
| <b>EPA Protocol, Section No. 2.2,</b><br><b>Procedure: G-1</b> | <b>REFERENCE STANDARD EMPLOYED FOR ANALYSIS</b> |              |              |                   |              |                |                 |                  |                   |
| <b>Analyst:</b><br>WR  | <b>Std name</b>                                 | <b>Conc.</b> | <b>Units</b> | <b>Std. Error</b> | <b>Comp.</b> | <b>Balance</b> | <b>Cyl. No.</b> | <b>Exp. Date</b> | <b>Sample No.</b> |
| <b>Calculated by:</b><br>WR                                    | 82745x  | 500.0        | ppm          | 4.9               | SO2          | N2             | CC63100         | 09/27/98         | 97080209          |
| <b>Approved by:</b><br>WR                                      | GMIS22  | 1510.0       | ppm          | 13.0              | SO2          | N2             | CC10208         | 07/25/99         | N.A.              |

|                              |             |
|------------------------------|-------------|
| <b>COMPONENT 1</b>           |             |
| <b>GAS ANALYZER EMPLOYED</b> |             |
| <b>Manufacturer:</b>         | KVB/ANALECT |
| <b>Model Number:</b>         | EN3024      |
| <b>Serial Number:</b>        | 3024        |
| <b>MPR Last Calibrated:</b>  | 03/18/98    |
| <b>Analytical Principle:</b> | FTIR        |

| 3/26/98                        | Trial 1 | Trial 2 | Trial 3 | Units      | 4/2/98                         | Trial 4 | Trial 5 | Trial 6 | Units      |
|--------------------------------|---------|---------|---------|------------|--------------------------------|---------|---------|---------|------------|
| Zero                           | 0.3     | 0.4     | 0.4     | VDC        | Zero                           | 0.0     | 0.1     | 0.0     | VDC        |
| Reference#1                    | 493.7   | 496.0   | 488.3   | VDC        | Reference#1                    | 496.6   | 494.8   | 490.5   | VDC        |
| Reference#2                    | 1476.8  | 1483.5  | 1478.1  | VDC        | Reference#2                    | 1487.6  | 1480.7  | 1482.0  | VDC        |
| Candidate                      | 1241.2  | 1231.4  | 1239.9  | VDC        | Candidate                      | 1238.4  | 1233.9  | 1237.1  | VDC        |
| Result                         | 1266.1  | 1256.1  | 1264.7  | ppm        | Result                         | 1263.2  | 1258.7  | 1261.9  | ppm        |
| <b>MEAN ANALYTICAL RESULT:</b> |         |         |         | 1262.3 ppm | <b>MEAN ANALYTICAL RESULT:</b> |         |         |         | 1261.3 ppm |

Analytical uncertainty and NIST traceability are in compliance with EPA-600/R-97/121

|                 |                       |                     |
|-----------------|-----------------------|---------------------|
| <b>Analyst:</b> | <b>Calculated by:</b> | <b>Approved by:</b> |
|                 |                       |                     |

AIR LIQUIDE AMERICA CORPORATION

11426 Fairmont Parkway • La Porte, TX 77571-6000 • 800/248-1427 • 281/474-8400 • Fax: 281/474-8419





# Scott Specialty Gases

500 WEAVER PARK RD, LONGMONT, CO 80501

Phone: 303-442-4700

Fax: 303-772-7873

## CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS

### Customer

ENERGY & ENV MEASUREMENT

C/O ED WADINGTON  
3730 N. PELLEGRINO DR.  
TUCSON, AZ 85749

### Assay Laboratory

SCOTT SPECIALTY GASES  
500 WEAVER PARK RD  
LONGMONT, CO 80501

Project No.: 08-34135-003

P.O. No.: VERBAL

### ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards; Procedure #G1; September, 1993.

Cylinder Number: ALM049127  
Cylinder Pressure\*\*\*: 1860 PSIG

Certification Date: 4/21/97

Exp. Date: 4/21/2000

### COMPONENT

SULFUR DIOXIDE \*  
NITROGEN

### CERTIFIED CONCENTRATION

1,770 PPM  
BALANCE

ANALYTICAL ACCURACY\*\*  
+/- 1% NIST TRACEABLE

\*\*\* Do not use when cylinder pressure is below 150 psig.

\*\* Analytical accuracy is inclusive of usual known error sources which at least include precision of the measurement processes.

Product certified as +/- 1% analytical accuracy is directly traceable to NIST standards.

\* This Protocol has been certified using corrected NIST SO2 standard values, per EPA guidance dated 7/24/96 and will not correlate with uncorrected Protocols.

### REFERENCE STANDARD

| TYPE/SRM NO. | EXPIRATION DATE | CYLINDER NUMBER | CONCENTRATION | COMPONENT      |
|--------------|-----------------|-----------------|---------------|----------------|
| NTRM-R-1696  | 7/03/98         | ALM057797       | 3131. PPM     | SULFUR DIOXIDE |

### INSTRUMENTATION

#### INSTRUMENT/MODEL/SERIAL#

FTIR System/8220/AAB9400261

#### LAST DATE CALIBRATED

03/20/97

#### ANALYTICAL PRINCIPLE

Scott Enhanced FTIR

### ANALYZER READINGS

(Z = Zero Gas R = Reference Gas T = Test Gas r = Correlation Coefficient)

First Triad Analysis

Second Triad Analysis

Calibration Curve

#### SULFUR DIOXIDE \*

| Date: 04/14/97      | Response Unit: PPM |             |  |
|---------------------|--------------------|-------------|--|
| Z1 = 0.7210         | R1 = 3127.7        | T1 = 1767.1 |  |
| R2 = 3131.7         | Z2 = 4.6770        | T2 = 1768.1 |  |
| Z3 = 4.6770         | T3 = 1768.1        | R3 = 3133.7 |  |
| Avg. Concentration: | 1768.              | PPM         |  |

| Date: 04/21/97      | Response Unit: PPM |             |  |
|---------------------|--------------------|-------------|--|
| Z1 = 0.4020         | R1 = 3125.8        | T1 = 1770.2 |  |
| R2 = 3132.3         | Z2 = 6.8540        | T2 = 1769.3 |  |
| Z3 = 4.9410         | T3 = 1770.9        | R3 = 3134.9 |  |
| Avg. Concentration: | 1770.              | PPM         |  |

| Concentration = A + Bx + Cx2 + Dx3 + Ex4 |             |
|--|-------------|
| r = 0.999990                             | 1696        |
| Constants:                               | A = 0.00000 |
| B = 1.00000                              | C = 0.00000 |
| D = 0.00000                              | E = 0.00000 |

Special Notes:

ANALYST:

*Devon VonFeldt*  
DEVON VONFELDT





# Certificate of Analysis

## ANALYTICAL CONTROL LABORATORY ANALYSIS

### ACETONE - OPTIMA

Catalog No.: A-929

January 13, 1997

Lot No.: 972630

This is to certify that this lot was tested and found to comply with the specifications for this product. The following are the actual analytical results obtained:

#### TESTS

Aldehyde  
Assay  
Color  
Density (g/mL) at 25°C  
Description  
Fluorescence Background  
(as Quinine Sulfate)  
Identification  
Isopropyl Alcohol  
Methanol  
Optical Absorbance at 350nm  
                                  at 340nm  
                                  at 330nm  
Pesticide Residue Analysis  
(as Heptachlor Epoxide)  
Refractive Index at 25°C  
Residue after Evaporation  
Solubility in Water  
Substances Reducing Permanganate  
Titratable Acid  
Titratable Base  
Water (H<sub>2</sub>O)

#### ACTUAL ANALYSIS

0.0005%  
99.6%  
5 APHA  
0.7851  
Clear, Colorless Liquid  
Not More Than 1 PPB  
Pass Test  
0.01%  
0.03%  
0.001  
0.05  
0.69  
Not More Than 10 ng/L  
1.3560  
0.3 PPM  
Pass Test  
Pass Test  
0.0003 Meq/g.  
0.0001 Meq/g.  
0.4%

Approved By:

*Robert Dowd*

Robert Dowd  
Q.C. Laboratory Manager

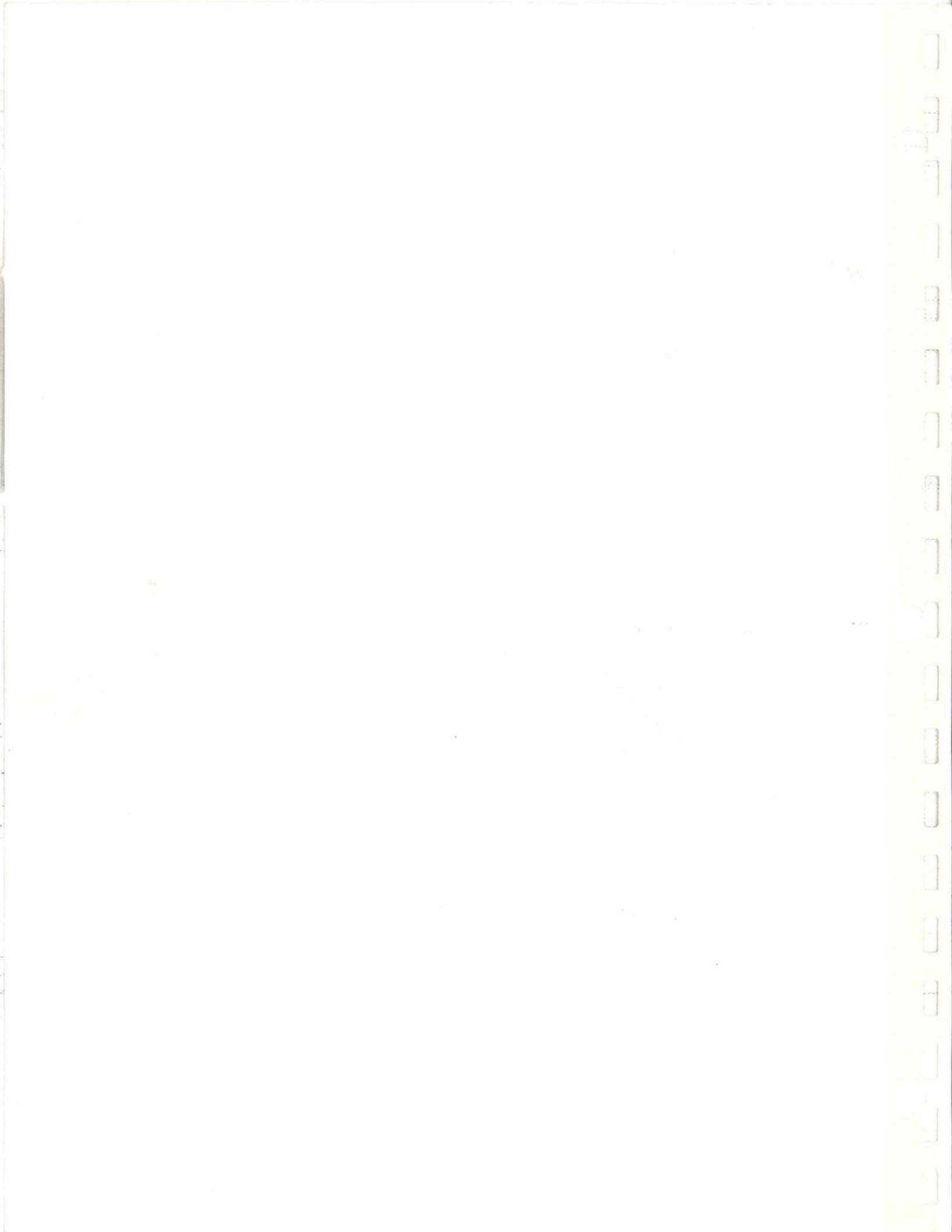


Fisher  
Scientific

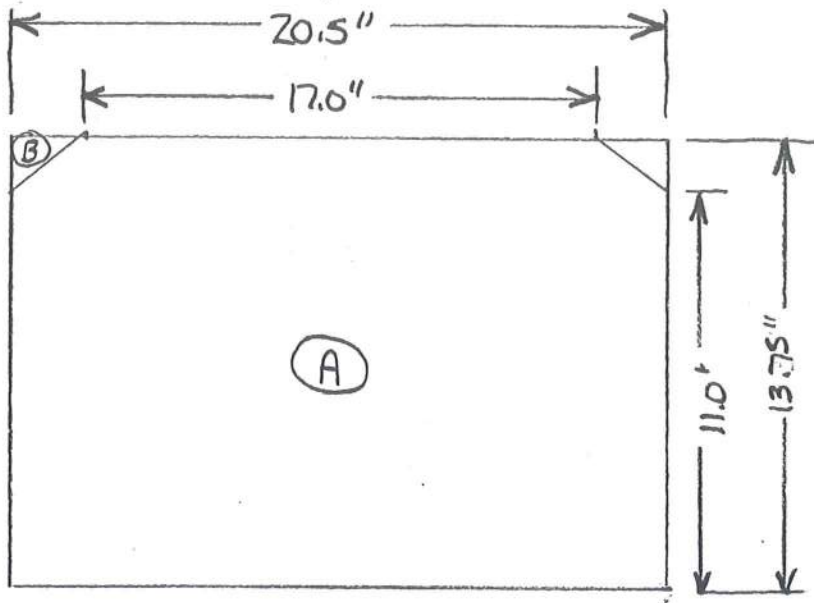
Chemical Division  
1 Reagent Lane  
Fair Lawn, N.J. 07410  
(201) 796-7100







# Jotul F400 Volume and Fuel Load Calculations

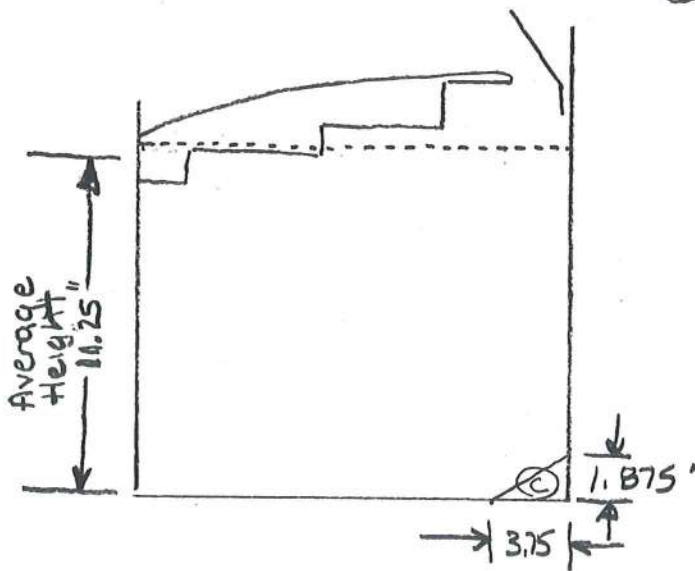


$$\begin{aligned}
 A &= 13.75 \times 20.5 \times 11.25 = 3171.094 \\
 (-2x) \quad B &= .5(9 \times 1.75 \times 2.5) = 19.688 \\
 - C &= .5(3.75 \times 1.875 \times 20.5) = 72.070
 \end{aligned}$$

$$3059.648$$

$$\div 1728.000$$

$$\text{Volume in ft}^3 = 1.771$$



Fuel Load

| Low  | Ideal  | High |
|------|--------|------|
| 11.2 | 12.394 | 13.6 |





Jotul North America  
400 Riverside Street  
Portland, ME 04104

4/5/2000

Chip Wadington  
LoKee Testing Laboratory  
13235 Prairie Circle East  
Sumner, WA 98390

**RE: Air Settings for the F400**

Dear Chip,

Here are the air settings for the F400. These are approximate.

|          |                              |
|----------|------------------------------|
| Low      | 0"- . 1"                     |
| Med-low  | . 1"- . 2"                   |
| Med high | . 2"- . 5" (possibly higher) |
| High     | Wide open                    |

These measurements are made across the slider gap (opening). I suggest measuring these against the control rod for reference.

Thanks,

Roger Purinton

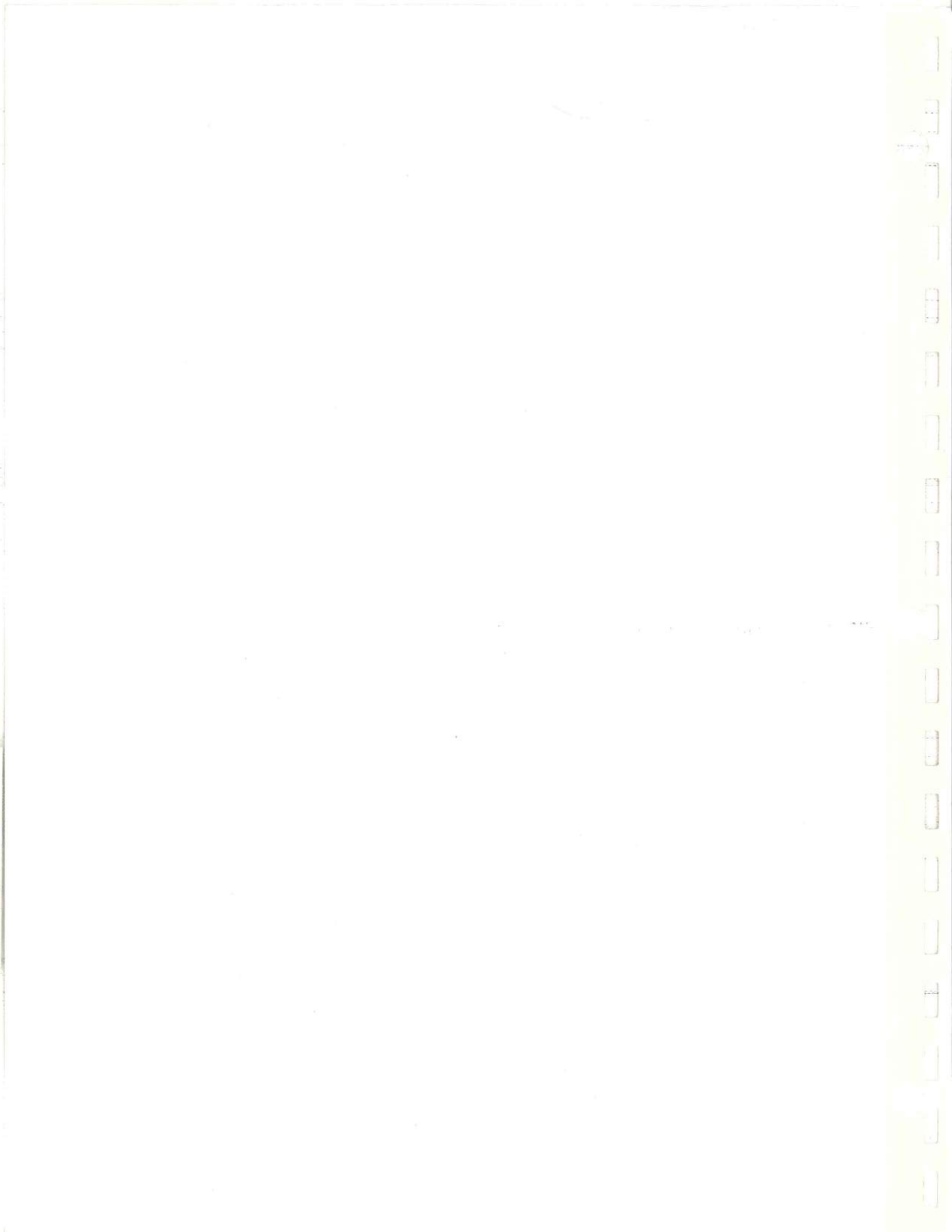




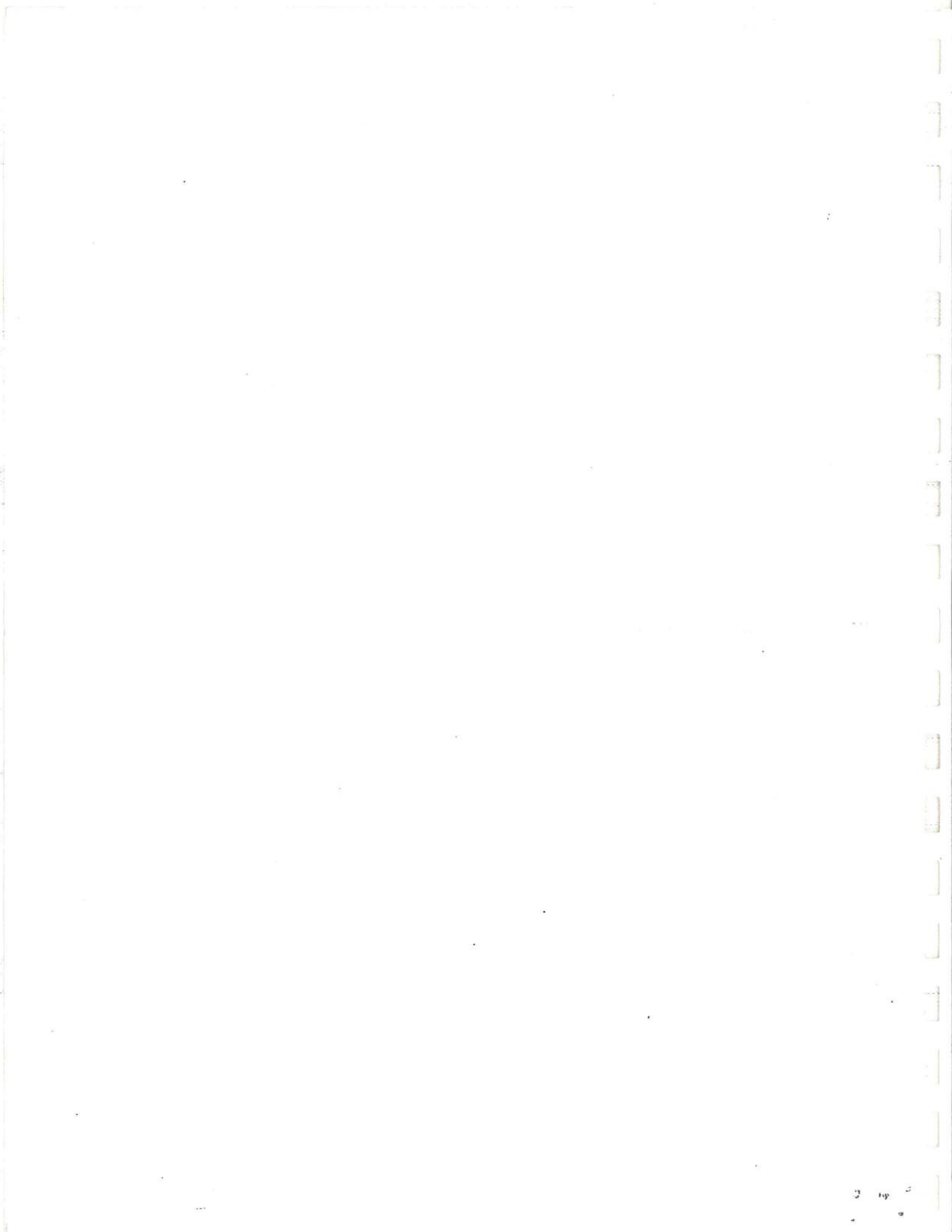
















# PARTS LIST FOR THE F 400 CASTINE WOODSTOVE

CONSULT YOUR DEALER FOR PART NUMBERS AND  
REPLACEMENT PARTS.

|    |                              |
|----|------------------------------|
| 1  | ASHLIP                       |
| 2  | LEFT DOOR                    |
| 3  | RIGHT DOOR                   |
| 4  | RIGHT SIDE PANEL             |
| 5  | FRONT PANEL                  |
| 6  | TOP CASTING                  |
| 7  | UPPER BACK PANEL             |
| 8  | SMOKE OUTLET                 |
| 9  | BACK PANEL                   |
| 10 | LEFT SIDE PANEL              |
| 11 | LEG (long leg)               |
| 12 | UPPER BOTTOM PANEL           |
| 13 | FRONT DOOR SHAFT (exterior)  |
|    | LATCH                        |
|    | NUT                          |
|    | SPRING                       |
| 14 | RIGHT BURN PLATE             |
| 15 | RIGHT GLASS PANEL            |
| 16 | LEFT GLASS PANEL             |
| 17 | AIR WASH MANIFOLD            |
| 18 | TOP BAFFLE (stainless steel) |
| 19 | BAFFLE COVER (cast iron)     |
| 20 | AIR INSPECTION COVER         |
| 21 | REAR BURN PLATE              |
| 22 | FIRE BRICK (3)               |
| 23 | BOTTOM GRATE                 |
| 24 | LEFT BURN PLATE              |
| 25 | LOWER BOTTOM PANEL           |
| 26 | ASHPAN HOUSING               |
| *  | ASHPAN                       |
| 27 | AIR SLIDER VALVE             |
| 28 | AIR DEVIDER                  |
| 29 | DOOR PINS                    |
| 30 | AIR CONTROL LEVER (chrome)   |
| 31 | ALLEN HEAD SCREW             |
| 31 | ASHPAN DOOR                  |
| *  | ASHPAN DOOR PIN              |
| 32 | ASH DOOR HANDLE              |
|    | LOOP HANDLE                  |
|    | SET SCREW                    |
|    | LATCH                        |
|    | SPRING                       |
|    | NUT                          |
| *  | NOT SHOWN                    |

## APPENDIX A:

### ALTERNATE FLOOR PROTECTION

All floor protection materials must be non-combustible i.e. metal, brick, stone, mineral fiber boards). Any combustible material may not be used.

The easiest means of determining if a proposed alternate floor material meets requirements listed in this manual is to follow this procedure.

R-value = thermal resistance  
k-value = thermal conductivity  
C-value = thermal conductance

- Convert the specification to R-value;
  - If R-value is given, no conversion is needed.
  - If k-value is given with a required thickness (T) in inches:  $R=1/k \times T$ .
  - If C-value is given:  $R=1/C$ .

- Determine the R-value of the proposed alternate floor protector.
  - Use the formula in Step 1 to convert values not expressed as "R".
  - For multiple layers, add R-values of each layer to determine overall R-value.
  - If the overall R-value of the system is greater than the R-value of the specified floor protector, the alternate is acceptable.

### EXAMPLE:

The specified floor protector should be 3/4" thick material with a k-factor of 0.84. The proposed alternate is 4" brick with a C-factor of 1.25 over

1/8" mineral board with a k-factor of 0.29.

Step A. Use formula above to convert specifications to R-value.  
 $R=1/k \times T = 1/.84 \times .75 = .893$

Step B. Calculate R of proposed system.  
 4" brick of C-1.25, therefore  
 $R \text{ brick} = 1/C = 1/1.25 = 0.80$   
 1/8" mineral board of  $k = 0.29$  therefore  
 $R \text{ mineral board} = 1/.29 \times 0.125 = 0.431$   
 Total  $R = R \text{ brick} + R \text{ mineral board} = 0.8 + 0.431 = 1.231$

Step C. Compare proposed system  $R = 1.231$  to specified R of 0.893. Since R is greater than required, the system is acceptable.

### Definitions:

Thermal conductance =  $C = \frac{B_{tu}}{(hr)(ft^2)(F)} = \frac{W}{(m^2)(K)}$

Thermal conductivity =  $k = \frac{B_{tu}}{(hr)(ft^2)(F)} = \frac{W}{(m^2)(K)}$

Thermal resistance =  $R = \frac{B_{tu}}{(hr)(ft^2)(F)} = \frac{W}{(m^2)(K)}$

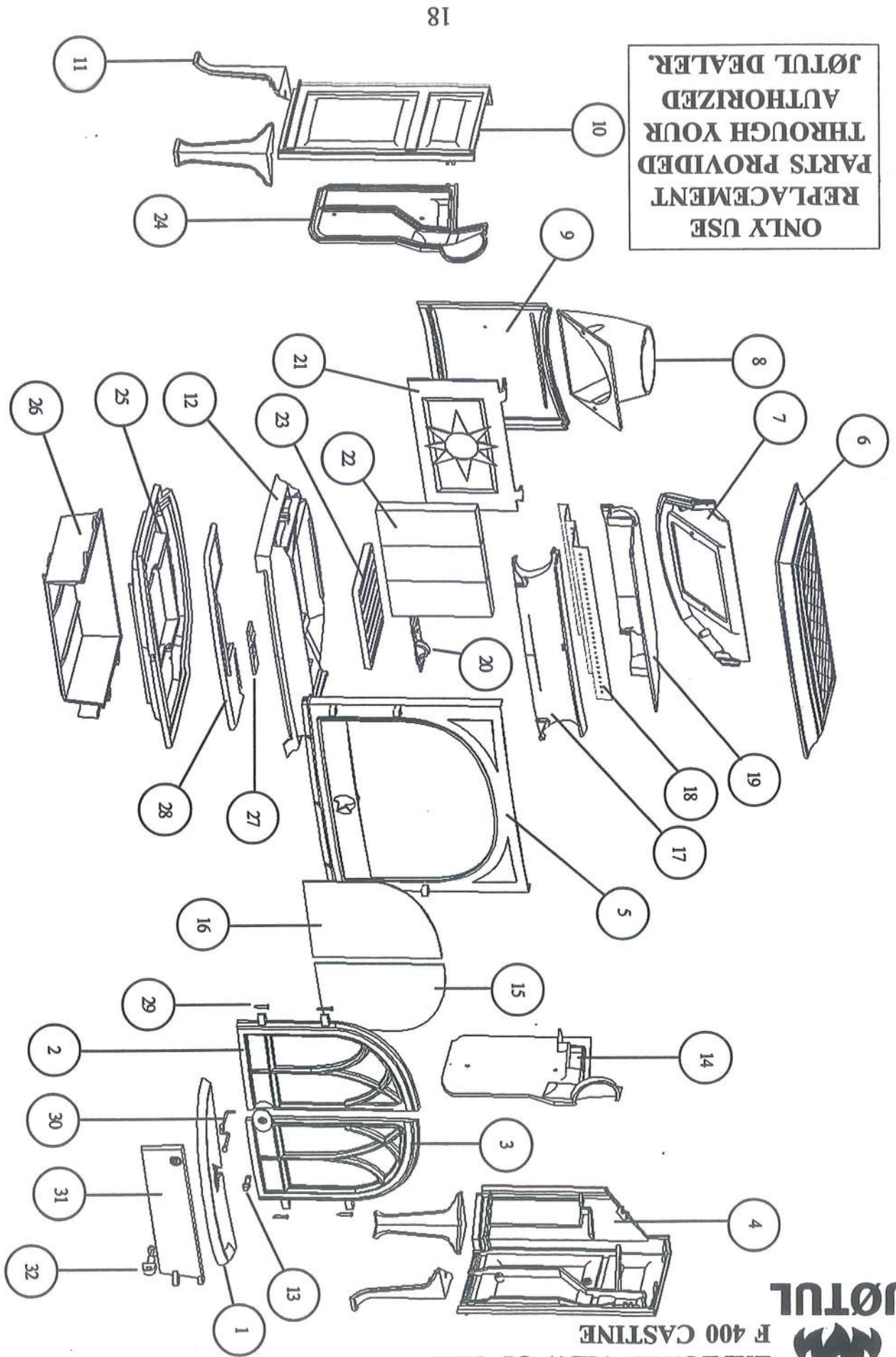
$R = \frac{B_{tu}}{(hr)(ft^2)(F)} = \frac{W}{(m^2)(K)}$

THE JOTUL F 400 CASTINE WOODSTOVE REQUIRES FLOOR PROTECTION WITH A MINIMUM INSULATING R VALUE OF 0.5.

ALCOVE INSTALLATION REQUIRE A MINIMUM R VALUE OF 1.6. (IF A UL/ULC OR WHI LISTED HEARTH PAD IS NOT USED.)



EXPLODED VIEW OF THE  
F 400 CASTINE



ONLY USE  
REPLACEMENT  
PARTS PROVIDED  
THROUGH YOUR  
AUTHORIZED  
JØTUL DEALER.





Jøtul recommends the use of a magnetic stove-top thermometer to monitor the surface temperature of the stove. The optimum surface temperature range for the most efficient, clean burn is between 400° and 600°.

**Stove-Top Thermometer (part # 5002)**

NO OTHER TYPE OF HEATSHIELD MAY BE USED ON THE BOTTOM OF THE F 400 Castine. If these or other indications suggest that infiltration air is inadequate, additional combustion air should be provided from the outdoors. Outside combustion air can be provided to the appliance by the following means:

**Bottom Heatshield (part # 154384)**

NO OTHER TYPE OF HEATSHIELD MAY BE USED ON THE REAR OF THE F 400 Castine. A stove rear heatshield has been specifically designed for the F 400 Castine to reduce clearances off the rear of the stove to combustible materials. Use of the heatshield DOES NOT affect the clearance off the sides of the appliance. See pages 11-12 for specific clearance requirements. Complete installation instructions are supplied with the heatshield.

**Rear Heatshield (part # 154385)**

Use of the Floor Bracket Kit is required in all mobile home installations to secure the stove to the floor. Complete installation instructions and diagrams are supplied with each Floor Bracket Kit.

**Floor Bracket Kit (part #750304)**

Use of the Floor Bracket Kit is required in all mobile home installations to secure the stove to the floor. Complete installation instructions and diagrams are supplied with each Floor Bracket Kit.

3. A mechanical ventilation system: if the house has a ventilation system (air change or heat recovery):  
 a. the ventilation system may be able to provide sufficient combustion make-up air for the solid-fuel fired appliance.  
 b. the homeowner should be informed that the ventilation system might need to be rebalanced by a ventilation technician after installation of the appliance.

2. Indirect method: outside air is ducted to a point no closer than (12") 300mm from the appliance, to avoid affecting the performance of the appliance.

1. Direct connection: the F 400 Castine has been tested and listed for use with an outside air kit. This outside air kit is connected directly to the stove, be sure to follow the instructions provided with the kit.

**6. A ventilation system is installed in the house.**

5. There is excessive condensation on the windows in the winter.

**5. There is excessive condensation on the windows in the winter.**

4. The house is equipped with a well-sealed vapor barrier and tight fitting windows and/or has any powered devices that exhaust house air.

3. Opening a window slightly on a calm (wind less) day alleviates any of the above symptoms.

2. Existing fuel-fired equipment in the house, such as fireplaces or other heating appliances, smell, do not operate properly, suffer smoke roll-out when opened, or back-draft whether or not there is combustion present.

1. The F 400 Castine does not "draw" steadily, smoke rollout occurs, fuel burns poorly, or back-drafts occur whether or not there is combustion present.

Outside air may be required if:  
 a. the appropriate length of metallic pipe for a conduit of the outside air (3" diameter).  
 b. a rain/weather resistant cap for the outside of the house.  
 c. a rodent screen- that is no larger than 1/4" mesh

The Outside Air Kit includes an adapter to mount onto the stove that will except the fresh air pipe. Installation will require some additional materials:





The F 400 Castine is designed to burn cleanly and efficiently when used according to the guidelines expressed in these operating instructions. However, to maintain the proper performance, a yearly chimney inspection and cleaning in necessary. Failure to keep the chimney system free of creosote and build up could result in a serious chimney fire.

**ACCESSORIES**

Many accessories have been manufactured for use with the Jøtul F 400 Castine. ONLY USE ACCESSORIES THAT ARE SPECIFICALLY DESIGNED FOR THE JØTUL F 400 CASTINE.

**Firescreen (part # 129650)**

The F 400 Castine has been approved for use as an open fireplace, with front door open. This feature is especially nice when the ambience of a fire is desired. Some care should be taken when operating the stove as a fireplace.

- Always have the firescreen in place, attached to the stove front.
- Never overload the stove, for the best appearance burn in the traditional three log configuration.
- Reminder, when burning the stove with the screen in place, you are sacrificing efficiency for aesthetics, and you will be consuming wood at a much faster rate.

**WARNING: OPERATE YOUR JØTUL F 400 CASTINE WITH THE FRONT DOORS FULLY OPEN AND THE FIRESCREEN IN PLACE OR FULLY CLOSED. A PARTIALLY OPENED DOORS MAY RESULT IN OVERFIRING. ALSO, IF THE DOORS ARE LEFT PARTLY OPEN, GAS AND FLAME MAY BE DRAWN OUT OF THE STOVE OPENING, CREATING RISKS FROM BOTH FIRE AND SMOKE.**

**Outside Air Kit (part #154335)**

In certain installations it may be necessary to provide outside air to your F 400 Castine wood stove. Guidelines to determine the need for additional combustion air may not be adequate for every situation. If in doubt, it is advisable to provide additional air.

**General Maintenance**

Like your car, regular maintenance prolongs the life of your appliance. The following procedures do not take long and are generally inexpensive, but when done consistently, increase the life of your appliance and in turn, increase your years of enjoyment.

At least once a year you should perform the following maintenance procedures:

**Gaskets**

Check door and window gaskets for tightness. To check the seal of the front doors, close and latch the doors on a dollar bill and slowly try to pull the dollar bill free. If it can be easily removed then the seal is too loose. Check several spots around the door, and repeat the procedure on the ash pan door as well.

If gaskets need to be replaced, scrape out the old gasket and cement and clean the area with a wire brush. Apply a small bead of cement and push in the new gasket. After closing and latching the doors wipe clean, any excessive cement that has come from beneath the gasketing.

**GASKET LIST FOR THE F 400 CASTINE**

| Description         | Order # | Size        | Length |
|---------------------|---------|-------------|--------|
| Top Plate Gasket    | 100038  | 3/8" LD     | 7      |
| Smoke Outlet Gasket | 200028  | 3/16" LD/SA | 3      |
| Ash Door Gasket     | 200024  | 5/16" LD    | 4      |
| Glass Gasket        | 100038  | 3/8" LD     | 5      |
| Right door Gasket   | 100038  | 5/16" LD    | 5      |
| Left door Gasket    | 100038  | 5/16" LD    | 5      |





The side of the glass treated with an infrared coating (marked on the permimeter) should always be facing outward. It is extremely important to tighten the glass clips slowly and in a repeating pattern, like tightening the lugs on an automobile wheel.

**IMPORTANT:**

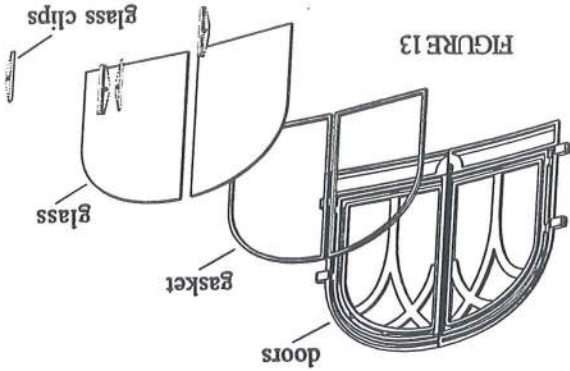


FIGURE 13

1. Remove the doors from the stove and place on a flat surface.
2. Carefully remove all of the glass clips from the inside of the doors.
3. Gently remove the glass panel and gasketing.
4. Remove all remaining debris from the glass area using a wire brush.
5. Apply a small bead of gasket/stove cement and the new gasket. Do not overlap the ends of the gasket rope.
6. Center the new glass panel over the gasket and reinstall the glass clips. See figure 13.
7. It may be necessary to retighten the glass clips after the stove has been burned and the gasketing has been seated.

**NEVER OPERATE THE STOVE WITH A CRACKED OR BROKEN GLASS PANEL.**

**Glass Removal:** Always operate the doors slowly and cautiously to avoid cracking or breaking the glass. Never use the door to push wood into the firebox. If the glass becomes cracked or broken follow this procedure for replacement:

**IMPORTANT:**  
REPLACE GLASS ONLY WITH A CERAMIC GLASS PANEL SPECIFICALLY DESIGNED FOR THE JØTUL F 400 CASTINE. DO NOT USE SUBSTITUTES. REPLACEMENT GLASS PANELS CAN BE ORDERED THROUGH YOUR JØTUL DEALER.

**MAINTENANCE**

**Ash removal:** OF COURSE, FOR YOUR PROTECTION ALWAYS WEAR SAFETY GLOVES WHEN HANDLING THE ASH PAN.

Ash removal will be required periodically depending on how frequently the stove is used. Conveniently, the F 400 Castine is equipped with an ash pan assembly for easy ash removal, without the need for opening the front doors.

The ash pan door is located under the front ashlip of the stove. To open the ash door place the receptacle end of your specially designed ash tool onto the square fitting of the ash door latch. Rotate the door counterclockwise to unlatch the door and clockwise to latch the door.

**WITH A GLOVED HAND** grasp the ash pan handle and remove the ash pan. Always close the ash pan door before leaving to dispose of the ashes.

The ashes should be placed in a metal container equipped with a tight sealing lid. The container should be placed on a noncombustible floor or on the ground, well away from all combustible materials, pending final disposal. If the ashes are disposed of by burial in soil or otherwise locally dispersed, they should be retained in the closed container until all cinders have thoroughly cooled.

**Glass Care:**

Cleaning: On occasion it will be necessary to clean the carbon deposits and fly ash off of the glass. If the carbon and fly ash are allowed to remain on the glass for an extended period of time it could eventually cause the glass to become etched and cloudy. Any creosote, which might deposit on the glass, will burn off during the next hot fire.

The proper cleaning procedure is as follows:

1. Glass needs to be COMPLETELY COOL.
2. Only use a cleaner that is specifically designed for this purpose. The use of abrasives will damage the glass and ultimately leave the glass frosted.
3. Rinse and dry glass completely, before burning your stove.





NEVER OVERTIRE THE STOVE. IF ANY PART OF THE STOVE OR CHIMNEY GLOWS, YOU ARE OVERTIRING, AND A HOUSE FIRE OR SERIOUS DAMAGE TO THE STOVE OR CHIMNEY COULD RESULT. IMMEDIATELY CLOSE DOWN THE AIR CONTROL. IF YOU NOTICE THIS CONDITION.

### Adding Fuel

When reloading the stove while it is still hot and a bed of hot embers still exist, follow this reloading procedure:

- Always wear gloves when tending to the stove.
- Push the air control lever to the full open position (far right).
- Wait a few seconds before opening the door.
- Use a stove tool or poker to distribute the hot embers equally around the firebox.
- Load the fuel, usually with smaller logs first.
- Close the door, be sure to latch the door tightly.
- Wait 5 – 10 minutes before adjusting the primary air to the desired heat output setting.

(If you have at least a 2" thick ember bed when reloading, it may be possible to close the door and immediately adjust the air control setting).

### The Formation of Creosote

When wood is burned slowly and at low temperatures, it produces tar and other organic vapors, which combine with moisture to form creosote. The slow moving smoke carries the creosote vapors, which condense in the cooler chimney flues, and this creosote then sticks to the chimney walls.

The creosote that accumulates in the chimney is highly flammable and is the fuel of chimney fires. To prevent chimney fires it is important to have the chimney and chimney connector pipe inspected and/or cleaned semi-annually. A qualified chimney sweep or other authorized service person can provide this service.

It is also important to remember that chimney size, temperature and height all affect draft which in turn affects the formation of creosote. Be sure to follow the installation and operation guidelines established in this manual.

### Starting and Maintaining a Fire

Burn only solid wood directly on the bottom grate of the stove, do not elevate the fire in any way.

The ash pan door on the stove must always be securely closed when the stove is in operation.

Burning the stove with the ashpan open will over-fire the stove and cause interior damage.

With the primary air control lever in the full open position, start with several sheets of crumpled newspaper placed directly on the grate. On top of the newspaper, place several pieces of small dry kindling (approx. 1" in diameter) with two to three larger logs (approx. 3" to 5" in diameter) on top.

Light the fire and close the door, slowly building the fire by adding larger and larger logs. Be sure to follow the break-in procedure before creating a fire that will damage the stove.

Once the stove has reached a surface temperature range of between 400° and 600°, adjust the primary air control lever as necessary to generate the heat output and burn time desired.

Stal recommends the use of a magnetic stove top thermometer to monitor the surface temperature of the stove. The optimum surface temperature range for the most efficient burn is between 400° and 600°. See figure 12 below for the optimum locations of a stove-top thermometer.

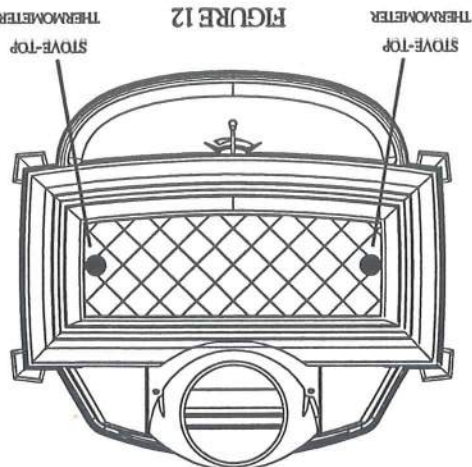


FIGURE 12





Note: IT IS NORMAL for a new painted stove to emit an odor and even smoke during its first several fires. This is caused by the seasoning of the high temperature paint and will diminish with each fire and will eventually disappear. Opening a window or door to provide additional ventilation will reduce the odor as this process takes its course.

Never allow the stove to exceed a 400° surface temperature during any "break-in fire" with the exception of the last "break-in" fire.

1. Light a small fire, newspaper and kindling only, only allow the stove to reach a maximum surface temperature of 200°. Burn for approximately 1 hour.
2. Allow stove to cool to room temperature.
3. Light a second fire, allowing the stove to reach a maximum temperature of 300° for 1 hour.
4. Cool the stove to room temperature.
5. Light a third fire and gradually allow the stove to reach a surface temperature of 400°
6. Cool stove to room temperature. This completes the "break-in" procedure.

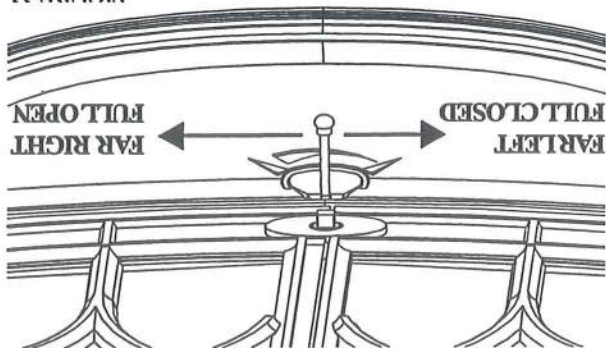
To monitor the stove's temperature, Jøtul recommends the use of a magnetic stove-top thermometer, placed directly on the corner of the stove's top plate.

Complete the following steps for the proper break-in procedure for the F 400 Castine:

Your new F 400 Castine is constructed of cast iron and stove furnace cement. This type of construction requires the stove to be "broken-in" gradually so that heat expansion does not occur too quickly and cause damage.

**Breaking in your new stove**

FIGURE 11



When first starting or reviving the fire: the primary control lever should be at the far right position, which allows the maximum amount of air into the stove. The more air entering the stove the hotter the fire the shorter the burn time. Moving the lever to the left reduces the air-flow into the stove which prolongs the fire at a lower heat output. See figure 11.

A single air control lever controls the burn time and heat output of the stove. This primary air control lever is located on the front of the stove directly above the ashpan. The primary air lever, controls the amount of air that enters the stove for combustion.

**Controls on the F 400 Castine**

**IMPORTANT**

NEVER BUILD OR ALLOW THE FIRE TO REST DIRECTLY ON THE GLASS. THE LOGS SHOULD ALWAYS BE SPACED AT LEAST ONE INCH FROM THE GLASS TO ALLOW FOR PROPER AIR FLOW WITHIN THE STOVE.

The burning of any of these materials can result in the release of toxic fumes. Never use gasoline, gasolene-type lantern fuel, kerosene, charcoal lighter fluid, or similar liquids to start or "freshen-up" the fire. Always keep such liquids away from the heater at all times.

- Do not burn:**
- \*Coal
  - \*Treated or painted wood
  - \*Chemical Chimney cleaners
  - \*Colored paper
  - \*Any synthetic fuel or logs
  - \*Garbage
  - \*Cardboard
  - \*Solvents

First this stove is designed to burn natural wood ONLY, wood that has been air-dried for a period of 6 to 14 months will provide the cleanest most efficient heat.

**Do Not Burn**

Before building a fire in your new F 400 Castine, please read the following section carefully and completely.

**OPERATION**

**WARNING:**

DO NOT INSTALL IN A BEDROOM/SLEEPING ROOM. THE STRUCTURAL INTEGRITY OF THE MOBILE HOME'S FLOOR, WALL, CEILING/ROOF MUST BE MAINTAINED.



# F 400 CASTINE WOODSTOVE CLEARANCES\*

| STOVE                        |                        | CLEARANCES                                  |       | UNPROTECTED SURFACE INSTALLATION |       | PROTECTED SURFACE INSTALLATION |       |
|------------------------------|------------------------|---|-------|----------------------------------|-------|--------------------------------|-------|
| Stove - no heatshield        | single wall pipe       | 19" A                                       | 485mm | 25" B                            | 635mm | 18" C                          | 460mm |
| Stove - with rear heatshield | single wall pipe       | 18" G                                       | 460mm | 18" H                            | 460mm | 13" I                          | 330mm |
| Stove - no heatshields       | double wall pipe       | 16"   | 405mm | 19"                              | 485mm | 13"                            | 330mm |
| Stove - with rear heatshield | with connector shield  | 15" M                                       | 380mm | 7" N                             | 180mm | 11" O                          | 280mm |
| Stove - rear heatshield      | with double wall pipe  | 15" S                                       | 380mm | 7" T                             | 180mm | 11" U                          | 280mm |
| CONNECTOR CLEARANCES (pipe)  |                        | UNPROTECTED SURFACE VERTICAL INSTALLATION   |       |                                  |       |                                |       |
| Single wall pipe             |                        | PROTECTED SURFACE VERTICAL INSTALLATION     |       |                                  |       |                                |       |
| Single wall pipe             | with rear heatshield   | 18"   | 460mm | 18"                              | 460mm | 12"                            | 300mm |
| Single wall pipe             | with connector shields | 7"  | 180mm | 7"                               | 180mm | 7"                             | 180mm |
| Double wall pipe             |                        | 7"  | 180mm | 7"                               | 180mm | 7"                             | 180mm |
| CONNECTOR CLEARANCES (pipe)  |                        | UNPROTECTED SURFACE HORIZONTAL INSTALLATION |       |                                  |       |                                |       |
| Single wall connector        |                        | PROTECTED SURFACE HORIZONTAL INSTALLATION   |       |                                  |       |                                |       |
| Single wall connector        |                        | 18"   | 460mm | 7"                               | 180mm | 6"                             | 150mm |
| Double wall Pipe             |                        | 6"  | 150mm | 6"                               | 150mm | 6"                             | 150mm |

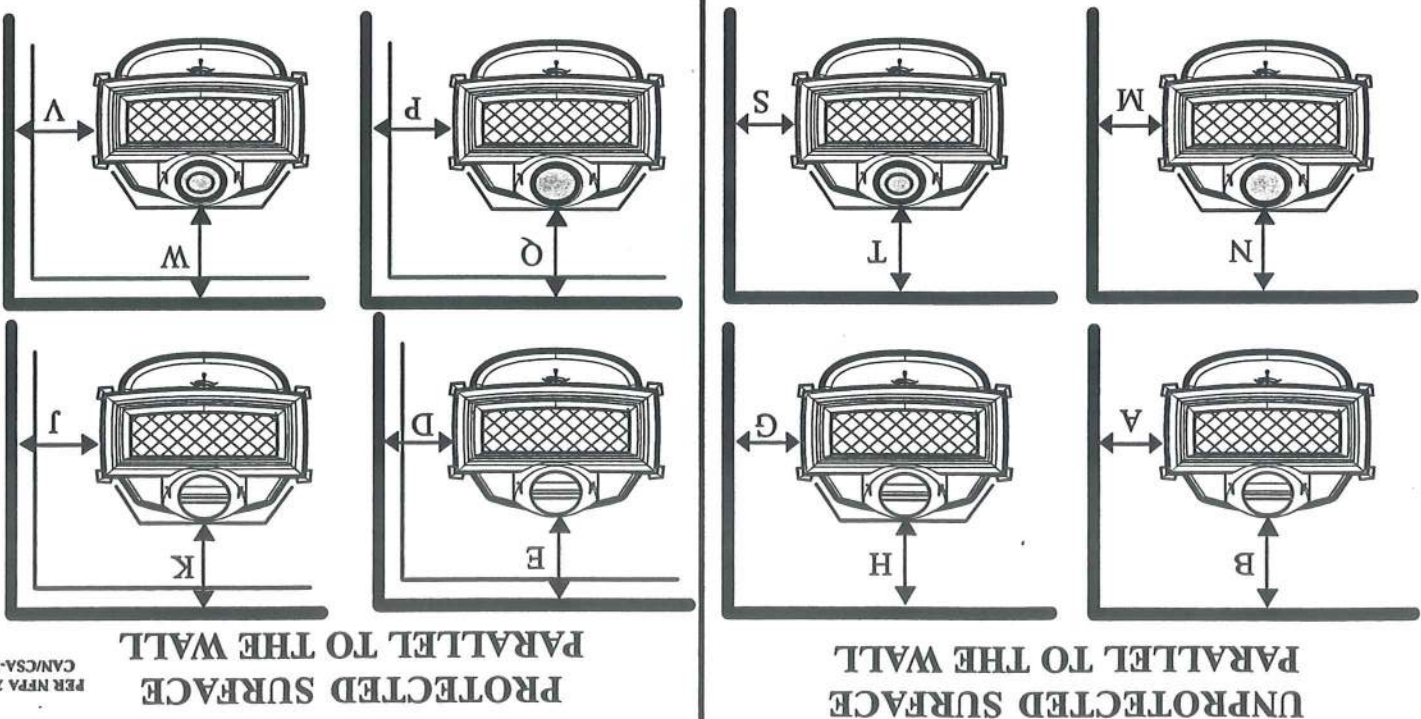
**MANTEL AND TRIM CLEARANCES**  
 Stove to 1" thick or less, side trim  
 Stove to 1" thick or less, top trim  
 Stove to mantel - maximum mantel depth 12"

13" 300mm  
 23" 585mm  
 25" 635mm





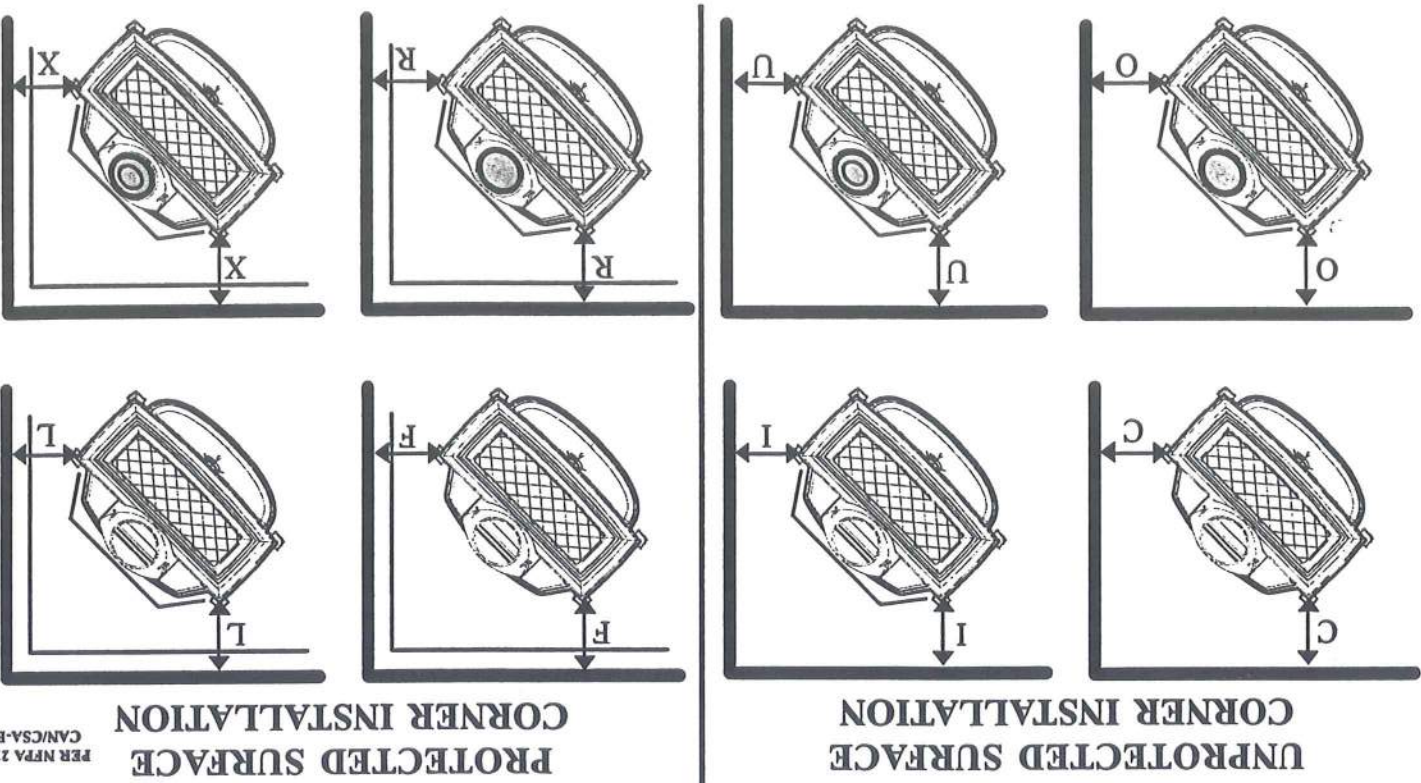
# F 400 CASTINE WOODSTOVE CLEARANCES



**IMPORTANT:**  
 CONNECTOR HEATSHIELDS AND DOUBLE WALL PIPE MUST BE A LISTED PRODUCT.  
 ALWAYS FOLLOW THE MANUFACTURER'S INSTRUCTIONS.

⊙ = SINGLE WALL PIPE WITH CONNECTOR SHIELDS

⊙ = DOUBLE WALL PIPE



PER NFPA 211 or  
 CAN/CSA-B365



**MOBILE HOME INSTALLATIONS**

The F 400 Castine has been approved for use in mobile homes in the U.S. and Canada, provided:

1. The stove is secured to the floor or the mobile home. Floor mounting kit #750304
2. The stove is provided outside air for combustion. Outside Air kit #154335 (see page 16 for more details)
3. Must be installed in accordance to 24CRR, Part 3280 (HUD).

As always consult with your local building inspector or fire officials about restrictions and requirements in your area, prior to installing the stove.

**UNPROTECTED ALCOVE INSTALLATION\***

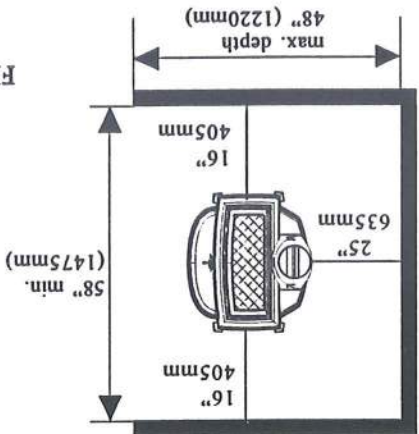


FIGURE 9

**PROTECTED ALCOVE INSTALLATION\***

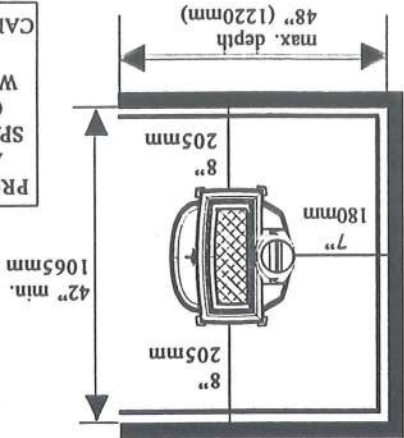


FIGURE 10

PROTECTION AND AIR SPACE MUST COMPLY WITH NFPA 211OR CAN/CSA-B365.

In Canada, refer to CAN/CSA-B365, *Installation Code for Solid-Fuel Burning Appliances and Equipment*, also for acceptable materials, proper sizing and construction guidelines.

Stove Mounted Heatshield: A stove rear heatshield has been specifically designed for the F 400 Castine. In the U.S. and Canada the rear heatshield part number is # 154911.

**NO OTHER HEAT SHIELD MAY BE USED.**

**NOTICE**

Accessories for woodstoves for clearance reduction have been developed by many manufacturers. If not following the methods of the installation codes, be sure that any accessory you choose has been tested by an independent laboratory and carries the laboratory's testing mark. Make sure to follow all of the manufacturer's instructions.

Always contact your local building inspector or fire officials about restriction and requirements in your area. Reminder, it is the local officials who have final authority in the installations approval.

**ALCOVE**

The F 400 Castine can be installed in an ALCOVE situation provided: See figures 9 and 10.

1. The stove must be installed with listed double wall pipe.

2. In a PROTECTED alcove installation both side walls and rear wall must be protected per NFPA 211 or CAN/CSA-B365. The wall protection must be elevated 1" from the floor and at least 1" off the combustible wall to allow for an air-flow.

3. The height of the wall protection including the bottom air space must be 48".

4. The Bottom heatshield is required in all Alcove installations.

5. ALCOVE floor protection must be: a UL/U/LC or WHI listed hearth pad or a non combustible material with a minimum R value of 2.0.

6. Minimum ceiling height in an unprotected installation, off the top of the stove is 58" (1475mm). The minimum ceiling height off the top of the stove in a protected ceiling installation is 36 (915mm).





**CLEARANCES TO COMBUSTIBLES**

**Floor Protection (In the U.S. and Canada)**

The F 400 Castine requires any one of the following three forms of hearth protection:

1. Any UL, ULC or WH listed hearth board. (No bottom hearthshield required).
2. Any non-combustible material that has a minimum R-value of 2.0. (No bottom hearthshield required).
3. Any non-combustible material WITH THE USE OF THE STOVE'S BOTTOM HEATSHIELD.

**ALL FORMS OF PROTECTION MUST be a non-combustible surface extending a minimum of 18" (460mm) in front of the stove. And 8" (200mm) from the sides and back of the stove (measured from side and back panels).**

In a rear vent installation the floor protection must also extend under the stove pipe a minimum of 2" (50mm) beyond either side of the pipe. See figure 8. WHEN CONSTRUCTING A NEW HEARTH OR FLOOR PAD, CONSULT APPENDIX A AT THE BACK OF THIS MANUAL, FOR ALTERNATE MATERIALS AND METHODS.

**This will result in a minimum floor protection of 42"W X 44"D. See figure 8.**

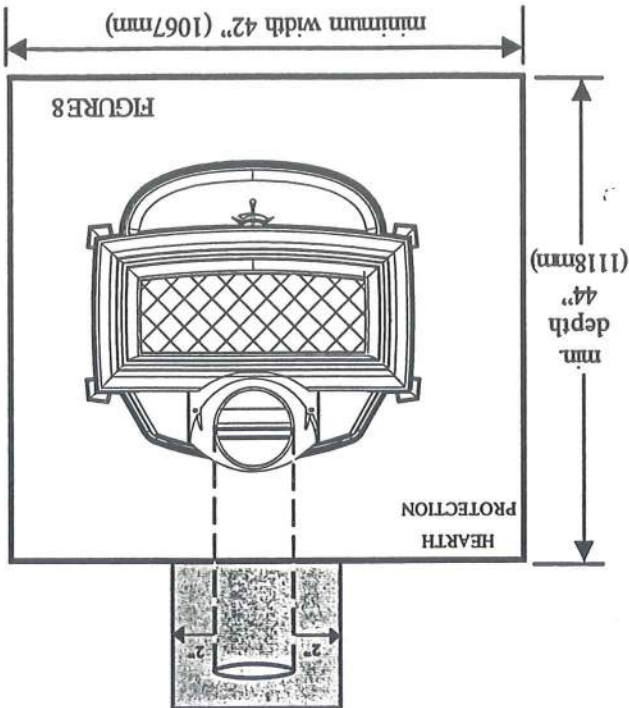
Pipe shields: When using listed pipe shields to reduce the connector clearance to combustibles, it must start 1" above the lowest exposed point of the connect pipe and extend vertically a minimum of 25" above the top surface of the stove.

Double wall pipe: Listed double wall pipe is an acceptable alternative to connector pipe heatshields. Wall-Mounted Protection: When reducing clearances through the use of wall mounted protection:

In the U.S. refer to NFPA 211, *Standard for Chimneys, Fireplaces, Vents and Solid Fuel Burning Appliances*, for acceptable materials, proper sizing and construction guidelines.

**SEE PAGES 10-12 FOR COMPLETE CLEARANCE REQUIREMENTS AND DIAGRAMS.**

**Using Shields to Reduce Clearances**





## Hearth-mount into a Masonry Fireplace

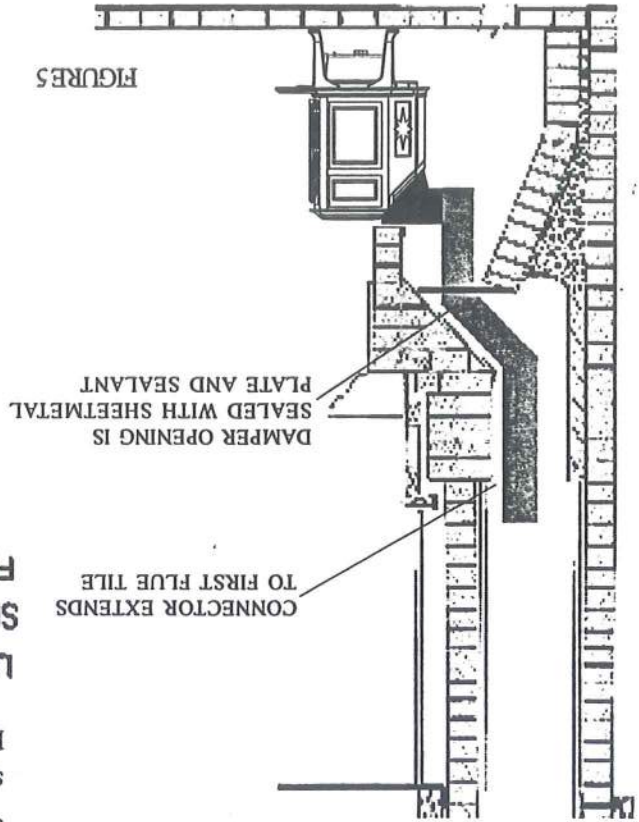
The F 400 Castine may be installed into a masonry fireplace provided the height of the opening is a minimum of 29 1/2". If necessary, the short leg package reduces the stove's height by 2 1/4".

When installing the F 400 Castine into a masonry fireplace, code requires that the fireplace damper plate be removed or securely fixed in the open position. A connector pipe must then extend from the stove's flue exit through the damper area of the fireplace and into the chimney tile liner. See figure 5.

The inside area of the flue liner must not be less than the area of the stove's flue exit, and cannot be more than three times greater than the cross sectional area of the stove's flue exit.

If the chimney liner is too large to accommodate the stove, an approved relining system must be installed to resize the flue.

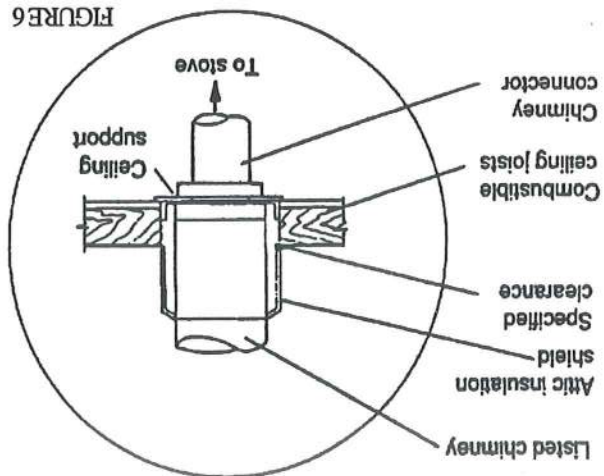
A new sheet metal damper block-off plate must be installed around the connector pipe at the damper frame and sealed with the proper sealant (usually High-Temp Silicone).



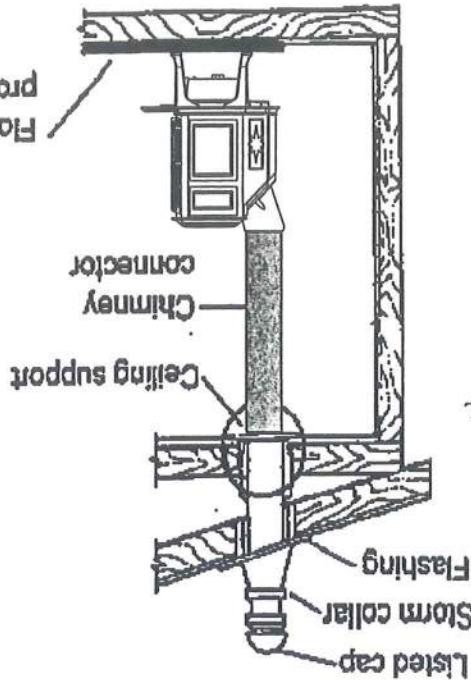
## Prefabricated Chimneys

When installing the F 400 Castine to a prefabricated metal chimney always follow the pipe manufacturer's instructions and be sure to use the components that are required. This usually includes some type of "smoke pipe adapter" that is secured to the bottom section of the metal chimney and allows the chimney pipe to be secured to it with three sheet metal screws.

See figures 6 and 7.



Fireplace installation must also observe the proper clearances to surrounding trim and mantels (addressed in clearance section of this manual). In addition, fireplace installations must also adhere to the floor protection guidelines specified in the following section.







Consult your local building inspector, authorized Jøtul Dealer, NFPA 211 in the U.S. or CAN/CSA-B635 in Canada for other approved wall pass-through methods.

### CONNECTING TO THE CHIMNEY

#### Masonry Chimney

When installing a Jøtul F 400 Castline into a masonry chimney through a "thimble" (the opening through the chimney wall to the flue), the thimble must be lined with ceramic tile or metal and be securely cemented in place.

The chimney connector/stove pipe must slide completely inside the thimble to the inner surface or the flue liner. It may be necessary to make use of a thimble sleeve (a pipe with a slightly smaller diameter than standard stove pipe). This special pipe can be easily installed into a thimble. See figure 4.

Make sure the connector pipe or thimble sleeve does not protrude into the flue liner, thereby restricting the area the smoke has to flow through. This bottle-neck will have a negative affect on the chimney system.

The chimney connector should be sealed at the thimble with refractory cement and the stove pipe leading to the stove should have a minimum of three screws.

### DO NOT CONNECT THIS STOVE TO A CHIMNEY FLUE SERVING ANOTHER APPLIANCE OF ANY KIND.

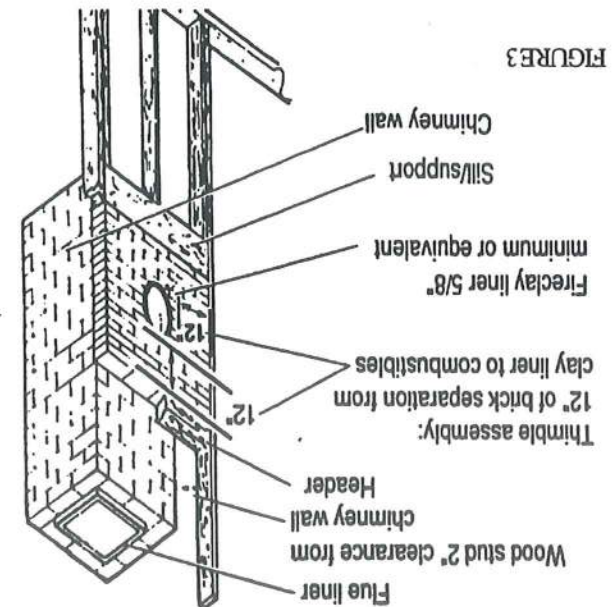
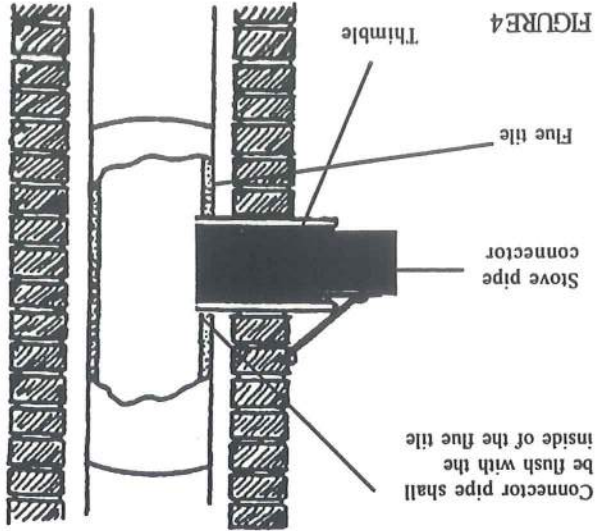


FIGURE 3

In Canada

The Canada standard has been established by the Canadian Standard Association. The installation must conform to CAN/CSA-B365, *Installation Code for Solid Fuel Burning Appliances and Equipment*. Before proceeding be sure to consult your local building inspector.

#### Common Method

This method requires the removal of all combustible materials from at least 18" (457mm) around the chimney connector's proposed location. With a 6" round liner the minimum area required would be 43" x 43" square.

It is important to remember to locate the pass-through at least 18" from the ceiling to maintain the proper clearance to combustibles.

The space that is cleared of combustible materials must then remain empty. Sheet metal panels can then be used to cover the area. However, when using a panel on both sides of the wall each cover must be installed on noncombustible spacers at least 1" from the wall. If one panel of sheet metal is to be used it may be installed flush to the wall.

SEE SECTION 5.3.1 and 5.3.2 of CAN/CSA - B365-M91.





## WALL PASS-THROUGHS

When your installation unavoidably requires the chimney connector to pass through a combustible wall to reach the chimney, always consult your local building officials, and be sure any materials to be used have been tested and listed for wall pass-throughs.

In the U.S.

The National Fire Protection Association's publication, *NFPA 211, Standard for Chimneys, Fireplaces, Vents and Solid Fuel Burning Appliances* permits four methods for passing through a combustible wall. Before proceeding with any method be sure to consult with your local building officials to discuss any local code requirements.

Common Method

When passing through a combustible wall to a masonry chimney this method requires the removal of all combustible materials from at least 12" around the chimney connectors proposed location. With a 6" round liner the minimum area required would be 31" x 31" square.

The space is then filled with at least 12" of brick around a fireclay liner. Remember, the liner must be ASTM C35 or equivalent, with a minimum wall thickness of 5/8".

It is important to remember to locate the pass-through at least 18" from the ceiling for proper clearance to combustibles.

It will be necessary to cut wall studs, install headers, and construct a sill frame to maintain the proper dimensions and to support the weight of the brick.

The bricks must be solid brick with a minimum of 3 1/2" thick (4" nominal).

Refractory mortar must be used at the junction of the chimney and the pass-through liner. The pass-through liner must not penetrate the chimney liner beyond the inner surface of the chimney liner. Use extreme care when constructing the hole in the chimney liner, the tiles can shatter easily. See figure 3.

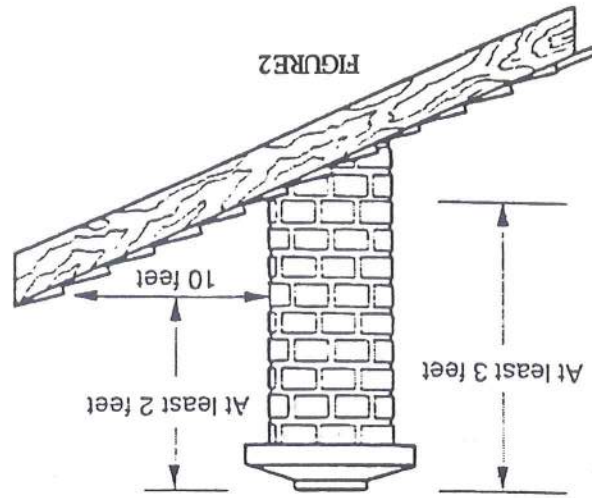
## Chimney Height

The manufacturer's installation instructions must be followed precisely. Always maintain the proper clearance to combustibles as established by the pipe manufacturer. This clearance is usually a minimum of 2", although it may vary by manufacturer or for certain chimney components.

Whether a masonry chimney or prefabricated metal chimney is used it must be the required height above the roof line.

The requirement is:

The chimney must be at least 3 feet higher than the highest point where it passes through the roof and at least 2 feet higher than the highest part of the roof or structure that is within 10 feet of the chimney, measured horizontally. See figure 2.



Chimneys shorter than 14 feet may not provide adequate draft. This could result in smoke spilling into the room from the stove when loading the stove, or when the door is open. In addition, inadequate draft can cause back puffing, which is a build up of gases inside the firebox.

Other times, chimney height can create excessive draft which can cause high stove temperatures and short burn times. Excessive drafts can be corrected by installing a butterfly damper. If you suspect you have a draft problem, consult your dealer.





The chimney size should not be less than the cross-sectional area of the flue collar, and not more than three times greater than the cross-sectional area of the flue collar.

When selecting a chimney type and the location for the chimney in the house, keep this in mind: it is the chimney that makes the stove work, NOT the stove that makes the chimney work. This is because a chimney actually creates a suction, called "draft" which pulls air through the stove.

Several factors affect draft: chimney height, cross-sectional area (size), and temperature of the chimney, as well as the proximity of surrounding trees or buildings.

As a result, a short masonry chimney on the exterior of a house will give the poorest performance. This is because it can be very difficult to warm the chimney thereby creating inadequate draft. In extremely cold northern areas it may be necessary to reline the chimney or extend its height to help establish draft.

Oppositely, a tall masonry chimney inside the house is easier to keep warm and will perform the best.

The following guidelines give the necessary chimney requirements based on the national code (ANSI-NFPA 211 for the US. And CSA CAN-B365 for Canada). However, many local codes differ from the national code to take into account climate, altitude, or other factors.

**NOTICE:** It is important that you check with your local building officials to find out what codes apply in your area before installing your new F 400 Castine.

**REMEMBER:** Your local inspector(s) have the final authority in approving your installation. It is always best to consult them prior to the installation.

DO NOT CONNECT THIS STOVE TO ANY AIR DISTRIBUTION DUCT OR SYSTEM.

### Masonry Chimneys

When installing the F 400 Castine into a masonry chimney you must conform to all of the following guidelines:

- The masonry chimney must have a fireclay liner or equivalent, with a minimum thickness of 5/8" and must be installed with refractory mortar. There must be at least 1/2" air space between the flue liner and chimney wall.

- The fireclay flue liner must have a nominal size of 8" X 8", and should not be larger than 8" X 12". If a round fireclay liner is to be used it must have a minimum inside diameter of 6" and not larger than 8" in diameter. If a chimney with larger dimensions is to be used, it should be relined with an appropriate liner that is code approved.

- The masonry wall of the chimney, if brick or modular block, must be a minimum of 4" nominal thickness. A mountain or rubble stone wall must be at least 12" thick.

- A newly-built chimney must conform to local codes and in their absence must recognize national regulations.

- When using an existing chimney, it must be inspected by a professional licensed chimney sweep, fire official, or code officer, to ensure that the chimney is in proper working order.

- No other appliance can be vented into the same flue.
- An airtight clean-out door should be located at the base of the chimney.

### Prefabricated Chimneys

If a prefabricated metal chimney is to be used it must be a chimney type that is tested and listed for use with solid fuel burning appliances. High Temperature (HT) Chimney Standard UL 103 for the U.S. and High Temperature Standard ULC S-629 for Canada.





## INSTALLATION

IF THIS SOLID FUEL ROOM HEATER IS NOT PROPERLY INSTALLED A HOUSE FIRE MAY RESULT. FOR YOUR SAFETY, FOLLOW THE INSTALLATION DIRECTIONS. CONTACT THE LOCAL BUILDING OR FIRE OFFICIALS ABOUT RESTRICTIONS AND INSTALLATION INSPECTION REQUIREMENTS IN YOUR AREA.

### Reminder:

Your local officials have final authority in determining if a proposed installation is acceptable. Any requirement, that is requested by the local authority having jurisdiction, that is not specifically addressed in THIS manual, defaults to NFPA 211, and local codes in the U.S. or in Canada, CAN/CSA-B365-M and local codes.

### TOP OR REAR EXIT FLUE

The F 400 Castine is shipped with the flue collar, gasketing and hardware inside the stove. To install the flue collar in the top or rear exit position remove the tape from the gasketing and adhere to the groove on the back of the stove around the flue opening. Place the flue collar on the stove in the top or rear exit position and secure with the nut, bolt and washer. The nut and washer are placed on the inside of the stove.

### STOVE PIPE CHIMNEY CONNECTOR

The chimney connector is a single walled pipe used to connect the stove to the chimney. For use with the F 400 Castine the chimney connector MUST be 6" in diameter, with a minimum thickness of 24 gauge black steel.

Aluminum and Galvanized steel pipe is not acceptable for use with the F400 Castine. These materials cannot withstand the extreme temperatures of a wood fire and can give off toxic fumes when heated.

**Do not use the connector pipe as a chimney.**

Each chimney connector or stove pipe section must be installed to the stove flue collar and to each other with the male (crimped) end toward the stove.

See figure 1.

This prevents any amount of condensed or liquid creosote from running down the outside of the pipe or the stove top. All joints, including the flue collar connection must be secured with three sheet metal screws to ensure that the sections do not separate.

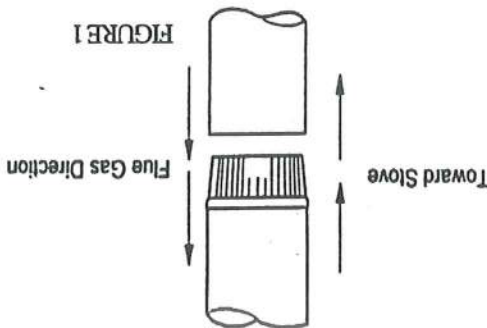


FIGURE 1

For the best performance the chimney connector should be as short and direct as possible, with no more than two 90° elbows. The maximum horizontal run is 36" and a recommended total length of stove pipe should not exceed 10 feet. Always slope horizontal runs upward 1/4" per foot toward the chimney.

No part of the chimney connector may pass through an attic or roof space, closet or other concealed space, or through a floor or ceiling. All sections of the chimney connectors must be accessible for cleaning. Where passage through a wall or partition of combustible construction is desired, the installation must conform with NFPA 211 or CAN/CSA-B365, and is also addressed in this manual.

## DO NOT CONNECT THIS UNIT TO A CHIMNEY FLUE SERVING ANOTHER APPLIANCE.

## CHIMNEY REQUIREMENTS

There are two types of chimneys suitable for the F 400 Castine:

1. A code-approved masonry chimney with a flue liner.
2. A prefabricated chimney complying with the requirements for Type HT (2100°F) chimneys per UL 103 or ULCS 629.





## NOTICES

• DO NOT: USE CHEMICALS OR FLUIDS TO START THE FIRE. DO NOT BURN GARBAFE OR FLAMMABLE FLUIDS.

• IF THIS ROOM HEATER IS NOT PROPERLY INSTALLED, A HOUSE FIRE MAY RESULT. TO REDUCE THE RISK OF FIRE, FOLLOW THE INSTALLATION INSTRUCTIONS. FAILURE TO FOLLOW THESE INSTRUCTIONS MAY RESULT IN PROPERTY DAMAGE, BODILY INJURY, OR EVEN DEATH.

• Jøtul recommends that you have your new Jøtul F 400 Castine installed by a professional installer of solid fuel burning appliances.

• EXTREMELY HOT WHILE IN OPERATION! KEEP CHILDREN, CLOTHING AND FURNITURE AWAY. CONTACT MAY CAUSE SKIN BURNS.

• Avoid creating a low pressure condition in the room where the stove is operating. Operating an exhaust fan or a clothes dryer could create a low pressure area, causing poisonous gases to come out of the stove into the room.

• You can prevent low pressure conditions by providing adequate combustion air within 24" but not closer than 12" from the stove. Or, simply install the optional outside air manifold system, which allows the direct connection of air from outside the house to the stove.

• Do not use chemicals or fluids to start the fire. Some fuels will, during combustion, separate carbon monoxide and generate it in the burn chamber. Carbon monoxide is toxic, so please follow the guidelines in this manual for proper operation of your Jøtul F 400 Castine.

• If you for some reason experience smoke "toll-out" from the stove, it may activate smoke detectors if installed in the house.

## STANDARDS

The F 400 Castine woodstove has been tested and listed to;

U.S. Standards: ANS/UL 737 and ANS/UL 1482.  
Canadian Standards: CAN/ULC-S627-M93

Tests performed by ITS, Intertek Testing Services, Middleton, WI

Manufactured by Jøtul A.S.A., P.O. Box 135  
Fredrikstad, Norway  
Distributed by Jøtul North America, P.O. Box 1157  
400 Riverside Street  
Portland, ME 04104

This heater meets the U.S. Environment Protection Agency's Emissions limits for wood heaters manufactured and sold after July 1, 1990.

Under specific test conditions, this heater has shown heat output at rates ranging from 12,000 to 35,000 BTU's per hour.

The Jøtul F 400 Castine woodstove is ONLY listed to burn wood . Do not burn any other fuels.

## JØTUL F 400 CASTINE WOODSTOVE

When installing, operating and maintaining your Jøtul F 400 Castine woodstove, follow the guidelines presented in these instructions, and make them available to anyone using or servicing the stove.

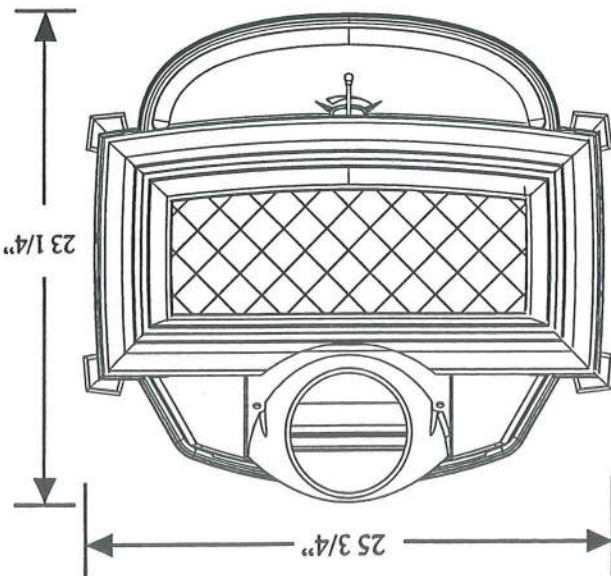
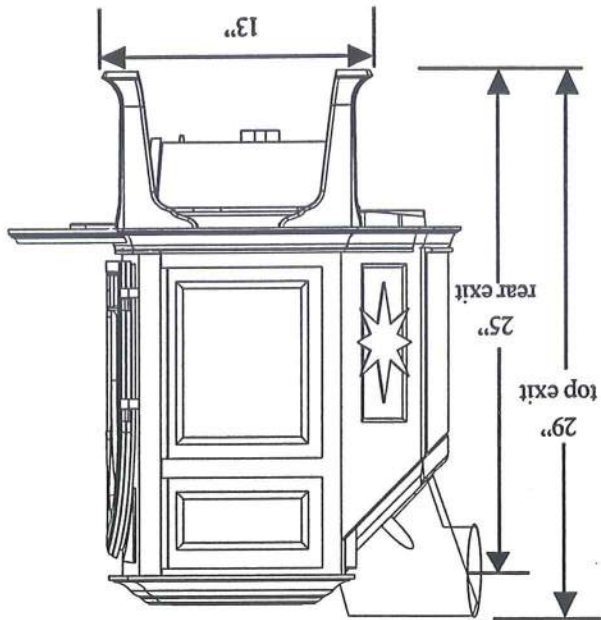
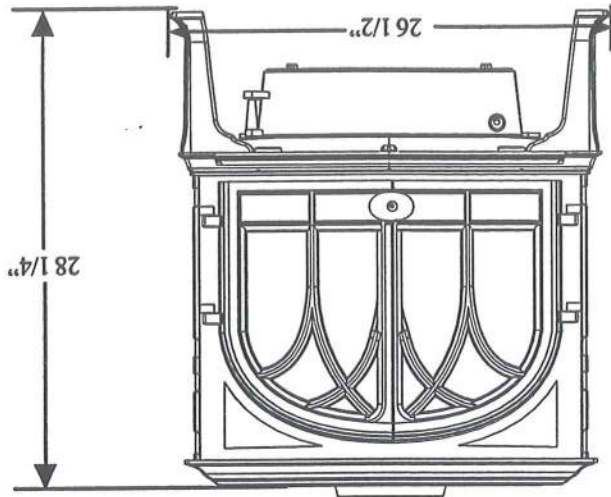
A number of areas require a building permit to install a solid fuel burning appliance. In the U.S., the National Fire Protection Association's Code, NFPA 211, *Standards for Chimneys, Fireplaces, Vents and Solid Fuel Burning Appliances*, or similar regulations, may apply to the installation of a solid fuel burning appliance in your area.

In Canada, the guideline is established by the CSA Standard, CAN/CSA-B365-M93, *Installation, Code for Solid-Fuel-Burning Appliances and Equipment*. Always consult your local building inspector or authority having jurisdiction to determine what regulations apply in your area.

DO NOT CONNECT TO ANY AIR DISTRIBUTION DUCT OR SYSTEM







SAVE THESE INSTRUCTIONS AND MAKE THEM AVAILABLE TO ANYONE USING OR SERVICING THE STOVE.  
 READ THIS ENTIRE MANUAL BEFORE YOU INSTALL AND USE YOUR NEW ROOM HEATER.

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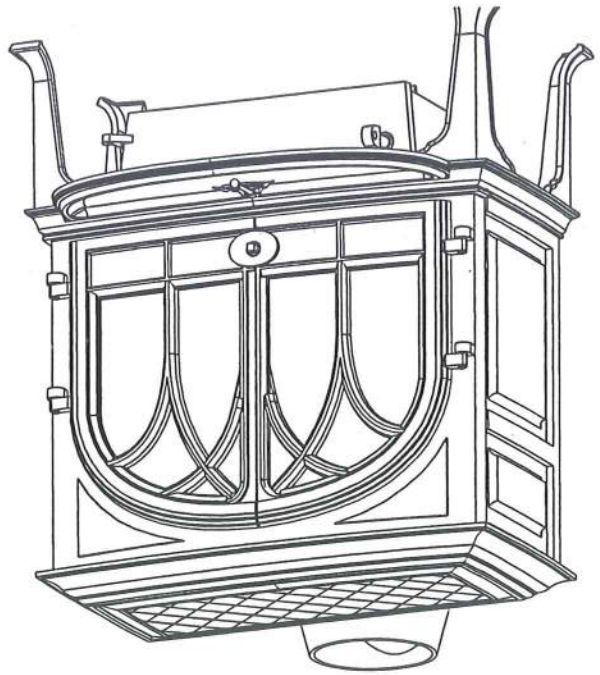
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- 17 Stove-Top Thermometer.....
- 18-19 Parts Diagram.....
- 19 Appendix A (alternate floor protection).....







# Jøtul F 400 Castine Woodstove



## Installation and Operating Instructions for USA Installation et fonctionnement pour Canada

Safety notice: If this solid fuel room heater is not properly installed, a house fire may result. For your safety, follow the installation directions. Contact local building or fire officials about restrictions and installation inspection requirements in your area. Kindly save these instructions for future reference.

Avis de sécurité: Une installation non appropriée de ce poêle de chauffage risque de provoquer un incendie. Assurez votre sécurité en respectant les directives d'installation suivantes. Consultez les autorités locales du bâtiment ou de la prévention des incendies au sujet des restrictions et exigences relatives aux inspections d'installations dans votre région.

Tested and listed by ITS Intertek Testing Services, Middleton, Wisconsin.  
Tested to U.S. Standards: ANSI/UL 1482, Canadian Standards: CAN/ULC-5627-M93





## EXAMPLE CALIBRATION/DATA FLOW

All individual test run raw data sheets are organized in a manner that would allow a data reviewer to follow the data as it is being calculated in a step by step fashion. In many cases, the equations used to calculate a specific required data are given on the raw data sheets themselves.

For example, the particulate emission rate in g/dscf is calculated on Data Sheet #7. However, the data used to derive this data begins on Data Sheet #2 (Meterbox Data Sheet) where the meter volume (cubic feet), average meter temperature (°F), average  $\Delta H$  (in. H<sub>2</sub>O), and average Barometric pressure (in. Hg) are recorded and averaged. Each of the averages for these parameters are used in equation 1 on P. 7 where the volume (MCF) is converted to dscf.

The moisture catch sheet (p. 3) total (g. H<sub>2</sub>O) is transferred to P. 7 and the percent stack moisture is calculated in equations 2 and 3.

The gross and net gravimetric (g) particulate catches are determined and calculated on PP. 4-6. Pages 4-1, 4-2 and 4-3 show the initial (tare) constant weights for filters (p. 4-1) and beakers (p. 4-2) and the final constant weights (p. 4-3) for those filters and beakers used for each run. Final and tare weight data is transferred to P. 5-1 (front half catch) and P. 5-2 (back half catch) and the gross gravimetric (g) catch for each filter and beaker is calculated. On P. 5-3 the gravimetric catch for each blank is calculated. The gross gravimetric catch for each filter and beaker is transferred to P. 6 and the net gravimetric catch (g) is calculated, as well as front half and back half catch totals. The net gravimetric catch (g) is transferred to P. 7 and the grain loading/dscf is calculated in equation 4.

Some data sheet specific information is listed below on a page by page basis.

P. 8           The % ambient moisture is determined by interpolating from psychrometric charts which are contained in the State of Oregon Department of Environmental Quality's "Standard Method for Measuring the Emissions and Efficiencies of Woodstoves".

              The % relative humidity is determined from the wet bulb/dry bulb temperature readings using the tables found in Section 3.1.2.4 of the State of Montana Air Quality Bureau's Quality Assurance Manual.

P. 10           The uncorrected moisture meter readings are corrected for pin insulation and may or may not be corrected for ambient (wood) temperatures. All corrections are based upon the correction equations or tables supplied by the moisture meter manufacturer. (These are standard, known corrections.)

P. 11           The moisture meter readings are corrected as discussed above.





P. 12 The gas concentrations shown for each gas monitored (CO<sub>2</sub>, O<sub>2</sub>, CO and SO<sub>2</sub>) are determined by converting the analyzer's voltage output recorded on P. 12 to the concentration shown using the analyzer's current calibration curve. The SO<sub>2</sub> concentration is determined using the manufacturer's calibration curve and the current calibration curve.

The cal. W/B (calculated wet bulb) temperature is obtained by first determining the % moisture in the extracted flue gas stream using the temperature data from thermocouples 1 (Wet Bulb) and 2 (Dry Bulb). Then based upon the stack temperature (thermocouple 3) and the % moisture in the extracted gas stream, a calculated wet bulb temperature is determined. All data is derived from the psychrometric tables found in the State of Oregon's "Standard Method for Measuring the Emissions and Efficiencies of Woodstoves".

The following pages contain the equations used to generate the data on Tables 3-5 on the computer printouts:

Dry Gas Volume (standard):

$$V_{m(std)} = \frac{V_m * 17.65 * mcf * \left( P_{bar} + \frac{\Delta H}{13.6} \right)}{T_m}$$

Volume of Water:

$$V_{w(std)} = (0.04707)(ml \text{ H}_2\text{O})$$

Moisture Content:

$$B_{ws} = \left( \frac{V_w}{V_w + V_{m(std)}} \right) * 100$$

Dry Burn Rate:

$$Br = \left( \frac{Wwt - (Wwt * \% \text{ H}_2\text{O})}{2.2046} \right) * \frac{60}{\theta}$$

Carbon Balance (N<sub>c</sub>):



$$N_t = \frac{K_3 N_c}{(Y_{CO_2} + Y_{CO} + Y_{HC})}$$

Stack Flow Rate ( $Q_{sd}$ ):

$$Q_{sd} = K_4 N_t Br$$

Particulate Concentration ( $C_s$ ):

$$C_s = \frac{M_n}{V_{m(std)}}$$

Particulate Emission Rate (E):

$$E = C_s Q_{sd}$$

Proportional Rate Variation (Pr):

$$Pr = \left( \frac{\theta S_i * V_{mi(std)}}{10 \sum_{i=1}^n [S_i * V_{mi(std)}]} \right) * 100$$

Where:

Br = dry wood burn rate, kg/hr.

$B_{ws}$  = Water vapor in the gas stream, proportion by volume.

$c_s$  = Concentration of particulate matter in stack gas, dry basis, corrected to standard conditions, g/dscm (g/dscf).

E = Particulate Emission Rate, g/hr.

$\Delta H$  = Average pressure differential across the orifice meter (see Figure 5-2), mm H<sub>2</sub>O (in. H<sub>2</sub>O).

$K_3$  = 1.0 lb/lb (English)  
1000 g/kg (metric)

$K_4$  = 0.02406 dsm<sup>3</sup>/g-mole (metric)  
384.8 dscf/lb-mole (English)

$m_n$  = Total amount of particulate matter collected, mg.

mcf = Dry gas meter correction factor.





- $N_c$  = Gram atoms of carbon/gram of dry fuel (lb/lb), equal to 0.0425.
- $N_t$  = Total dry moles of exhaust gas/Kg of dry wood burned.
- $P_r$  = Percent of proportional sampling rate.
- $P_{bar}$  = Barometric pressure at the sampling site, mm Hg (in. Hg).
- $Q_{sd}$  = Total gas flow rate, dscf/hr.
- $S_i$  = Concentration measured at the  $SO_2$  analyzer for the "i<sup>th</sup>" 5 minute interval, ppm.
- $S_1$  = Concentration measured at the  $SO_2$  analyzer for the first 5 minute interval  
ppm
- $T_m$  = Absolute average DGM temperature (see Figure 5-2), °K (°R).
- $T_{std}$  = Standard absolute temperature, 293°K (528°R).
- $V_m$  = Volume of gas sample as measured by dry gas meter, dcm (dcf).
- $V_{m(std)}$  = Volume of gas sample measured by the dry gas meter, corrected to standard conditions, dscm (dscf).
- $V_{w(std)}$  = Volume of water vapor in the gas sample, corrected to standard conditions, scm (scf).
- $W_{wt}$  = Wet wood weight.
- $Y$  = Dry gas meter calibration factor.
- $Y_{CO}$  = Measured mole fraction of CO (dry).
- $Y_{CO_2}$  = Measured mole fraction of  $CO_2$  (dry).
- $Y_{HC}$  = Assumed mole fraction of HC (dry);  
 =0.0088 for catalytic woodheaters  
 =0.0132 for noncatalytic woodheaters  
 =0.0080 for pellet fired woodheaters
- $\theta$  = Total sampling time, min.
- 13.6 = Specific gravity of mercury.
- 60 = Sec/min.
- 100 = Conversion to percent.



## M5H PARTICULATE SAMPLING TRAIN

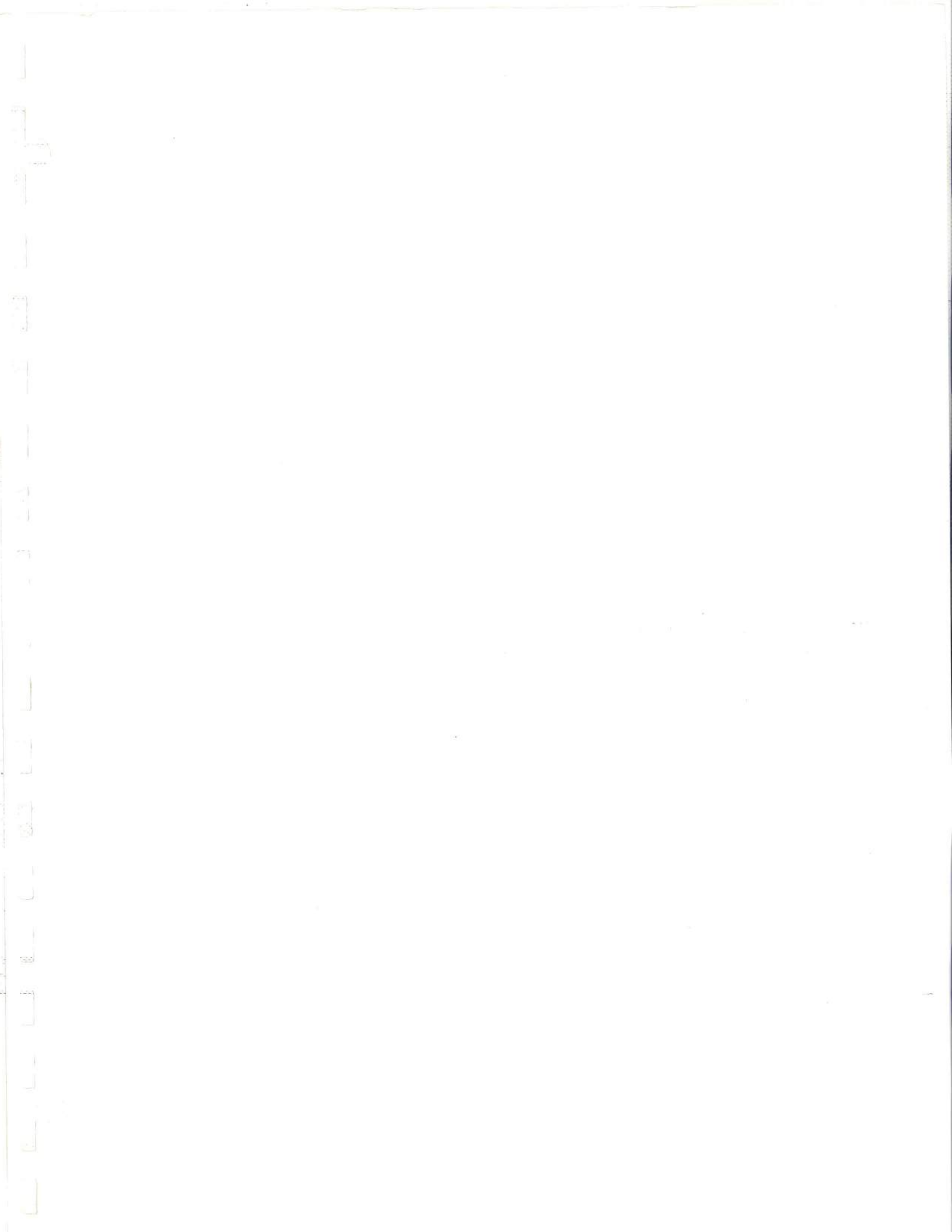
1. Probe  
3/8" seamless SS-20" long. Outlet end of probe is attached to a SS outlet fitting with a Sweglock SS union. The probe is unheated except for the portion that is in the stack and the heated filter box. The probe is sealed to the stack with a washer.
2. Filter Holder  
A 3" or 4" standard M5 filter holder. A SS filter support with gasket.
3. Filters  
3" or 4" fiber glass (#25 glass) manufactured by Schleicher and Schuell.
4. Front Half Filter Heater  
A box containing a fan for air circulation and a cone heater. The temperature in the box is monitored with a type K thermocouple and adjusted with a voltage regulator to maintain a temperature below 248 °F.
5. Desiccant  
Indicating silica gel, 6-20 mesh. The silica gel is changed as needed.
6. Filter (Back Half) Holder  
Same as front half 3" or 4" filter.
7. Impinger Gas  
Type K thermocouple threaded into the exit "arm" of the impinger. Ice is added to the cooler whenever necessary to maintain an exit gas temperature less than 68 °F.
8. Meterbox  
RAC Stack Sampler modified by EEMC  
Ranges: 0-1.0" inclined water manometer  
          0-10.0" vertical water manometer  
Accuracy: Dry gas Meter 0-999,999 cu ft ±1.0%  
          Temperatures are monitored using two type K thermocouples.













## SAMPLING PROCEDURES AND INSTALLATION DESCRIPTION

This section is broken into two major parts. The first contains a brief description of the sampling and procedures used by LoKee when performing a test using EPA Methods 28, 28A and 5H. The second section contains a complete listing of all equipment in each of the major sampling trains and a diagram of each major train.

LoKee uses EPA M5H for the particulate sampling procedure and collects the required data so that efficiency of a unit can be calculated using the Oregon Method.

## TEST FACILITY AND WOOD HEATER EQUIPMENT LIST

1. Flue Pipe

The diameter of the 24 gauge black steel flue pipe used for each stove varies with the size of the stove's flue collar, e.g., 6" flue pipe is used with a 6" flue collar. The joint at the flue collar is sealed with mortar. The pipe is attached to the stove at the flue collar with three sheet metal screws. All sampling ports are sized for the sampling probes and sealed using washers.

2. Insulated Flue Pipe

The diameter of the insulated flue pipe matches the diameter of the flue collar on the stove. The 6", 7" and 8" pipe meet the requirements of UL 103 HT. The SO<sub>2</sub> injection loop port is sealed with high temperature silicone sealant.

3. Liquid Seal

The liquid (oil) seal used by LoKee varies in size with the flue pipe. The seals are made of 12 gauge steel. The liquid sealant is mineral oil. The cooler consists of 3/8" copper tubing which is coiled in the bottom of the lower half of the seal. Ambient air is pumped through this line when necessary to cool the seal.

4. Supports

The lower half of the seal and the 24 gauge steel black flue pipe is supported by the stove. The upper half of the seal and the insulated flue pipe are hung from wooden supports.

5. Platform Scale

Platform (30" X 30" deck)

Manufacturer: Weightronics

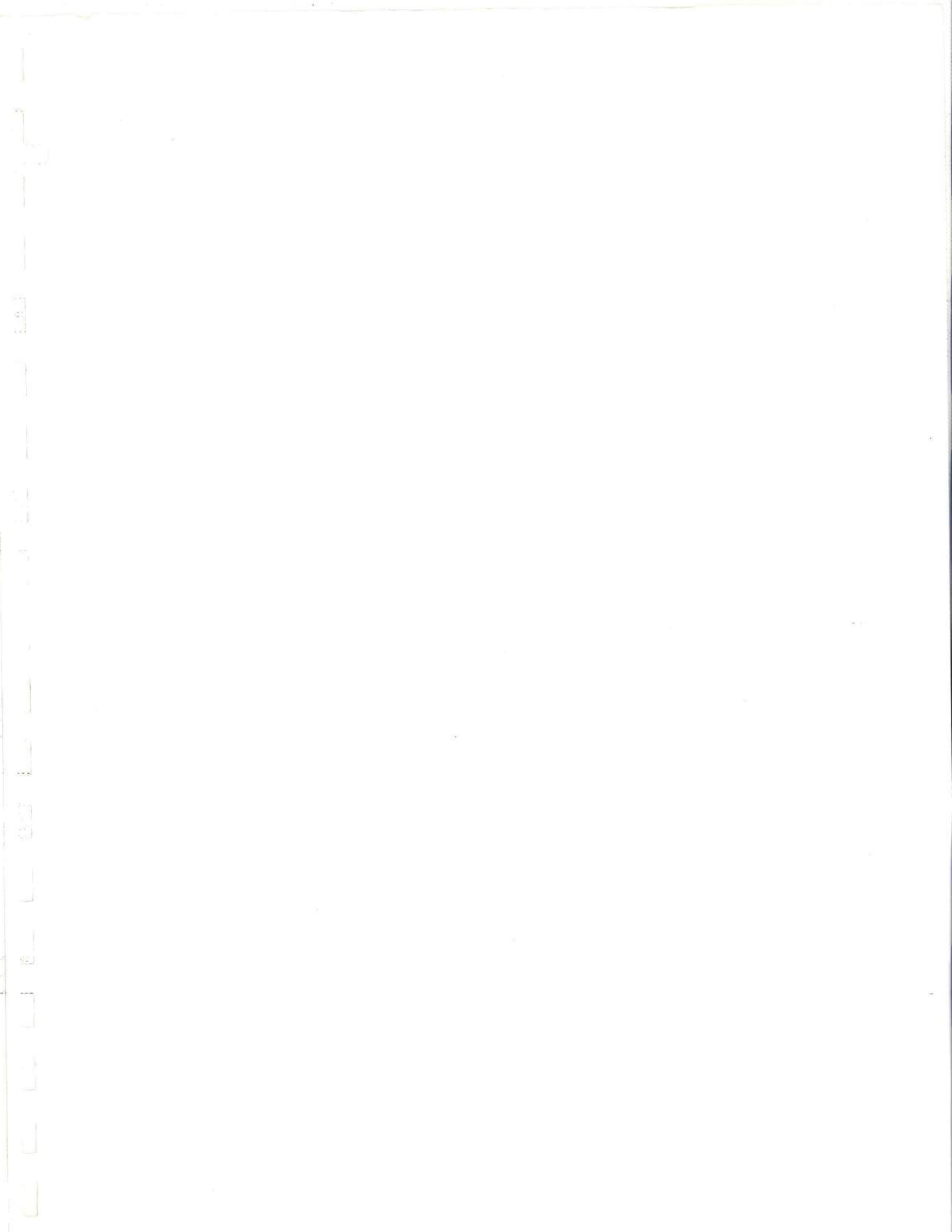
Model: platform: DS-014/SN 4479 readout: W1-110/SN 016409

Type: Electronic

Range: 0-1000 lb.









Capacity: 1000 lb.  
 Resolution:  $\pm 0.1$  lb.  
 Accuracy:  $\pm 0.1\%$

6. Fuel Balance Scale

LoKee uses the platform scale listed above to weigh the fuel charges.

7. Fuel Storage Area

LoKee stores the fuel in a humidity and temperature regulated room.

8. Moisture Meter

LoKee has two moisture meters which it uses to determine wood moisture levels.

*The primary meter is:*

Manufacturer: Delmhorst Instrument Co.  
 Model: RC-1C/SN 16152 with 26-E probe and #496 insulated pins.  
 Type: Electrical Resistance  
 Resolution:  $\pm 0.1\%$  moisture  
 Ranges: 6-11%, 11-25%, 25-80%  
 Accuracy: Moisture Content Accuracy  
                   6-12%  $\pm 0.5\%$   
                   12-20%  $\pm 1.0\%$   
                   20%-saturation point  $\pm 2.0\%$

Type of Calibration: The RC-1C is equipped with two potentiometers (Zero and Span) which are checked and adjusted on a daily basis. The unit is also checked with a calibration block.

Electrode and Pin Type: 26-E probe and #496 insulated pins

*The backup moisture meter:*

Manufacturer: Delmhorst Instrument Co.  
 Model: G-30SN/2477 with 26-E probe and #496 insulated pins  
 Type: Electrical Resistance  
 Resolution:  $\pm 0.1\%$  moisture  
 Accuracy: Moisture Content Accuracy  
                   6-12%  $\pm 0.5\%$   
                   12-20%  $\pm 1.0\%$   
                   20%-saturation point  $\pm 2.0\%$

Type of Calibration: Calibration is accomplished with an internal calibration point and a potentiometer. The calibration can also be checked against a calibration block.



Description of Operation: The pins are pounded into the wood to be sampled. The meter reading is recorded on Data Sheet #10 (Wood Moisture) or Data Sheet #11 (Density Determination). This is the uncorrected reading which is then corrected for pin insulation and, as needed, temperature using the correction tables for each parameter supplied by the manufacturer.

9. Temperature Monitors

The temperatures are monitored with Type K thermocouples. Each thermocouple's calibration is checked prior to use.

The thermocouple readout is an Omega Model 410B-K/SN 05/4475, with a range of -58 °F to 1999 °F (type K) and an accuracy of  $\pm 0.9$  °C, which can be read at  $\pm 0.1$  °F. EEMC reads and rounds to 1.0 °F. The single channel readout is interfaced with a manually operated selector switch that allows 24 channels to be monitored with the same readout. The thermocouples are attached to the test unit with sheet metal screws. The thermocouples monitoring internal stove temperature are sealed at the point of entry with sealant.

10. Draft Gauge

Manufacturer: Dwyer  
Model:  
Type: Inclined Water Manometer  
Range: 0-0.25" water  
Resolution: 0.001" water  
Accuracy:  $\pm 0.001$ " water (readability)

11. Anemometer

Manufacturer: Dwyer  
Model: 480 Vaneometer/SN S 222 D  
Range: 0-400 FPM  
Accuracy:  $\pm 5\%$  of full scale from 0-1 FPM

12. Humidity Gauge

Manufacturer: Bacharach  
Model: SAC  
Type: Sling Psychrometer  
Range: Wet Bulb: 30-110 °F  
Dry Bulb: 30-110 °F  
Resolution:  $\pm 1$  °F  
Accuracy:  $\pm 1$  °F

13. Barometer

Manufacturer: Princo Instruments, Inc.  
Model: NOVA 469





Type: Mercury Barometer  
Range: 20-32" Hg  
Resolution: 0.01" Hg  
Accuracy:  $\pm 0.01$ " when calibrated and installed as per the manufacturer's written operating instructions.

Equation 6.3.1a of the "Standard Methods for Measuring the Emissions and Efficiencies of Residential Wood Stoves" and equation #1 are programmed into a Hewlett Packard 15C calculator which first calculates stack gas flow rate and then the  $\Delta H$ . The stack gas flow rate and  $\Delta H$  are both recorded on Data sheet #2. The  $\Delta H$  is used to set the flow rate through the dry gas meter at 5 minute intervals during the test.

In order to successfully maintain the correct sampling ratio, the following data is recorded on Data Sheet #2 (Meter Box Data Sheet): temperature ( $^{\circ}\text{F}$ ) at the  $\text{SO}_2$  injection rotameter ( $\text{Tr}$ ), pressure (inches  $\text{H}_2\text{O}$ ) at the  $\text{SO}_2$  injection rotameter ( $\text{Pr}$ ),  $\text{SO}_2$  injection rate ( $\text{cc}/\text{min}$ ), barometric pressure ( $\text{BP}$ ) (inches Hg), stack gas  $\text{SO}_2$  concentration ( $\text{ppm SO}_2$ ), sampling ratio ( $\text{Sr}$ ), and the average dry gas meter temperature ( $^{\circ}\text{F}$ ). This data is entered into the HP15C, which is used to first calculate a stack gas flow rate ( $\text{dscf}$ ) and then a  $\Delta H$  for every sampling interval. The flow rate through the dry gas meter is adjusted and maintained by maintaining the appropriate  $\Delta H$ .

## CEM MONITORS

### 1. Calibration Gases

LoKee uses vendor certified ( $\pm 2.0\%$ ) calibration gases for each CEM. The concentrations purchased coincide with ranges specified in M5H. Upon receipt of the cylinder, the concentrations are verified with Method 3 (ORSAT) analysis.

### 2. Flow Regulators

LoKee uses a variety of standard gas flow regulators to meter the flow of calibration gases from the cylinders.

### 3. Point of Injection

Calibration gases are injected directly into the end of the probe. The line carrying the calibration gases from the cylinders is connected to the probe with a short piece of rubber tubing.

### 4. Sample Gas Conditioning System

The combustion gas is conditioned with a train that is a duplicate of a M5H train. It contains the following components:

SS probe

Glass 4" M5H filter and holder in a heated box



4 1000 ml glass impingers  
Glass 4" M5H filter and holder  
Indicating silica gel  
Type K thermocouple to monitor exit gas temperature  
Thomas pump

5. Filters

The filters used are the same as EPA M5H filters.

6. Manifold and Exhaust

The gas stream is delivered to each analyzer through a manifold and flowmeter with the excess gases being routed to an exhaust.

7. CO Analyzer

Horiba PIR 2000/SN 408005  
Nondispersive infrared (NDIR)

The gas stream flow is controlled by a SS flowmeter downstream of the analyzer. The calibrated range used is 0-10.0% by volume. The resolution is 0.01% CO. The manufacturer's specification given for linearity is  $\pm 1.0\%$ .

8. CO<sub>2</sub> Analyzer

Horiba PIR 2000/SN 407069

The CO<sub>2</sub> analyzer is also a NDIR and is operated in exactly the same manner as the CO analyzer. The range of the CO<sub>2</sub> analyzer is 0-25.0% CO<sub>2</sub>.

## COMBUSTION GAS ANALYZER TRAIN OPERATING INSTRUCTIONS

A. Pretest Preparation, Checks and Audit Procedures

1. Clean the probe with acetone and a brush. Seal the end of the probe for a leak check.
2. Remove the filter holder from the sample box and change the filter.
3. Empty water from all the impingers in the train. Clean all impingers and fill the first 2 with 100 ml of water.
4. Remove the second filter holder from the train and change the filter.
5. Visually check the indicating silica gel in the fourth impinger. If it is visibly impacted by water, replace the silica gel with dry silica gel.
6. Turn on the pump and perform a leak check on the entire train. This is done by placing the exhaust line in water. A successful leak check is accomplished when no bubbles are detected.
7. Slowly release the plug from the probe to prevent any back flushing.
8. Turn off the pump.





9. Turn on the heat in the sample box. Adjust Variac voltage controller so that temperature in the sample box does not exceed 248 °F.
10. Open the bypass valve on the pump.
11. Connect the probe to the zero/span gas delivery line.
12. Turn on the zero gas and adjust the flow rate to 1.5 SCFH.
13. Wait until the zero gas has completely flushed the train and a stable reading is obtained.
14. Record the zero gas readings of the DVM on Data Sheets #15.
15. Turn off the zero gas at the cylinder.
16. Disconnect the zero/span gas delivery line from the zero gas cylinder.
17. Connect the zero/span gas delivery line to the span gas source for each analyzer.
18. Turn on the span gas and adjust the flow rate to 1.5 SCFH. Wait until a stable reading is obtained on each analyzer. Repeat until all three analyzers are spanned properly.
19. Record the span gas readings of the DVM. Record the analyzer's output and all other pertinent information Data Sheets #15.
20. Turn off the span gas at the cylinder.
21. Disconnect the probe from the zero/span gas delivery line.
22. Insert the probe in the stack.
23. Close the bypass valve on the pumps.
24. Approximately 15-20 minutes before the actual start of the test, turn on the pump and adjust the flow through each analyzer until the flow rate is 1.5 SCFH.

**B. Operation During Testing**

1. Monitor the flow rate to the analyzers periodically to maintain a flow rate of 1.5 SCFH. Make any necessary adjustments.
2. Record data as follows:
  - a. At the start of each 5 minute data cycle, record the scale weight, wet bulb/dry bulb, stack gas temperature and static pressure on Data Sheet #12 (Gas Data).
  - b. Record the combustion gas (CO<sub>2</sub>, O<sub>2</sub> and CO) analyzer data and the SO<sub>2</sub> analyzer data on Data Sheet #12.
  - c. Record the remainder of the temperature data.

**C. Post Test Checks and Audit Procedures**

1. Remove the probe from the stack. (Be careful when handling the probe as it can be quite hot.)
2. Seal the end of the probe.
3. Perform a leak check on the entire train.
4. Slowly release the plug from the end of the probe to prevent any back flushing.
5. Turn off the pump.



6. Open the bypass valve on the pump.
7. Connect the probe to the zero/span gas delivery line.
8. Turn on the zero gas and adjust the flow rate through each analyzer to 1.5 SCFH.
9. Wait until the zero gas has completely flushed the train and a stable reading is obtained from each analyzer.
10. Record the zero gas reading. Record each analyzer's output and all other pertinent information on Data Sheets #15.
11. Turn off the zero gas at the cylinder.
12. Disconnect the zero/span gas delivery line from the zero gas cylinder.
13. Connect the zero/span gas delivery line to the span gas source for each analyzer.
14. Turn on the span gas and adjust until the flow rate through each analyzer to 1.5 SCFH. Wait until the span gas has completely flushed the train and a stable reading is obtained on each analyzer.
15. Record the span gas reading. Record each analyzer's output and all other pertinent information on Data Sheets #15.
16. Turn off the span gas at the cylinder.
17. Disconnect the probe from the zero/span gas delivery line.

D. Determination of the Combustion Gas Train's Response Time

1. The response time of the combustion gas analyzer train is to be determined using the following procedures. It is best to determine the combustion gas analyzer train response time during the "charcoal phase" of a test burn so that CO levels are relatively stable.
  - a. Leak check the combustion gas (CEM) analyzer train.
  - b. Zero the CO analyzer using ambient air.
  - c. Calibrate the CO analyzer.
  - d. Insert the probe for the combustion gas analyzer train in the stack.
  - e. Sample flue gas until a stable reading is obtained.
  - f. Remove the probe from the stack, note the exact CO concentration as measured on the DVM and start a stop watch at the exact time of removal.
  - g. Observe the stop watch and DVM. Record the length of time to initial response, i.e., when the CO levels begin to decline.
  - h. Continue observing the stop watch and DVM. Record the time when the analyzer's output equals zero (0.000 v).
  - i. Repeat steps d-h 2 or 3 times to verify results.

E. Calibration and Audit Procedures for the Combustion Gas Analyzers



1. Calibrate by presenting zero and span gases to each analyzer at the probe and through the entire sampling train. (See Sections 6.7.2 and 6.9 [M5H].) Record the responses on the appropriate calibration forms.
2. Immediately prior to and after each test run, present the zero and span gases to the analyzers through the entire sampling train as is discussed in section C. Record each analyzer's response on Data Sheets #15.
3. Calculate the  $\pm$  concentration difference and the actual percent difference as follows using the zero and span gas values obtained in #2 above. All calculations are to be based upon the actual gas concentrations involved.

$$\pm \text{ Concentration Difference} = \text{Actual Conc (\%)} - \text{Std Conc (\%)}$$

$$\text{Zero \% Difference} = \frac{\text{Act Conc (\% or ppm)} - \text{Std Conc (\% or ppm)}}{\text{Full Scale Value (\% or ppm)}} * 100$$

$$\text{Span Act \% Difference} = \frac{\text{Act Response (\% or ppm)} - \text{Exp Response (\% or ppm)}}{\text{Full Scale Value (\% or ppm)}} * 100$$

Then refer to Section 4.2 and 4.3 (M5H) to determine whether the audits are acceptable or not.

#### TRACER GAS (SO<sub>2</sub>) EQUIPMENT

1. SO<sub>2</sub> Injection Probe  
A circular SS loop about 4" in diameter is positioned in the center of the stack. The loop extends outside the stack and is connected to the line leading from the SO<sub>2</sub> injection rotameter with Sweglock fittings. The loop is inserted in the stack at 9.5  $\pm$  0.5 ft above the top of the scale.
2. Rotameter  
A rotameter that has been calibrated with a bubble tube. The rotameter is all glass, stainless steel and Teflon. The rotameter has a flow control mechanism which is set to the calibrated flow.
3. Temperature  
The temperature at the injection rotameter is measured with a type K thermocouple.
4. Injection Gas  
Pure SO<sub>2</sub>, 99.999% pure, released from the cylinder through a SS regulator and shut off valve.
5. Calibration Gases





LoKee uses vendor certified calibration gases with traceability established in accordance with EPA Protocol #1 as specified in Section 3.3.1 and verified using EPA Method 6.

6. Sample Probe  
3/8" SS tubing inserted at 13.5 ±0.5 feet above the platform scale. No obstructions are in the stack between the injection and sample probes.
7. Combustor  
Lindberg tube furnace, Model 55035/SN 800125, range 0-2000 °F. The temperature in the tube furnace is monitored with a type K thermocouple and controlled with a Variac voltage regulator. Power adjustments are made as necessary to maintain temperature at 1425 °F ±25 °F.
8. Sample Condenser  
The sample condenser consists of 3 modified M5 impingers immersed in a freezer.  
A filter assembly  
The exit gas temperature is monitored with a type K thermocouple.
9. Filter  
A standard EPA M5H 3" or 4" filter.
10. SO<sub>2</sub> Analyzer  
Horiba, PIR 2000/SN 403019  
Nondispersive infrared (NDIR)  
The analyzer is operated as per the manufacturer's instructions at a flow rate of 1.5 SCFH. The calibration range is 0-2500 ppm SO<sub>2</sub> at a resolution of ±25.0 ppm. The manufacturer's specification for linearity is ±1.0%. The voltage response is displayed on a DVM which is converted to ppm using the manufacturer's calibration curves.
11. Flow Control  
Flow through the tracer gas sampling train is controlled by a SS flowmeter.

## TRACER GAS TRAIN OPERATING INSTRUCTIONS

- A. Pretest Preparation and Checks and Audit Procedures
  1. Clean the probe with a brush. After cleaning, seal the end of the probe. **Note: Do Not Use Acetone Or Other Organic Solvents To Clean The Probe Immediately Prior To Running A Test Or Conducting A Leak Check.**
  2. Turn on the tube furnace in order to insure that the unit is at the correct operating temperature (1425 °F) at the start of the test.
  3. Remove all water and clean the impingers.
  4. Change the filter.
  5. Turn on the pump.



6. Perform a leak check on the entire tracer gas train. This is done by placing the SO<sub>2</sub> exhaust line in water. A successful leak check is accomplished when no bubbles are detected.
7. Slowly remove the plug from the end of the probe to prevent any back flushing.
8. Turn off the pump.
9. Bypass the pump.
10. Connect the probe to the zero/span delivery gas line.
11. Connect the zero/span gas delivery line to the zero gas cylinder and turn on the zero gas and adjust the flow until the flow rate through the SO<sub>2</sub> analyzer is 1.5 SCFH.
12. Wait until the zero gas has completely flushed the train.
13. Record the zero gas reading. Record the SO<sub>2</sub> analyzer's DVM output on Data Sheets #15.
14. Turn off zero gas at the cylinder.
15. Disconnect the zero/span gas delivery line from the zero gas cylinder.
16. Connect the zero/span gas delivery line to the span gas cylinder.
17. Turn on the span gas and adjust the flow until the flow rate through the SO<sub>2</sub> analyzer is 1.5 SCFH. Wait until the span gas has completely flushed the train and a stable reading is obtained on the analyzer.
18. Record the span gas reading. Record the analyzer's output and all other pertinent information on Data Sheets #15.
19. Turn off the span gas at the cylinder.
20. Disconnect the zero/span gas delivery line from the probe.
21. Insert the probe in the stack.
22. Close the bypass on the pump.
23. Approximately 15 to 20 minutes before the actual start of the test, turn on the SO<sub>2</sub> injection train and the pump for the tracer gas train.

**B. Operation**

1. Turn on the tube furnace to insure furnace is at approximately 1425 °F when the test begins.
2. Approximately 15-20 minutes before the actual start of the test, turn on the cylinder of pure SO<sub>2</sub>.
3. Using the rotameter's current calibration, adjust the SO<sub>2</sub> flow rate to the calibrated level.
4. Turn on the pump in the tracer gas train. Adjust the flow rate through the SO<sub>2</sub> analyzer so that it remains at 1.5 SCFH.
5. Monitor the SO<sub>2</sub> concentrations in the stack and stack gas flow rates in order to establish a sampling ratio for the test and a correct  $\Delta H$  at the start of the test.





6. At the start of the test and every 5 minutes thereafter, record the SO<sub>2</sub> analyzer output in volts and the stack gas SO<sub>2</sub> concentration in order to calculate the stack gas flow rate and determine the correct  $\Delta H$  for the meter box.

Also monitor and record the temperature at the Rotameter (Tr), pressure at the Rotameter (Pr), barometric pressure (BP) SO<sub>2</sub> injection rate (cc/min) and static pressure on Data Sheets #2 and #12.

C. Post Test Checks and Audit (Zero/Span) Procedures

1. Remove the probe from the stack. (Be careful when removing the probe from the stack as it can be quite hot.)
2. Plug the end of the probe.
3. Perform a leak check.
4. Slowly remove the plug from the end of the probe to prevent any back flushing.
5. Turn off the pump.
6. Bypass the pump.
7. Connect the probe to the zero/span gas delivery line.
8. Connect the zero/span gas delivery line to the zero gas cylinder. Turn on and adjust until the flow rate through the SO<sub>2</sub> analyzer is 1.5 SCFH.
9. Wait until the zero gas has completely flushed the train.
10. Record the zero gas reading. Record the SO<sub>2</sub> analyzer's DVM output on Data Sheet #15.
11. Turn off zero gas at the cylinder.
12. Disconnect the zero/span gas delivery line from the zero gas cylinder.
13. Connect the zero/span gas delivery line to the span gas cylinder.
14. Turn on the span gas and adjust the flow until the flow rate through the SO<sub>2</sub> analyzer is 1.5 SCFH. Wait until the span gas has completely flushed the train and a stable reading is obtained.
15. Record the span gas reading. Record the analyzer's output and all other pertinent information on Data Sheet #15.
16. Turn off the span gas at the cylinder.
17. Disconnect the zero/span gas delivery line from the probe.

D. Determination of Tracer Gas Train's Response Time

1. Zero and calibrate the SO<sub>2</sub> analyzer.
2. Prepare and leak check the tracer gas train as per A above.
3. Insert the probe in the stack which contains flue gas and SO<sub>2</sub> concentrations in the ranges normally encountered during wood stove testing.



4. Sample flue gas with SO<sub>2</sub> concentrations until a stable reading is obtained. It is best to determine the tracer gas train's response time during the "charcoal phase" of a test burn so that the SO<sub>2</sub> concentrations are as stable as possible.
5. Remove the probe from the stack, noting the exact SO<sub>2</sub> concentration as measured by the DVM and starting a stop watch at the exact time of removal.
6. Observe the stop watch and DVM. Record the length of time to the initial response, i.e., when the SO<sub>2</sub> levels begin to decline.
7. Continue observing the stop watch and DVM. Record the time when the SO<sub>2</sub> analyzer's output equals zero (0.000 v.).
8. Repeat steps 3-7 two or three times to verify results.

**E. Calibration and Audit Procedures for the Tracer Gas (SO<sub>2</sub>) Analyzer**

1. Calibrate by presenting zero and span gases to the analyzer at the probe and through the entire sampling train. Record the responses on the appropriate calibration form.
2. Immediately prior to and after each test run, present the zero and span gases to the analyzer through the entire sampling train as is discussed in Sections A and C. Record the analyzer's response on Data Sheet #15.
3. Calculate the ± concentration differences and actual percent difference as follows using values obtained in #2 above as the expected response. All calculations are to be based upon the actual gas concentration involved.

$$\pm \text{Concentration Difference} = \text{Actual Conc (\%)} - \text{Std Conc (\%)}$$

$$\text{Zero \% Difference} = \frac{\text{Act Conc (\% or ppm)} - \text{Std Conc (\% or ppm)}}{\text{Full Scale Value (\% or ppm)}} * 100$$

$$\text{Span Act \% Difference} = \frac{\text{Act Response (\% or ppm)} - \text{Exp Response (\% or ppm)}}{\text{Full Scale Value (\% or ppm)}} * 100$$

Then refer to Section 4.2 and 4.3 (M5H) to determine whether the audits are acceptable or not.

**TEMPERATURE SENSING OPERATING INSTRUCTIONS**

- A. Operate the thermocouple readout selector switch and record the temperature for each thermocouple. All the temperature in the test facility should be approximately the same. Repair as necessary.



- B. Check the operation and output of the thermocouple readout using the Omega NBS Traceable Thermocouple Simulator. The simulator is hooked up to thermocouple readout #23. Check the readout over its full range at 200 °F intervals. Record the data on Data Sheet #16.
- C. One hour before the actual test start record stove temperatures (thermocouple readout #'s 4, 5, 6, 7 and 8), firebox (readout #9), post catalytic combustor or secondary burn chamber (readout #10), and room temperature (readout #11). Record the temperatures every 5 minutes until the start of the test on Data Sheet #13 (Preburn).
- D. During the test record the temperatures every 5 minutes for each of the thermocouples on Data Sheets #12 and 14.

#### FUEL PREPARATION

- A. No more than 4 hours prior to use, obtain 3 moisture readings from each piece of wood. Record all moisture readings on Data Sheet #10.
- B. Obtain kindling by finely splitting pieces that otherwise cannot be used as test fuel. Weigh the kindling and record the weight on Data Sheet #8.
- C. Obtain the pretest fuel by using 2 x 4's. The length of the pretest fuel can be no less than 1/3 the length of the test fuel. Weigh the pretest fuel prior to its being loaded in the stove. Record weights on Data Sheets #8 and #9.
- D. Obtain the test fuel by cutting dimensional lumber (either 2 x 4's or 4 x 4's) so that the length is 5/6's the length of the longest usable dimension of the firebox. Use the mix of 2 x 4's and 4 x 4's specified in Section 4.3 M28. The test fuel shall be essentially free of knots, sap seams or rotten areas.
- E. The spacers shall measure 1 x 5 x 1" (nominally). The spacers shall be free of knots, sap seams or rotten areas. Nail the spacers to the 2 x 4's and 4 x 4's as described in the regulations.
- F. Take a photograph of the assembled fuel charge at a 90° angle from the photograph that will be take when the fuel charge is loaded in the stove.

#### WOOD DENSITY DETERMINATION

- A. When cutting the test fuel, cut a representative piece of 2 x 4 or 4 x 4 that is approximately 3 to 5-inches in length.
- B. Take a moisture reading from the top, bottom and side of the piece. Record readings on Data Sheet #11. Determine the % moisture on a wet and dry basis.
- C. Weight the piece on a balance.
- D. Take measurements of width, depth and length at the four corners with a micrometer. Determine the volume of the piece. (Length x width x depth = Volume in cubic centimeters)
- E. Dry the piece in an oven at 95-100 °C for a minimum of 24 hours.
- F. Reweigh the piece on the balance.





- G. Calculate % moisture on a dried basis.

$$\% \text{ moisture (dry basis)} = 1 - \frac{\text{dried weight}}{\text{wet weight}} * 100$$

- H. Calculate the density.

$$\text{Density (g/cc)} = \frac{\text{dried weight (g)}}{\text{volume (cc)}}$$

#### BTU'S/LB DETERMINATION

- A. When cutting the test fuel (only the test fuel, not the kindling, pretest fuel or spacers), collect a sawdust sample. Place in a clearly marked plastic bag.
- B. Forward sample to a commercial laboratory for BTU contents analysis.

#### STOVE PREPARATION

- A. Clean the stove.
- B. Weigh the stove, record the weight on Data Sheet #8.
- C. Add approximately 0.3 lb. of wadded newspaper to the stove. Record weight of newspaper on Data Sheet #8. Add 4-8 lb. of kindling to the stove, and record the weight of the kindling on Data Sheet #8.
- D. Light the paper and kindling, leaving the stove's air draft control(s) wide open and the door cracked until well ignited.
- E. Close door.
- F. When between 50% - 75% of the weight of the kindling has been burned add the first pretest fuel charge.
- G. Continue to add pretest fuel until the stove has thoroughly warmed up. As necessary, rake the coal bed prior to adding additional pretest fuel charges.
- H. Remove all material from the firebox after two or more hours of burning on high. Obtain the dry empty stove weight and record on Data Sheet #8.
- I. Set the stove's air draft control(s) at the desired setting a minimum of 1 hour before the test run is to begin.
- J. As necessary set the heat exchange blower(s) at the specified setting a minimum of one hour before the test is to begin.
- K. Record the stove surface temperatures, firebox and post catalytic or secondary burn temperatures and scale weigh for a minimum of one hour before the test run begins. As necessary add fuel,



rake the coal bed, level the coal bed and/or remove coals during the first 45 minutes of the hour immediately preceding the start of the test. Record all information concerning raking, fuel additions, etc. on Data Sheet #13.

- L. If necessary, sometime during the last 15 minutes before the start of the test, open the door and break up all large pieces and then rake and level the pretest fuel in the stove. At this time, level the coal bed as necessary to accommodate loading the fuel charge into the stove. Close the door. Total time door can be open during the last 15 minutes is 1 minute. No further manipulation of the stove is allowed during the 15 minutes immediately preceding the start of the test.
- M. When the weight of the coal bed equals 20-25% of the weight of the test fuel charge, load the test fuel. Take a photograph of the fuel load in the stove immediately after loading the fuel. Leave the door open as per the manufacturer's instruction, but no longer than 5 minutes.
- N. Document all stove operating data from ignition through loading and test start up on Data Sheet #9.

